

STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: siting.council@ct.gov

www.ct.gov/csc

September 24, 2009

Steven L. Levine
Real Estate Consultant
New Cingular Wireless PCS, LLC
500 Enterprise Drive
Rocky Hill, CT 06067-3900

RE: **EM-CING-T-MOBILE-103-090901** - New Cingular Wireless PCS, LLC and T-Mobile Northeast LLC notice of intent to modify an existing telecommunications facility located off Willruss Street, Norwalk, Connecticut.

Dear Mr. Levine:

The Connecticut Siting Council (Council) hereby acknowledges your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies.

The proposed modifications are to be implemented as specified here and in your notice dated September 1, 2009, including the placement of all necessary equipment and shelters within the tower compound. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

Very truly yours,


S. Derek Pappas
Executive Director

SDP/MP/laf

c: The Honorable Richard Moccia, Mayor, City of Norwalk
Michael Greene, Director of Planning and Zoning, City of Norwalk
Hans Fiedler, T-Mobile USA, Inc.
John R. Morissette, Manager - Transmission Siting and Permitting, Northeast Utilities Service Company
Daniel J. Garstka, Senior Engineer, Transmission Project, Northeast Utilities Service Company



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051

Phone: (860) 827-2935 Fax: (860) 827-2950

E-Mail: siting.council@ct.gov

www.ct.gov/csc

September 2, 2009

The Honorable Richard Moccia
Mayor
City of Norwalk
City Hall
125 East Avenue
P. O. Box 5125
Norwalk, CT 06856-5125

RE: **EM-CING-T-MOBILE-103-090901** - New Cingular Wireless PCS, LLC and T-Mobile
Northeast LLC notice of intent to modify an existing telecommunications facility located off
Willruss Street, Norwalk, Connecticut.

Dear Mayor Moccia:

The Connecticut Siting Council (Council) received this request to modify an existing telecommunications
facility, pursuant to Regulations of Connecticut State Agencies Section 16-50j-72.

If you have any questions or comments regarding this proposal, please call me or inform the Council by
September 17, 2009.

Thank you for your cooperation and consideration.

Very truly yours,

S. Derek Phelps
Executive Director

SDP/jbw

Enclosure: Notice of Intent

c: Michael Greene, Director of Planning and Zoning, City of Norwalk



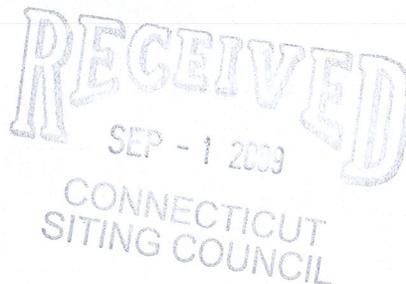
New Cingular Wireless PCS, LLC
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7636
Fax: (860) 513-7190

Steven L. Levine
Real Estate Consultant

ORIGINAL

September 1, 2009

Honorable Daniel F. Caruso, Chairman,
and Members of the Connecticut Siting Council
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051



Re: Notice of Exempt Modification – Existing CL&P Transmission Tower off Willruss Street, Norwalk

Dear Chairman Caruso and Members of the Council:

New Cingular Wireless PCS, LLC (“AT&T”) and T-Mobile Northeast LLC (“T-Mobile”) intend to modify their existing telecommunications facilities off Willruss Street in Norwalk. AT&T and T-Mobile each operate under licenses issued by the Federal Communications Commission (“FCC”) to provide cellular and PCS mobile telephone service in Fairfield County.

T-Mobile has authorized AT&T to submit this Notice on its behalf.

Please accept this letter as notification to the Council, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter is being sent to the Mayor of Norwalk.

Existing Facility

The Norwalk facility is located off Willruss Street, approximately 1/3 mile west of the intersection of US Hwy 7 and CT Rte 123. Site coordinates (NAD83) are N41° 07’ 34” and W73° 25’ 58”.

The facility is owned and managed by the Connecticut Light and Power Company (“CL&P”), and consists of a 94-foot self-supporting lattice electric transmission structure (CL&P Line #1880, Structure #1102) and separate fenced compounds for AT&T and T-Mobile radio

equipment. AT&T was approved under Council Petition 446 in 2000 to install an extension mast and three antennas atop the CL&P structure. Subsequently, T-Mobile was approved under Petition 734 in 2005 to install a second extension mast with two clusters of three antennas each.

Currently, AT&T and T-Mobile antennas are mounted on separate masts extending to 13 ft. and 23 ft. AGL, respectively, above the transmission structure. AT&T currently operates antennas at a centerline height of 104 ft. AGL on its extension mast. T-Mobile installed three of the six antennas originally planned for the site, and currently operates antennas at centerline 114 ft. AGL on its mast.

Proposed Modifications

Attached to this Notice are a location map, pre- and post-modification tower profile drawings, site plans, and a structural analysis report demonstrating that the tower is structurally capable of supporting the proposed AT&T and T-Mobile modifications.

T-Mobile

T-Mobile proposes to replace its three existing panel antennas and three TMAs with different antennas at 114 ft. AGL. In addition, T-Mobile will install three additional panel antennas, for a total of six. Were these antennas placed on the existing T-Mobile mast at a height of 104 ft. AGL, as contemplated in Petition No. 734, there would be potential for significant RF interference between these antennas and the AT&T antennas also at 104 ft. AGL. In order to resolve this RF issue, the two carriers have agreed that the existing AT&T mast should be replaced with a new 10-ft.-longer mast to match the height of the existing T-Mobile mast. Both sets of T-Mobile antennas will be installed at a centerline height of 114 ft. AGL (on separate masts), and AT&T's will remain at 104 ft. AGL, thereby eliminating the potential for RF interference. Six additional coaxial cables, associated with the second set of antennas, will also be installed.

T-Mobile has two equipment cabinets within a fenced compound. One of the two cabinets will be replaced with a new cabinet.

AT&T

AT&T's proposed modifications would take place on the replacement extension mast proposed by T-Mobile, per the above discussion. As shown on the attached drawings and as further described below, AT&T proposes to replace its existing antenna array with a new array of three Powerwave 7770-panel antennas, or their functional equivalents, and six Powerwave TMA's at the existing centerline height of 104 ft. AGL. No additional coax cables are required. This modification is for the purpose of installing UMTS equipment as part of the on-going statewide UMTS upgrade.

Statutory Considerations

The changes to the Norwalk tower facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in R.C.S.A. Section 16-50j-72(b)(2) because they will not result in any substantial adverse environmental effect.

1. The height of the overall structure will be unaffected. The proposed replacement mast will not exceed the height of the existing T-Mobile mast.
2. The proposed changes will not affect the property boundaries. All new construction will take place inside the existing fenced compound.
3. The proposed additions will not increase the noise level at the existing facility by six decibels or more.
4. Operation of the T-Mobile and AT&T antennas will not increase the total radio frequency electromagnetic radiation power density, measured at the tower base, to or above the standard adopted by the State of Connecticut and the FCC. The "worst-case" exposure calculation in accordance with FCC OET Bulletin No. 65 (1997) for a point of interest at the base of the structure in relation to the operation of the proposed antenna arrays is as follows:

Company	Centerline Height (feet)	Frequency (MHz)	Number of Channels	Power Per Channel (Watts)	Power Density [†] (mW/cm ²)	Standard Limits (mW/cm ²)	Percent of Limit
T-Mobile GSM *	114	1945	8	185	0.0409	1.0000	4.09
T-Mobile UMTS *	114	2100	2	772	0.0427	1.0000	4.27
AT&T GSM	104	1930-1935 1965-1970	2	427	0.0284	1.0000	2.84
AT&T GSM	104	880-894	4	296	0.0394	0.5867	6.71
AT&T UMTS	104	1930-1935 1965-1970	1	500	0.0166	1.0000	1.66
AT&T UMTS	104	880-894	1	500	0.0166	0.5867	2.83
TOTAL							22.4%

* Power density parameters from T-Mobile.

† Please note that the standard power density equation provided by the Council in its memo of January 22, 2001 incorporates a ground reflection factor of 2.56 (i.e., the square of 1.6) as described in FCC OET Bulletin No. 65.

As the table demonstrates, the cumulative "worst-case" power density would be 22.4 % of the ANSI/IEEE standard, as calculated for mixed frequency sites. Total power density levels

resulting from AT&T's and T-Mobile's use of the tower facility would thus remain within applicable standards.

For the foregoing reasons, New Cingular Wireless PCS, LLC and T-Mobile Northeast LLC respectfully submit that proposed changes at the Norwalk facility constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me with any questions concerning this notice. Thank you for your consideration in this matter.

Respectfully yours,

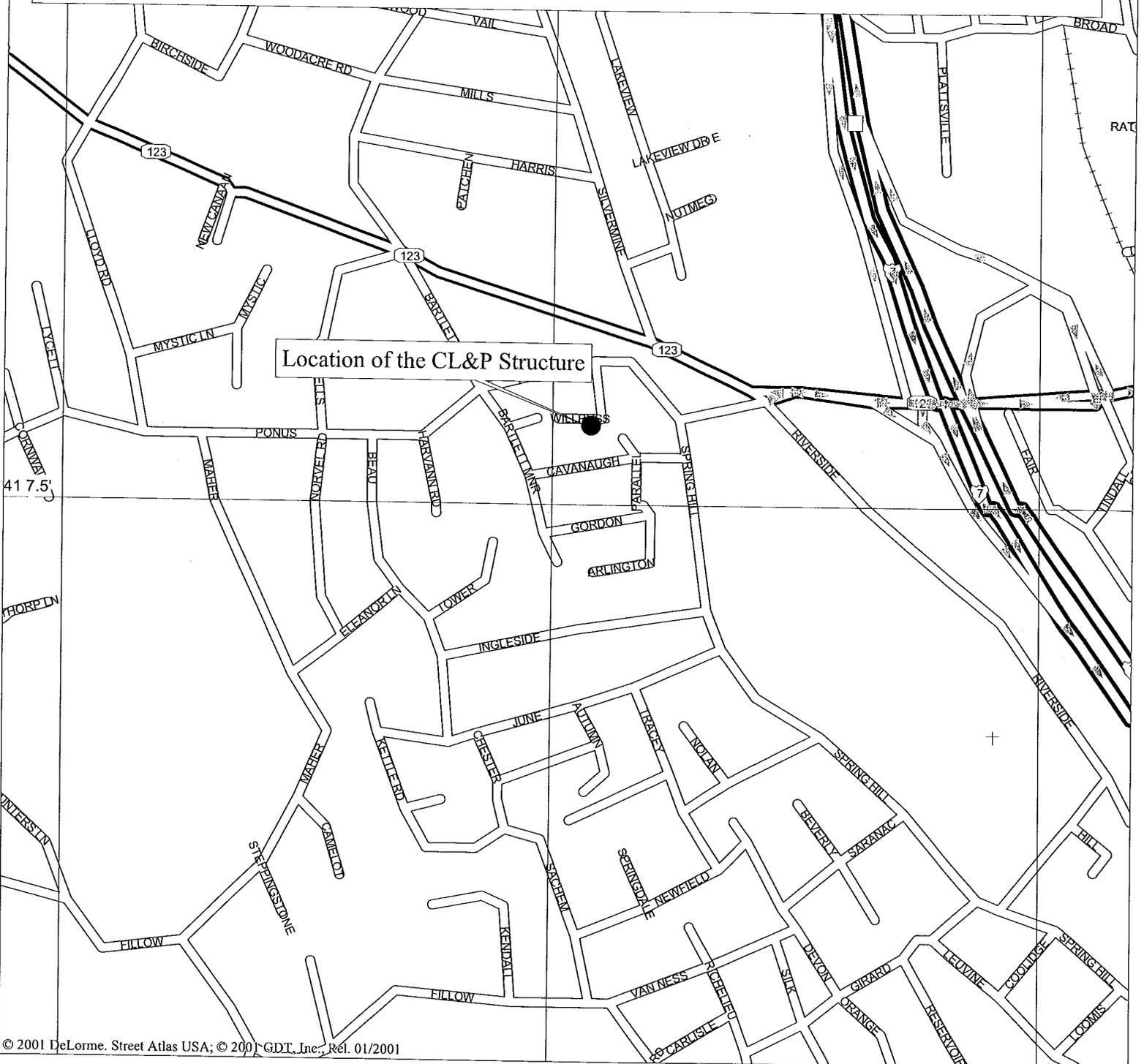
A handwritten signature in blue ink, appearing to read 'S. Levine'.

Steve Levine
Real Estate Consultant

Enclosures

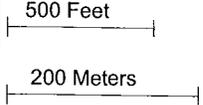
cc: Honorable Richard Moccia, Mayor, City of Norwalk
Michele G. Briggs, Manager of Real Estate
Jennifer Young Gaudet, T-Mobile Northeast LLC
Christopher B. Fisher, Esq.

Norwalk - Willruss Street



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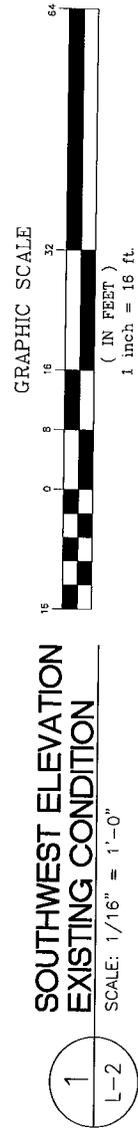
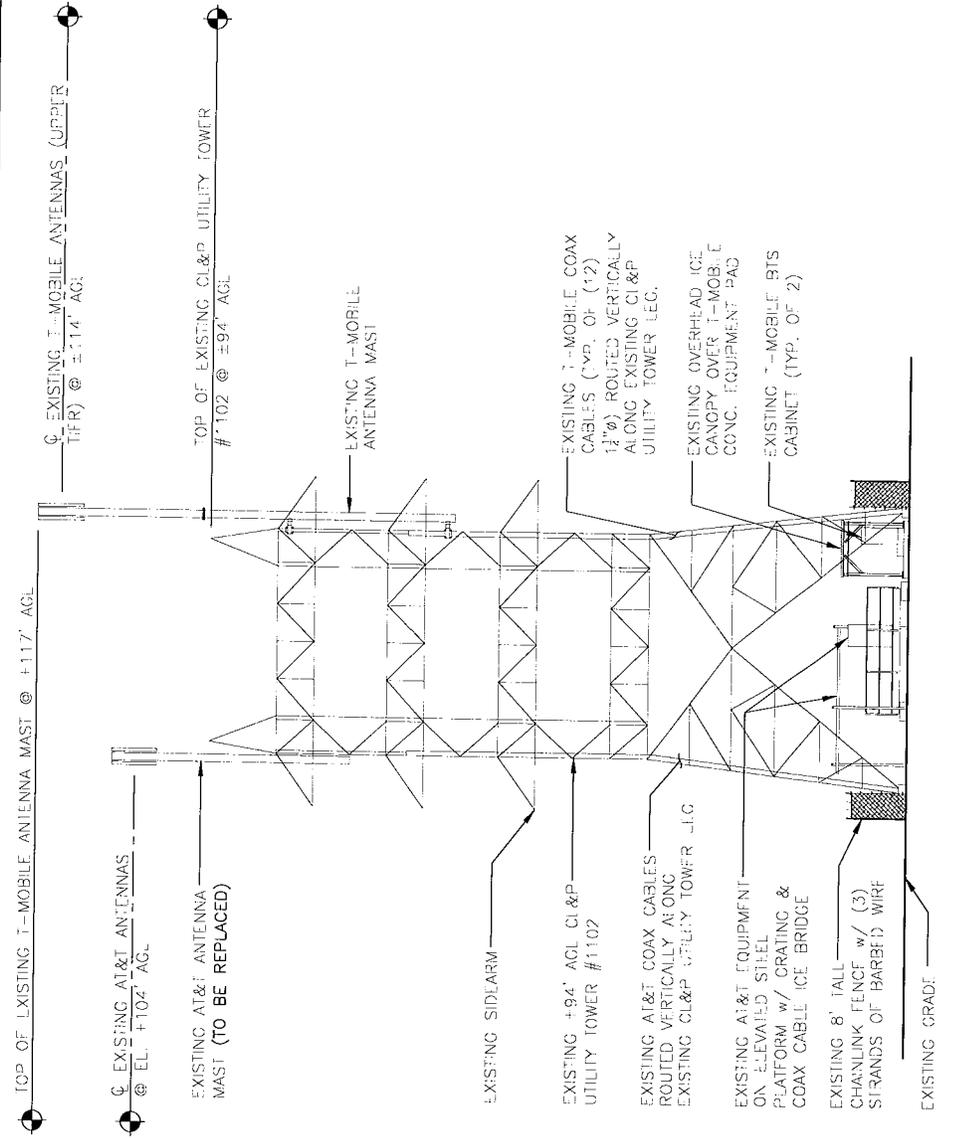
Mag 16.00
 Thu Aug 27 09:19 2009
 Scale 1:7,812 (at center)



- Local Road
- Major Connector
- State Route
- Interstate/Limited Access
- Exit
- Railroad
- Cemetery
- Population Center
- Water
- River/Canal

LEASE EXHIBIT

THIS LEASE PLAN IS DIAGRAMMATIC IN NATURE AND IS INTENDED TO PROVIDE GENERAL INFORMATION REGARDING THE LOCATION AND SIZE OF THE PROPOSED WIRELESS COMMUNICATION FACILITY. THE SITE LAYOUT WILL BE FINALIZED UPON COMPLETION OF SITE SURVEY AND FACILITY DESIGN.



REV	DATE	BY	CHK'D BY	DESCRIPTION
01	07/29/09	DEB	DEB	LEAST EXHIBIT - REVIEW
02	12/21/09	DEB	DEB	LEAST EXHIBIT - REVIEW

PROFESSIONAL ENGINEER SEAL

NAIOPMM
T Mobile

T-MOBILE
PROPOSED WIRELESS COMMUNICATIONS FACILITY (W/ST. WORK)
CT11356C
CL&P TOWER - RTE 123
10 MILLERS STREET
NEWARK, CT 06602

DATE: 12/7/09
SCALE: AS SHOWN
JOB NO.: 0817A-025

LEASE EXHIBIT
SHEET NO. L-2
Sheet No. 2 of 2

(3) RFS APX16PV-16PVL
 PANEL ANTENNA AND (6)
 POWERWAVE LGP214 TMAS

☉ T-MOBILE ANTENNAS
 EL. ±114'-0" AGL

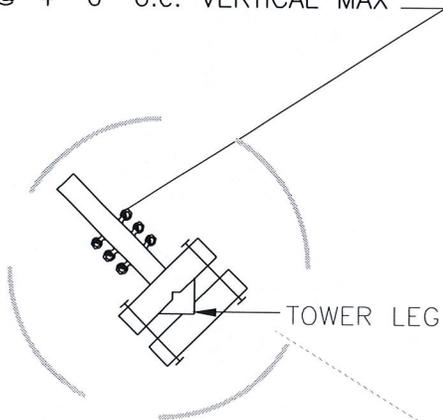
(3) RFS APX16DWV-
 16DWVS-A20
 PANEL ANTENNAS

☉ T-MOBILE ANTENNAS
 EL. ±114'-0" AGL

(3) POWERWAVE 7770
 PANEL ANTENNAS AND (6)
 POWERWAVE LGP214 TMAS

☉ AT&T ANTENNAS
 EL. ±104'-0" AGL

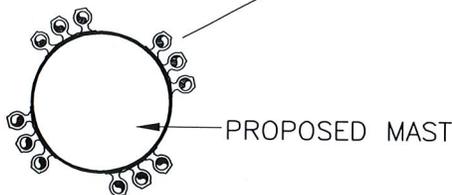
UNIVERSAL SNAP-IN BRACKET FOR
 ANGLE LEG, VALMONT-MICROFLECT
 (P/N B2249). w/ VALMONT
 SNAP-IN HANGER (P/N B1562)
 @ 4'-0" o.c. VERTICAL MAX



TOWER LEG

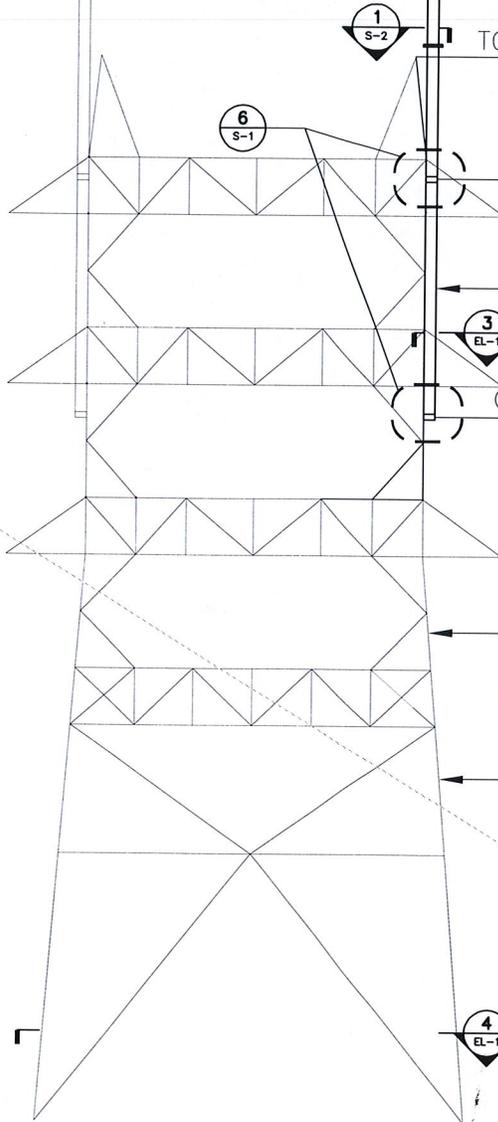
2 COAX MOUNTING PLAN
 EL-1 NOT TO SCALE

(12) 1-1/4" DIA. COAX CABLES
 MOUNTED TO PROPOSED PIPE
 MAST @ 4'-0" o.c. VERTICAL MAX.
 w/ VALMONT SNAP-IN HANGER
 (P/N B1562), MONOPOLE
 TRANSMISSION LINE BRACKET (P/N
 B3254), STAINLESS STEEL
 BANDING (P/N B1769) AND
 BUCKLES (P/N B1770)



PROPOSED MAST

3 COAX MOUNTING PLAN
 EL-1 NOT TO SCALE



HEIGHT OF MAST
 PROPOSED

HEIGHT OF MAST
 EXISTING

☉ TOP EXISTING NU TOWER
 ±94'-0" AGL

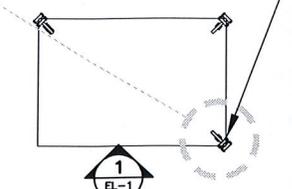
☉ TOP CONNECTION
 EL. ±83'-6" AGL

PROPOSED 12" DIA.
 SCH.80 PIPE MAST

☉ BOTTOM CONNECTION
 EL. ±62'-0" AGL

EXISTING (6) 1-1/4"
 DIA. COAX CABLES
 MOUNTED ON TOWER LEG

PROPOSED (6) 1-1/4"
 DIA. COAX CABLES
 MOUNTED ON TOWER LEG



4 TOWER PLAN
 EL-1 SCALE: NOT TO SCALE

1 NORTHEAST ELEVATION
 EL-1 SCALE: NOT TO SCALE



TRUE
 NORTH

REVISIONS		
00	3/25/09	REPORT
01	7/09/09	ISSUED FOR REVIEW

NATCOMM
 CONSULTING ENGINEERS INC.
 p: 203.488.0580 f: 203.488.8587
 w: nat-eng.com e: info@nat-eng.com
 63-2 N. Branford Rd. Branford, CT 06405

NORWALK RT.123
 NU STRUCTURE #1102
 10 WILLRUSS STREET

PROJECT NO: 08174.CO5
 DRAWN BY: TJL
 CHECKED BY: CFC
 SCALE: AS NOTED



TOWER & MAST
 ELEVATION
EL-1



NATCOMM INC.
CONSULTING ENGINEERS

*Structural Analysis of PCS
Mast and CL&P Tower*

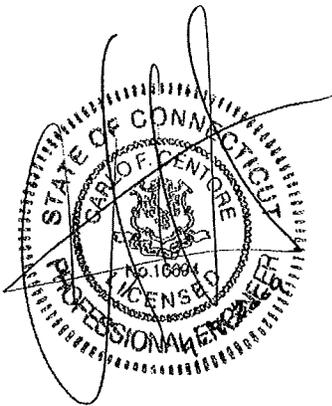
T-Mobile: CT11356-Rt.123

*CL&P Structure No. 1102
94' Electric Transmission Tower
and existing 55' PCS Mast*

*10 Willruss Street,
Norwalk, CT*

Natcomm Project No. 08174.CO.05

*~~Date: April 9, 2009~~
Rev 1: July 9, 2009*



Prepared for:
HPC Development, LLC
53 Lake Ave Ext
Danbury, CT 06811

p: 203.488.0580
f: 203.488.8587
w: nat-eng.com
63-2 N. Branford Rd.
Branford, CT 06405

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Introduction

The purpose of this report is to design a proposed pipe mast and analyze the existing 94' CL&P tower located at 10 Willruss Street Norwalk, CT for the proposed antenna and equipment upgrade by T-Mobile.

The proposed loads consist of the following:

- **T-MOBILE (Existing to be remain):**
Antennas: Three (3) RFS APX16PV-16PVL panel antennas and six (6) TMAs mounted on an existing PCS mast with a RAD center elevation of 114-ft above the tower base plate.
Coax Cables: Twelve (12) 1-1/4" \varnothing coax cables.
- **AT&T (Future):**
Antennas: Three (3) Powerwave 7770 panel antennas and six (6) Powerwave LGP214 TMAs mounted on a proposed PCS mast with a RAD center elevation of 104-ft above grade level.
Coax Cables: Six (6) 1-1/4" \varnothing and three (3) 1/2" \varnothing coax cables.
- **T-MOBILE (Proposed):**
Antennas: Three (3) RFS APX16DWV-16DWVS-C-A20 panel antennas mounted on a proposed PCS mast with a RAD center elevation of 114-ft above grade level.
Coax Cables: Six (6) 1-1/4" \varnothing coax cables.

Primary assumptions used in the analysis

- Allowable steel stresses are defined by AISC-ASD 9th edition for design of the PCS Mast and antenna supporting elements.
- ASCE Manual No. 72, "Design of Steel Transmission Pole Structures Second Edition", defines allowable steel stresses for evaluation of the CL&P utility structure.
- All utility structure members are adequately protected to prevent corrosion of steel members.
- All proposed antenna mounts are modeled as listed above.
- All coaxial cable will be installed within the pipe mast unless specified otherwise.
- Pipe mast will be properly installed and maintained.
- No residual stresses exist due to incorrect pole erection.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds conform to the requirements of AWS D1.1.
- All proposed pipe mast members will be as specified in the construction documents to be prepared by Natcomm, Inc.
- Pipe mast and utility structure will be in plumb condition.
- Utility structure was properly installed and maintained and all members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
- Any deviation from the analyzed loading will require a new analysis for verification of structural adequacy.

A n a l y s i s

Structural analysis of the existing *PCS Mast Structure* was completed using the current version of RISA-3D computer program licensed to Natcomm, Inc.

The proposed pipe mast is a 55' long 12" SCH 80 pipe (dia. = 12.8") attached to the CL&P pole structure at two locations. It was analyzed for its ability to resist loads prescribed by the TIA/EIA standard. Section 5 of this report details these gravity and lateral wind loads. NESC prescribed loads were also applied to the mast structure in order to obtain reactions needed for analyzing the CL&P pole structure. These loads are developed in Section 7 of this report. Load cases and combinations used in RISA-3D for TIA/EIA loading and for NESC/NU loading are listed in report Sections 6 and 8, respectively.

An envelope solution was first made to determine maximum and minimum forces, stresses, and deflections to confirm the selected section as adequate. Additional analyses were then made to determine the NESC forces to be applied to the CL&P pole structure.

The RISA-3D program contains a library of all AISC shapes and corresponding section properties are computed and applied directly within the program. The program's Steel Code Check option was also utilized. The forces calculated in RISA-3D using NESC guidelines were then applied to the CL&P pole using PLS-Pole. Maximum usage for the pole was calculated considering the additional forces from the mast and associated appurtenances.

D e s i g n B a s i s

Our analysis was performed in accordance with EIA-222-F-1996, ASCE Manual No. 72 – "Design of Steel Transmission Pole Structures Second Edition", NESC C2-2007 and Northeast Utilities Design Criteria.

The CL&P pole structure, considering existing and future conductor and shield wire loading, with the proposed antenna mast was analyzed under two conditions:

- **UTILITY POLE ANALYSIS**

The purpose of this analysis is to determine the adequacy of the existing utility pole to support the proposed antenna loads. The loading and design requirements were analyzed in accordance with the NU Design Criteria Table, NESC C2-2007 ~ Construction Grade B, and ASCE Manual No. 72.

Load cases considered:

Load Case 1: NESC Heavy

Wind Pressure.....	4.0 psf
Vertical Overload Capacity Factor.....	1.50
Wind Overload Capacity Factor.....	2.50
Wire Tension Overload Capacity Factor.....	1.65

Load Case 2: NESC Extreme

Wind Speed.....	110 mph ⁽¹⁾
Radial Ice Thickness.....	0"

Note 1: NESC C2-2007, Section 25, Rule 250C: Extreme Wind Loading.
1.25 x Gust Response Factor (wind speed: 3-second gust)

▪ ANTENNA MAST ANALYSIS

The antenna mast pipe, appurtenances and connections to the utility pole were analyzed and designed in accordance with the NU Design Criteria Table, TIA/EIA-222-F, and AISC-ASD standards.

Load cases considered:

Load Case 1:

Wind Speed..... 85 mph ⁽²⁾

Radial Ice Thickness..... 0"

Load Case 2:

Wind Pressure..... 75% of 85 mph wind pressure

Radial Ice Thickness..... 0.5"

| Note 2: Per NU Mast Design Criteria Exception 1.

Results

▪ PIPE MAST

The proposed pipe mast was determined to be structural adequate.

Component	Design Limit	Stress Ratio (percentage of capacity)	Result
12" SCH 80 Pipe (diam = 12.8")	Bending	71.9%	PASS

▪ UTILITY TOWER

This analysis finds that the subject utility tower is adequate to support the proposed antenna mast and related appurtenances. The tower stresses meet the requirements set forth by the ASCE Manual No. 72, "Design of Steel Transmission Pole Structures Second Edition", for the applied NESC Heavy and Extreme load cases. The detailed analysis results are provided in Section 9 of this report. The analysis results are summarized as follows:

A maximum usage of **92.14%** occurs in the utility tower under the NESC Heavy Broken Wire loading condition.

TOWER SECTION:

The utility tower was found to be within allowable limits.

Tower Section	Component	Stress Ratio (percentage of capacity)	Result
156XY	Angle	92.14%	PASS

▪ FOUNDATION AND ANCHORS

The existing foundation consists of a four (4) 6-ft x 6-ft tapering to 3-ft x 3-ft x 9-ft-6-in long reinforced concrete piers with 11-ft x 11-ft x 3-ft thick pads. The base of the tower is connected to the foundation by means of one (1) anchor stub per leg.

Review of the foundation and anchor design consisted of verification of applied loads obtained from the tower design calculations and code check of for uplift:

BASE REACTIONS:

From PLS-Tower analysis of CL&P tower based on NESC/NU prescribed loads.

Load Case	Shear	Compression	Uplift
NESC Heavy Wind	40.14 kips	124.72 kips	66.21 kips
NESC Extreme Wind	41.22 kips	120.03 kips	92.79 kips
NESC Heavy Wind w/ Broken Wire	43.62 kips	129.65 kips	87.42 kips

FOUNDATION:

The foundation factor of safety (FS) was found to be within allowable limits.

Foundation	Design Limit	NU Required (FS) ⁽²⁾	Proposed Loading (FS) ⁽²⁾	Result
Reinf. Conc. Pier w/ Rock Anchors	UL ⁽¹⁾	1.5	3.1	PASS

Note 1: UL denotes uplift.
 Note 2: FS denotes Factor of Safety.

Natcomm, Inc.
Structural Analysis – T-Mobile: CT11356-Rt.123
CL&P Structure No. 1102
Norwalk, CT
Revision 1 ~ July 9, 2009

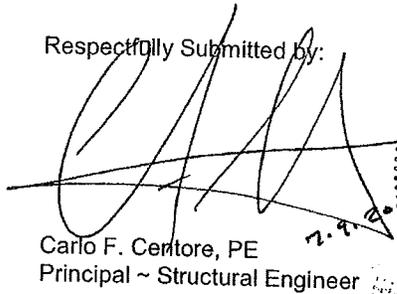
C o n c l u s i o n s

This analysis shows that the subject utility tower is adequate to support the proposed antenna mast and related appurtenances.

The analysis is based, in part on the information provided to this office by Northeast Utilities and T-Mobile. If the existing conditions are different than the information in this report, Natcomm, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:


Carlo F. Centore, PE
Principal ~ Structural Engineer





New Cingular Wireless PCS, LLC
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7636
Fax: (860) 513-7190

Steven L. Levine
Real Estate Consultant

September 1, 2009

Honorable Richard Moccia, Mayor
City of Norwalk
City Hall 125 East Avenue
Norwalk, CT 06856

Re: Notice of Exempt Modification – Existing CL&P Transmission Tower off Willruss Street, Norwalk

Dear Mayor Moccia:

New Cingular Wireless PCS, LLC (“AT&T”) and T-Mobile Northeast LLC (“T-Mobile”) intend to modify telecommunications antennas and associated equipment at an existing telecommunications facility off Willruss Street in Norwalk.

The facility is owned and managed by the Connecticut Light and Power Company (“CL&P”).

A Notice of Exempt Modification has been filed with the Connecticut Siting Council as required by Regulations of Connecticut State Agencies (“R.C.S.A.”) Section 16-50j-73. Please accept this letter as notification to the City of Norwalk under Section 16-50j-73 of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2).

The attached letter fully sets forth the AT&T and T-Mobile proposal. However, if you have any questions or require any further information on the plans for the site or the Siting Council’s procedures, please contact Mr. Tim Burks at 860-080-0001 (AT&T), Ms. Jennifer Young Gaudet (T-Mobile), or Mr. Derek Phelps, Executive Director of the Connecticut Siting Council, at (860) 827-2935.

Sincerely,

Steve Levine
Real Estate Consultant

Enclosure


NATCOMM INC.
CONSULTING ENGINEERS ●

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CONNECTICUT
SITING COUNCIL

*Structural Analysis of PCS
Mast and CL&P Tower*

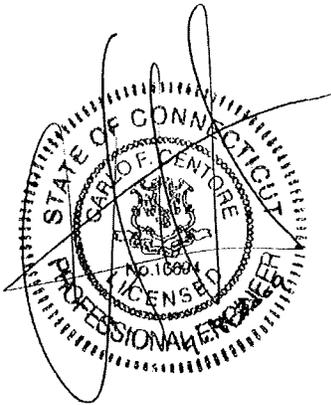
T-Mobile: CT11356-Rt.123

*CL&P Structure No. 1102
94' Electric Transmission Tower
and existing 55' PCS Mast*

*10 Willruss Street,
Norwalk, CT*

Natcomm Project No. 08174.CO.05

*~~Date: April 9, 2009~~
Rev 1: July 9, 2009*



Prepared for:
HPC Development, LLC
53 Lake Ave Ext
Danbury, CT 06811

p: 203.488.0580
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63-2 N. Branford Rd.
Branford, CT 06405

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Introduction

The purpose of this report is to design a proposed pipe mast and analyze the existing 94' CL&P tower located at 10 Willruss Street Norwalk, CT for the proposed antenna and equipment upgrade by T-Mobile.

The proposed loads consist of the following:

- **T-MOBILE (Existing to be remain):**
Antennas: Three (3) RFS APX16PV-16PVL panel antennas and six (6) TMAs mounted on an existing PCS mast with a RAD center elevation of 114-ft above the tower base plate.
Coax Cables: Twelve (12) 1-1/4" \varnothing coax cables.
- **AT&T (Future):**
Antennas: Three (3) Powerwave 7770 panel antennas and six (6) Powerwave LGP214 TMAs mounted on a proposed PCS mast with a RAD center elevation of 104-ft above grade level.
Coax Cables: Six (6) 1-1/4" \varnothing and three (3) 1/2" \varnothing coax cables.
- **T-MOBILE (Proposed):**
Antennas: Three (3) RFS APX16DWV-16DWVS-C-A20 panel antennas mounted on a proposed PCS mast with a RAD center elevation of 114-ft above grade level.
Coax Cables: Six (6) 1-1/4" \varnothing coax cables.

Primary assumptions used in the analysis

- Allowable steel stresses are defined by AISC-ASD 9th edition for design of the PCS Mast and antenna supporting elements.
- ASCE Manual No. 72, "Design of Steel Transmission Pole Structures Second Edition", defines allowable steel stresses for evaluation of the CL&P utility structure.
- All utility structure members are adequately protected to prevent corrosion of steel members.
- All proposed antenna mounts are modeled as listed above.
- All coaxial cable will be installed within the pipe mast unless specified otherwise.
- Pipe mast will be properly installed and maintained.
- No residual stresses exist due to incorrect pole erection.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds conform to the requirements of AWS D1.1.
- All proposed pipe mast members will be as specified in the construction documents to be prepared by Natcomm, Inc.
- Pipe mast and utility structure will be in plumb condition.
- Utility structure was properly installed and maintained and all members were properly designed, detailed, fabricated, and installed and have been properly maintained since erection.
- Any deviation from the analyzed loading will require a new analysis for verification of structural adequacy.

A n a l y s i s

Structural analysis of the existing *PCS Mast Structure* was completed using the current version of RISA-3D computer program licensed to Natcomm, Inc.

The proposed pipe mast is a 55' long 12" SCH 80 pipe (dia. = 12.8") attached to the CL&P pole structure at two locations. It was analyzed for its ability to resist loads prescribed by the TIA/EIA standard. Section 5 of this report details these gravity and lateral wind loads. NESC prescribed loads were also applied to the mast structure in order to obtain reactions needed for analyzing the CL&P pole structure. These loads are developed in Section 7 of this report. Load cases and combinations used in RISA-3D for TIA/EIA loading and for NESC/NU loading are listed in report Sections 6 and 8, respectively.

An envelope solution was first made to determine maximum and minimum forces, stresses, and deflections to confirm the selected section as adequate. Additional analyses were then made to determine the NESC forces to be applied to the CL&P pole structure.

The RISA-3D program contains a library of all AISC shapes and corresponding section properties are computed and applied directly within the program. The program's Steel Code Check option was also utilized. The forces calculated in RISA-3D using NESC guidelines were then applied to the CL&P pole using PLS-Pole. Maximum usage for the pole was calculated considering the additional forces from the mast and associated appurtenances.

D e s i g n B a s i s

Our analysis was performed in accordance with EIA-222-F-1996, ASCE Manual No. 72 – "Design of Steel Transmission Pole Structures Second Edition", NESC C2-2007 and Northeast Utilities Design Criteria.

The CL&P pole structure, considering existing and future conductor and shield wire loading, with the proposed antenna mast was analyzed under two conditions:

- UTILITY POLE ANALYSIS

The purpose of this analysis is to determine the adequacy of the existing utility pole to support the proposed antenna loads. The loading and design requirements were analyzed in accordance with the NU Design Criteria Table, NESC C2-2007 ~ Construction Grade B, and ASCE Manual No. 72.

Load cases considered:

Load Case 1: NESC Heavy

Wind Pressure.....	4.0 psf
Vertical Overload Capacity Factor.....	1.50
Wind Overload Capacity Factor.....	2.50
Wire Tension Overload Capacity Factor.....	1.65

Load Case 2: NESC Extreme

Wind Speed.....	110 mph ⁽¹⁾
Radial Ice Thickness.....	0"

Note 1: NESC C2-2007, Section 25, Rule 250C: Extreme Wind Loading,
1.25 x Gust Response Factor (wind speed: 3-second gust)

▪ ANTENNA MAST ANALYSIS

The antenna mast pipe, appurtenances and connections to the utility pole were analyzed and designed in accordance with the NU Design Criteria Table, TIA/EIA-222-F, and AISC-ASD standards.

Load cases considered:

Load Case 1:

Wind Speed..... 85 mph ⁽²⁾
 Radial Ice Thickness..... 0"

Load Case 2:

Wind Pressure..... 75% of 85 mph wind pressure
 Radial Ice Thickness..... 0.5"

| Note 2: Per NU Mast Design Criteria Exception 1.

Results

▪ PIPE MAST

The proposed pipe mast was determined to be structural adequate.

Component	Design Limit	Stress Ratio (percentage of capacity)	Result
12" SCH 80 Pipe (diam = 12.8")	Bending	71.9%	PASS

▪ UTILITY TOWER

This analysis finds that the subject utility tower is adequate to support the proposed antenna mast and related appurtenances. The tower stresses meet the requirements set forth by the ASCE Manual No. 72, "Design of Steel Transmission Pole Structures Second Edition", for the applied NESC Heavy and Extreme load cases. The detailed analysis results are provided in Section 9 of this report. The analysis results are summarized as follows:

A maximum usage of **92.14%** occurs in the utility tower under the NESC Heavy Broken Wire loading condition.

TOWER SECTION:

The utility tower was found to be within allowable limits.

Tower Section	Component	Stress Ratio (percentage of capacity)	Result
156XY	Angle	92.14%	PASS

▪ FOUNDATION AND ANCHORS

The existing foundation consists of a four (4) 6-ft x 6-ft tapering to 3-ft x 3-ft x 9-ft-6-in long reinforced concrete piers with 11-ft x 11-ft x 3-ft thick pads. The base of the tower is connected to the foundation by means of one (1) anchor stub per leg.

Review of the foundation and anchor design consisted of verification of applied loads obtained from the tower design calculations and code check of for uplift:

BASE REACTIONS:

From PLS-Tower analysis of CL&P tower based on NESC/NU prescribed loads.

Load Case	Shear	Compression	Uplift
NESC Heavy Wind	40.14 kips	124.72 kips	66.21 kips
NESC Extreme Wind	41.22 kips	120.03 kips	92.79 kips
NESC Heavy Wind w/ Broken Wire	43.62 kips	129.65 kips	87.42 kips

FOUNDATION:

The foundation factor of safety (FS) was found to be within allowable limits.

Foundation	Design Limit	NU Required (FS) ⁽²⁾	Proposed Loading (FS) ⁽²⁾	Result
Reinf. Conc. Pier w/ Rock Anchors	UL ⁽¹⁾	1.5	3.1	PASS

Note 1: UL denotes uplift.

Note 2: FS denotes Factor of Safety.

Natcomm, Inc.
Structural Analysis – T-Mobile: CT11356-Rt.123
CL&P Structure No. 1102
Norwalk, CT
Revision 1 ~ July 9, 2009

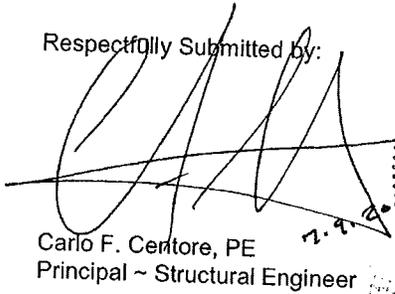
C o n c l u s i o n s

This analysis shows that the subject utility tower **is adequate** to support the proposed antenna mast and related appurtenances.

The analysis is based, in part on the information provided to this office by Northeast Utilities and T-Mobile. If the existing conditions are different than the information in this report, Natcomm, Inc. must be contacted for resolution of any potential issues.

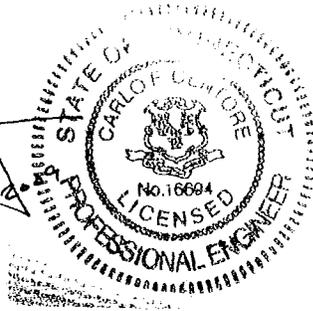
Please feel free to call with any questions or comments.

Respectfully Submitted by:



2.9

Carlo F. Centore, PE
Principal ~ Structural Engineer



Natcomm, Inc.
Structural Analysis – T-Mobile: CT11356-Rt.123
CL&P Structure No. 1102
Norwalk, CT
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STANDARD CONDITIONS FOR FURNISHING OF
PROFESSIONAL ENGINEERING SERVICES ON
EXISTING STRUCTURES

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Natcomm, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Natcomm, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the "as new" condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222.
- All services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. Natcomm, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM ~ RISA - 3 D

RISA-3D Structural Analysis Program is an integrated structural analysis and design software package for buildings, bridges, tower structures, etc.

Modeling Features:

- Comprehensive CAD-like graphic drawing/editing capabilities that let you draw, modify and load elements as well as snap, move, rotate, copy, mirror, scale, split, merge, mesh, delete, apply, etc.
- Versatile drawing grids (orthogonal, radial, skewed)
- Universal snaps and object snaps allow drawing without grids
- Versatile general truss generator
- Powerful graphic select/unselect tools including box, line, polygon, invert, criteria, spreadsheet selection, with locking
- Saved selections to quickly recall desired selections
- Modification tools that modify single items or entire selections
- Real spreadsheets with cut, paste, fill, math, sort, find, etc.
- Dynamic synchronization between spreadsheets and views so you can edit or view any data in the plotted views or in the spreadsheets
- Simultaneous view of multiple spreadsheets
- Constant in-stream error checking and data validation
- Unlimited undo/redo capability
- Generation templates for grids, disks, cylinders, cones, arcs, trusses, tanks, hydrostatic loads, etc.
- Support for all units systems & conversions at any time
- Automatic interaction with RISASection libraries
- Import DXF, RISA-2D, STAAD and ProSteel 3D files
- Export DXF, SDNF and ProSteel 3D files

Analysis Features:

- Static analysis and P-Delta effects
- Multiple simultaneous dynamic and response spectra analysis using Gupta, CQC or SRSS mode combinations
- Automatic inclusion of mass offset (5% or user defined) for dynamic analysis
- Physical member modeling that does not require members to be broken up at intermediate joints
- State of the art 3 or 4 node plate/shell elements
- High-end automatic mesh generation — draw a polygon with any number of sides to create a mesh of well-formed quadrilateral (NOT triangular) elements.
- Accurate analysis of tapered wide flanges - web, top and bottom flanges may all taper independently
- Automatic rigid diaphragm modeling
- Area loads with one-way or two-way distributions
- Multiple simultaneous moving loads with standard AASHTO loads and custom moving loads for bridges, cranes, etc.
- Torsional warping calculations for stiffness, stress and design
- Automatic Top of Member offset modeling
- Member end releases & rigid end offsets
- Joint master-slave assignments
- Joints detachable from diaphragms
- Enforced joint displacements
- 1-Way members, for tension only bracing, slipping, etc.

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Structural Analysis – T-Mobile: CT11356-Rt.123
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- 1-Way springs, for modeling soils and other effects
- Euler members that take compression up to their buckling load, then turn off.
- Stress calculations on any arbitrary shape
- Inactive members, plates, and diaphragms allows you to quickly remove parts of structures from consideration
- Story drift calculations provide relative drift and ratio to height
- Automatic self-weight calculations for members and plates
- Automatic subgrade soil spring generator

Graphics Features:

- Unlimited simultaneous model view windows
- Extraordinary “true to scale” rendering, even when drawing
- High-speed redraw algorithm for instant refreshing
- Dynamic scrolling stops right where you want
- Plot & print virtually everything with color coding & labeling
- Rotate, zoom, pan, scroll and snap views
- Saved views to quickly restore frequent or desired views
- Full render or wire-frame animations of deflected model and dynamic mode shapes with frame and speed control
- Animation of moving loads with speed control
- High quality customizable graphics printing

Design Features:

- Designs concrete, hot rolled steel, cold formed steel and wood
- ACI 1999/2002, BS 8110-97, CSA A23.3-94, IS456:2000, EC 2-1992 with consistent bar sizes through adjacent spans
- Exact integration of concrete stress distributions using parabolic or rectangular stress blocks
- Concrete beam detailing (Rectangular, T and L)
- Concrete column interaction diagrams
- Steel Design Codes: AISC ASD 9th, LRFD 2nd & 3rd, HSS Specification, CAN/CSA-S16.1-1994 & 2004, BS 5950-1-2000, IS 800-1984, Euro 3-1993 including local shape databases
- AISI 1999 cold formed steel design
- NDS 1991/1997/2001 wood design, including Structural Composite Lumber, multi-ply, full sawn
- Automatic spectra generation for UBC 1997, IBC 2000/2003
- Generation of load combinations: ASCE, UBC, IBC, BOCA, SBC, ACI
- Unbraced lengths for physical members that recognize connecting elements and full lengths of members
- Automatic approximation of K factors
- Tapered wide flange design with either ASD or LRFD codes
- Optimization of member sizes for all materials and all design codes, controlled by standard or user-defined lists of available sizes and criteria such as maximum depths
- Automatic calculation of custom shape properties
- Steel Shapes: AISC, HSS, CAN, ARBED, British, Euro, Indian, Chilean
- Light Gage Shapes: AISI, SSMA, Dale / Incor, Dietrich, Marino\WARE
- Wood Shapes: Complete NDS species/grade database
- Full seamless integration with RISAFoot (Ver 2 or better) for advanced footing design and detailing
- Plate force summation tool

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Results Features:

- Graphic presentation of color-coded results and plotted designs
- Color contours of plate stresses and forces with quadratic smoothing, the contours may also be animated
- Spreadsheet results with sorting and filtering of: reactions, member & joint deflections, beam & plate forces/stresses, optimized sizes, code designs, concrete reinforcing, material takeoffs, frequencies and mode shapes
- Standard and user-defined reports
- Graphic member detail reports with force/stress/deflection diagrams and detailed design calculations and expanded diagrams that display magnitudes at any dialed location
- Saved solutions quickly restore analysis and design results.

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Norwalk, CT
Revision 1 ~ July 9, 2009

GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM ~ PLS-TOWER

PLS-TOWER is a Microsoft Windows program for the analysis and design of steel latticed towers used in electric power lines or communication facilities. Both self-supporting and guyed towers can be modeled. The program performs design checks of structures under user specified loads. For electric power structures it can also calculate maximum allowable wind and weight spans and interaction diagrams between different ratios of allowable wind and weight spans.

Modeling Features:

- Powerful graphics module (stress usages shown in different colors)
- Graphical selection of joints and members allows graphical editing and checking
- Towers can be shown as lines, wire frames or can be rendered as 3-d polygon surfaces
- Can extract geometry and connectivity information from a DXF CAD drawing
- CAD design drawings, title blocks, drawing borders or photos can be tied to structure model
- XML based post processor interface
- Steel Detailing Neutral File (SDNF) export to link with detailing packages
- Can link directly to line design program PLS-CADD
- Automatic generation of structure files for PLS-CADD
- Databases of steel angles, rounds, bolts, guys, etc.
- Automatic generation of joints and members by symmetries and interpolations
- Automated mast generation (quickly builds model for towers that have regular repeating sections) via graphical copy/paste
- Steel angles and rounds modeled either as truss, beam or tension-only elements
- Guys are easily handled (can be modeled as exact cable elements)

Analysis Features:

- Automatic handling of tension-only members
- Automatic distribution of loads in 2-part suspension insulators (v-strings, horizontal vees, etc.)
- Automatic calculation of tower dead, ice, and wind loads as well as drag coefficients according to:
 - ASCE 74-1991
 - NESC 2002
 - NESC 2007
 - IEC 60826:2003
 - EN50341-1:2001 (CENELEC)
 - EN50341-3-9:2001 (UK NNA)
 - EN50341-3-17:2001 (Portugal NNA)
 - ESAA C(b)1-2003 (Australia)
 - TPNZ (New Zealand)
 - REE (Spain)
 - EIA/TIA 222-F
 - ANSI/TIA 222-G
 - CSA S37-01
- Automated microwave antenna loading as per EIA/TIA 222-F and ANSI/TIA 222-G
- Minimization of problems caused by unstable joints and mechanisms
- Automatic bandwidth minimization and ability to solve large problems
- Design checks according to (other standards can be added easily):
 - ASCE Standard 10-90

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Structural Analysis – T-Mobile: CT11356-Rt.123
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- AS 3995 (Australian Standard 3995)
- BS 8100 (British Standard 8100)
- EN50341-1 (CENELEC, both empirical and analytical methods are available)
- ECCS 1985
- NGT-ECCS
- PN-90/B-03200
- EIA/TIA 222-F
- ANSI/TIA 222-G
- CSA S37-01
- EDF/RTE Resal
- IS 802 (India Standard 802)

Results Features:

- Design summaries printed for each group of members
- Easy to interpret text, spreadsheet and graphics design summaries
- Automatic determination of allowable wind and weight spans
- Automatic determination of interaction diagrams between allowable wind and weight spans
- Capability to batch run multiple tower configurations and consolidate the results
- Automated optimum angle member size selection and bolt quantity determination
- Tool for interactive angle member sizing and bolt quantity determination

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Norwalk, CT
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Criteria for Design of PCS Facilities On or
Extending Above Metal Electric Transmission
Towers & Analysis of Transmission Towers
Supporting PCS Masts ⁽¹⁾

Introduction

This criteria is the result from an evaluation of the methods and loadings specified by the separate standards, which are used in designing telecommunications towers and electric transmission towers. That evaluation is detailed elsewhere, but in summary; the methods and loadings are significantly different. This criteria specifies the manner in which the appropriate standard is used to design PCS facilities including masts and brackets (hereafter referred to as "masts"), and to evaluate the electric transmission towers to support PCS masts. The intent is to achieve an equivalent level of safety and security under the extreme design conditions expected in Connecticut and Massachusetts.

ANSI Standard TIA/EIA-222 covering the design of telecommunications structures specifies a working strength/allowable stress design approach. This approach applies the loads from extreme weather loading conditions, and designs the structure so that it does not exceed some defined percentage of failure strength (allowable stress).

ANSI Standard C2-2002 (National Electrical Safety Code) covering the design of electric transmission metal structures is based upon an ultimate strength/yield stress design approach. This approach applies a multiplier (overload capacity factor) to the loads possible from extreme weather loading conditions, and designs the structure so that it does not exceed its ultimate strength (yield stress).

Each standard defines the details of how loads are to be calculated differently. Most of the NU effort in "unifying" both codes was to establish what level of strength each approach would provide, and then increasing the appropriate elements of each to achieve a similar level of security under extreme weather loadings.

Two extreme weather conditions are considered. The first is an extreme wind condition (hurricane) based upon a 50-year recurrence (2% annual probability). The second is a winter condition combining wind and ice loadings.

The following sections describe the design criteria for any PCS mast extending above the top of an electric transmission tower, and the analysis criteria for evaluating the loads on the transmission tower from such a mast from the lower portions of such a mast, and loads on the pre-existing electric lower portions of such a mast, and loads on the pre-existing electric transmission tower and the conductors it supports.

Note 1: Prepared from documentation provided from Northeast Utilities.

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Structural Analysis – T-Mobile: CT11356-Rt.123
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PCS Mast

The PCS facility (mast, external cable/trays, including the initial and any planned future support platforms, antennas, etc. extending the full height above the top level of the electric transmission structure) shall be designed in accordance with the provisions of TIA/EIA Standard 222 with two exceptions:

1. An 85 mph extreme wind speed shall be used for locations in all counties throughout the NU system.
2. The stress increase of TIA Section 3.1.1.1 is disallowed. The combined wind and ice condition shall consider ½" radial ice in combination with the wind load (0.75 Wi) as specified in TIA section 2.3.16.

ELECTRIC TRANSMISSION TOWER

The electric transmission tower shall be analyzed using yield stress theory in accordance with the attached table titled "NU Design Criteria". This specifies uniform loadings (different from the TIA loadings) on the each of the following components of the installed facility:

- PCS mast for its total height above ground level, including the initial and planned future support platforms, antennas, etc. above the top of an electric transmission structure.
- Conductors are related devices and hardware.
- Electric transmission structure. The loads from the PCS facility and from the electric conductors shall be applied to the structure at conductor and PCS mast attachment points, where those load transfer to the tower.

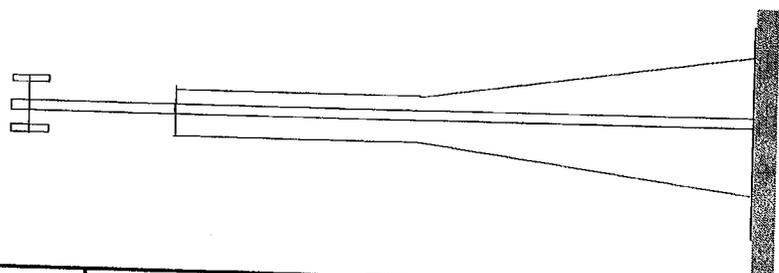
The uniform loadings and factors specified for the above components in the table are based upon the National Electrical Safety Code 2002 Edition Extreme Wind (Rule 250C) and Combined Ice and Wind (Rule 250B-Heavy) Loadings. These provide equivalent loadings compared to TIA and its loads and factors with the exceptions noted above. (Note that the NESC does not require the projected wind surfaces of structures and equipment to be increased by the ice covering.)

In the event that the electric transmission tower is not sufficient to support the additional loadings of the PCS mast, reinforcement will be necessary to upgrade the strength of the overstressed members.

NU DESIGN CRITERIA TABLE

	Basic Wind Speed		Pressure		Height Factor		Gust Factor		Load or Stress Factor		Force Coef - Shape Factor	
	V (mph)	q (psf)	Kz	Gh	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA
EXTREME WIND (50-YR) PCS Mast, etc. Design (Allowable stress)	85	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA
Tower/Pole Analysis (Yield stress) PCS above tower/pole-top	Use NES C2-2007, Section 25, Rule 250C: Extreme Wind Loading 1.25 x Gust Response Factor Height above groundline based on top of mast/antenna											
Tower/Pole & PCS below tower/pole-top	Use NES C2-2007, Section 25, Rule 250C: Extreme Wind Loading Height above groundline based on top of tower/pole											
Conductors Only for structures installed 2007 and after	Use NES C2-2007, Section 25, Rule 250C: Extreme Wind Loading, and Use NES C2-2007, Section 25, Rule 250D; Combined Extreme Ice and Wind											
NESC HEAVY PCS Design (Allowable stress)	TIA	TIA (.75Wi)	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA	TIA
Tower/Pole Analysis (Yield stress) PCS above tower/pole-top	4	4	1.00	1.00	1.00	1.00	1.00	2.50	2.50	1.60 flat surfaces 1.30 round surfaces	1.60 flat surfaces 1.30 round surfaces	1.00
Tower (on each of 2 faces)/pole and PCS below tower-top	4	4	1.00	1.00	1.00	1.00	1.00	2.50	2.50	1.60 flat surfaces 1.30 round surfaces	1.60 flat surfaces 1.30 round surfaces	1.00
Conductors Wind Horizontal comp. of tension Vertical weight w/ 1/2" ice	4	4	1.00	1.00	1.00	1.00	1.00	2.50	2.50	1.65	1.50	1.00

rev 12/19/07



**Northeast Utilities/ Western Massachusetts Electric Co.
Transmission Structure Shape factor Criteria Supporting PCS
Antennas (Issued April 12, 2007)**

The shape factor Multiplier.

- Flat member $Cd = 1.6$:
- Round Member $Cd=1.3$

Where the coax cables are mounted along side of the pole structure the shape factor multiplier shall be as follows:

- Coax cables attached on outside periphery of the pole in one layer $Cd=1.45$ to the pole and the coax.
- Coax cables mounted on stand off, use $Cd=1.6$ for coax cables and $Cd=1.3$ for pole



Mohsen Sahirad, P.E.
Transmission Civil Engineer



Job : AT&T Norwalk, CT-5046
 Description:

Spec. Number
 Computed by
 Checked by

Page of
 Sheet of
 Date 7/21/08
 Date

INPUT DATA

TOWER ID: 1102

Structure Height (ft) : 94

Wind Zone : Central CT (green)

Wind Speed : 110 mph

Tower Type : Suspension
 Strain

Extreme Wind Model : PCS Addition

Shield Wire Properties:

	BACK	AHEAD
NAME =	0.438 COMP	0.438 COMP
DESCRIPTION =	0.438	0.438
STRANDING =	9/3 Cu/Cal Brz	9/3 Cu/Cal Brz
DIAMETER =	0.438 in	0.438 in
WEIGHT =	0.408 lb/ft	0.408 lb/ft

Conductor Properties:

		BACK	AHEAD		
Number of Conductors per phase	NAME =	TERN	TERN	1	Number of Conductors per phase
		795.000	795.000		
		45/7 ACSR	45/7 ACSR		
	DIAMETER =	1.063 in	1.063 in		
	WEIGHT =	0.895 lb/ft	0.895 lb/ft		

Insulator Weight = 200 lbs

Broken Wire Side = AHEAD SPAN

Horizontal Line Tensions:

	BACK		AHEAD	
	Shield	Conductor	Shield	Conductor
NESC HEAVY =	3,800	7,000	3,800	7,000
EXTREME WIND =	3,140	7,568	3,140	7,568
LONG. WIND =	na	na	na	na
250D COMBINED =	na	na	na	na
NESC W/O OLF =	na	na	na	na
60 DEG F NO WIND =	1,412	2,734	1,412	2,734

Line Geometry:

	BACK:		AHEAD:		SUM
LINE ANGLE (deg) =		13		13	26
WIND SPAN (ft) =		409		409	818
WEIGHT SPAN (ft) =		415		415	830



Job : AT&T Norwalk, CT-5046

Description:

Spec. Number

Computed by

Checked by

Page of

Sheet of

Date 7/21/08

Date

WIRE LOADING AT ATTACHMENTS

TOWER ID: 1102

Wind Span =	818 ft
Weight Span =	830 ft
Total Angle =	26 degrees

Broken Wire Span =	AHEAD SPAN
Type of Insulator Attachment =	STRAIN

1. NESC RULE 250B Heavy Loading:

	INTACT CONDITION			BROKEN WIRE CONDITION		
	Horizontal	Longitudinal	Vertical	Horizontal	Longitudinal	Vertical
Shield Wire =	3,810 lb	0 lb	1,234 lb	1,905 lb	6,108 lb	617 lb
Conductor =	6,618 lb	0 lb	2,924 lb	3,309 lb	11,252 lb	1,462 lb

2. NESC RULE 250C Transverse Extreme Wind Loading:

	Horizontal	Longitudinal	Vertical
Shield Wire =	2,270 lb	0 lb	339 lb
Conductor =	5,486 lb	0 lb	1,143 lb

3. NESC RULE 250C Longitudinal Extreme Wind Loading:

	Horizontal	Longitudinal	Vertical
Shield Wire =	#VALUE!	#VALUE!	339 lb
Conductor =	#VALUE!	#VALUE!	1,143 lb

4. NESC RULE 250D Extreme Ice & Wind Loading:

	Horizontal	Longitudinal	Vertical
Shield Wire =	#VALUE!	#VALUE!	1,823 lb
Conductor =	#VALUE!	#VALUE!	3,272 lb

5. NESC RULE 250B w/o OLF's

	Horizontal	Longitudinal	Vertical
Shield Wire =	#VALUE!	#VALUE!	823 lb
Conductor =	#VALUE!	#VALUE!	1,949 lb

6. 60 Deg. F, No Wind

	Horizontal	Longitudinal	Vertical
Shield Wire =	637 lb	0 lb	339 lb
Conductor =	1,234 lb	0 lb	1,143 lb

7. Construction

	Horizontal	Longitudinal	Vertical
Shield Wire =	956 lb	0 lb	508 lb
Conductor =	1,851 lb	0 lb	1,714 lb

NOTE: All loads include required overload factors (OLF's).



Job : AT&T Norwalk, CT-5046
Description:

Spec. Number
Computed by
Checked by

Page of
Sheet of
Date 7/21/08
Date

INPUT DATA

TOWER ID: 1102

Structure Height (ft) : 94

Wind Zone : Central CT (green)

Wind Speed : 110 mph

Tower Type : Suspension
 Strain

Extreme Wind Model : PCS Addition

Shield Wire Properties:

	BACK	AHEAD
NAME =	OPGW-120 ✓	OPGW-120 ✓
DESCRIPTION =	6-Groove	6-Groove
STRANDING =	10/9 FOCAS	10/9 FOCAS
DIAMETER =	0.738 in	0.738 in
WEIGHT =	0.518 lb/ft	0.518 lb/ft

Conductor Properties:

		BACK	AHEAD		
Number of Conductors per phase	NAME =	NONE	NONE	Number of Conductors per phase	
	1	-	-	1	
		--	--		
	DIAMETER =	0.000 in	0.000 in		
	WEIGHT =	0.000 lb/ft	0.000 lb/ft		

Insulator Weight = 200 lbs

Broken Wire Side = AHEAD SPAN

Horizontal Line Tensions:

	BACK		AHEAD	
	Shield	Conductor	Shield	Conductor
NESC HEAVY =	6,000*	na	6,000✓	na
EXTREME WIND =	7,760✓	na	7,760✓	na
LONG. WIND =	na	na	na	na
250D COMBINED =	na	na	na	na
NESC W/O OLF =	na	na	na	na
60 DEG F NO WIND =	2,076✓	na	2,076✓	na

Line Geometry:

					SUM
LINE ANGLE (deg) =	BACK:	13	AHEAD:	13	26
WIND SPAN (ft) =	BACK:	409	AHEAD:	409	818
WEIGHT SPAN (ft) =	BACK:	415	AHEAD:	415	830



Job : AT&T Norwalk, CT-5046
 Description:

Spec. Number
 Computed by
 Checked by

Page of
 Sheet of
 Date 7/21/08
 Date

WIRE LOADING AT ATTACHMENTS

TOWER ID: 1102

Wind Span = 818 ft
 Weight Span = 830 ft
 Total Angle = 26 degrees

Broken Wire Span = AHEAD SPAN
 Type of Insulator Attachment = STRAIN

1. NESC RULE 250B Heavy Loading:

	INTACT CONDITION			BROKEN WIRE CONDITION		
	Horizontal	Longitudinal	Vertical	Horizontal	Longitudinal	Vertical
Shield Wire =	5,652 lb	0 lb	1,603 lb	2,826 lb	9,645 lb	802 lb
Conductor =	#VALUE!	#VALUE!	987 lb	#VALUE!	#VALUE!	494 lb

2. NESC RULE 250C Transverse Extreme Wind Loading:

	Horizontal	Longitudinal	Vertical
Shield Wire =	4,939 lb	0 lb	430 lb
Conductor =	#VALUE!	#VALUE!	400 lb

3. NESC RULE 250C Longitudinal Extreme Wind Loading:

	Horizontal	Longitudinal	Vertical
Shield Wire =	#VALUE!	#VALUE!	430 lb
Conductor =	#VALUE!	#VALUE!	400 lb

4. NESC RULE 250D Extreme Ice & Wind Loading:

	Horizontal	Longitudinal	Vertical
Shield Wire =	#VALUE!	#VALUE!	2,224 lb
Conductor =	#VALUE!	#VALUE!	1,432 lb

5. NESC RULE 250B w/o OLF's

	Horizontal	Longitudinal	Vertical
Shield Wire =	#VALUE!	#VALUE!	1,069 lb
Conductor =	#VALUE!	#VALUE!	658 lb

6. 60 Deg. F. No Wind

	Horizontal	Longitudinal	Vertical
Shield Wire =	937 lb	0 lb	430 lb
Conductor =	#VALUE!	#VALUE!	400 lb

7. Construction

	Horizontal	Longitudinal	Vertical
Shield Wire =	1,405 lb	0 lb	645 lb
Conductor =	#VALUE!	#VALUE!	600 lb

NOTE: All loads include required overload factors (OLF's).

(3) RFS APX16PV-16PVL
PANEL ANTENNA AND (6)
POWERWAVE LGP214 TMS

(3) RFS APX16DWV-
16DWVS-A20
PANEL ANTENNAS

☉ T-MOBILE ANTENNAS
EL. ±114'-0" AGL

☉ T-MOBILE ANTENNAS
EL. ±114'-0" AGL

UNIVERSAL SNAP-IN BRACKET FOR
ANGLE LEG, VALMONT-MICROFLECT
(P/N B2249). w/ VALMONT
SNAP-IN HANGER (P/N B1562)
@ 4'-0" o.c. VERTICAL MAX

(3) POWERWAVE 7770
PANEL ANTENNAS AND (6)
POWERWAVE LGP214 TMS

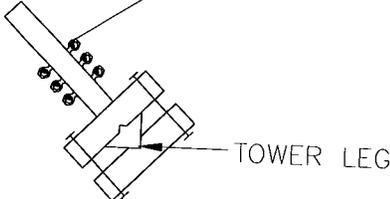
☉ AT&T ANTENNAS
EL. ±104'-0" AGL

TOP EXISTING NU TOWER
±94'-0" AGL

☉ TOP CONNECTION
EL. ±83'-6" AGL

PROPOSED 12" DIA.
SCH.80 PIPE MAST

☉ BOTTOM CONNECTION
EL. ±62'-0" AGL

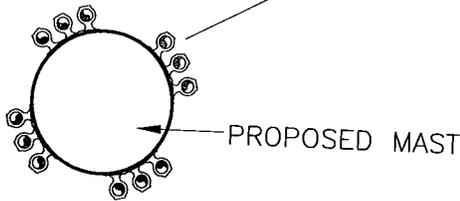


TOWER LEG

2 COAX MOUNTING PLAN

EL-1 NOT TO SCALE

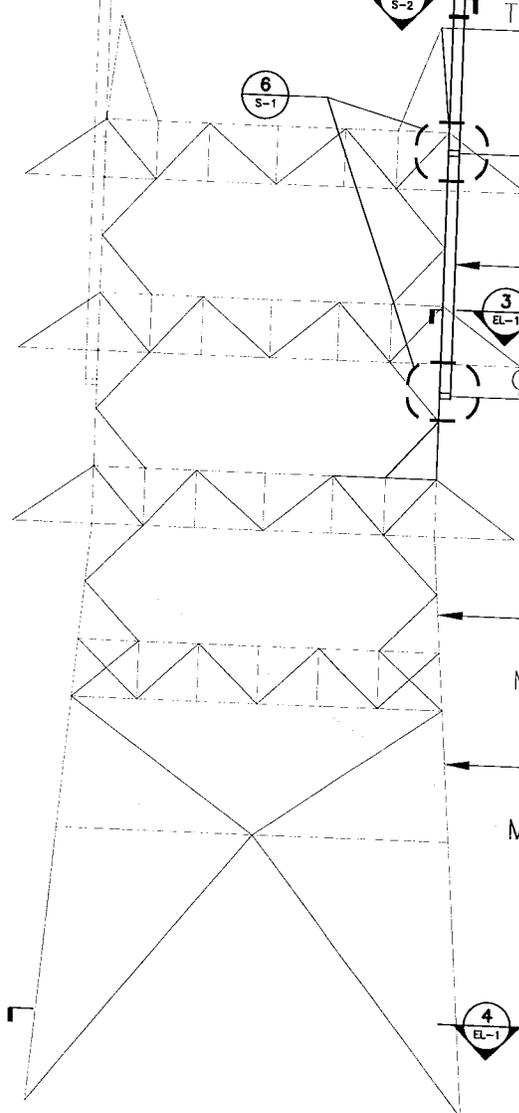
(12) 1-1/4" DIA. COAX CABLES
MOUNTED TO PROPOSED PIPE
MAST @ 4'-0" o.c. VERTICAL MAX.
w/ VALMONT SNAP-IN HANGER
(P/N B1562), MONOPOLE
TRANSMISSION LINE BRACKET (P/N
B3254), STAINLESS STEEL
BANDING (P/N B1769) AND
BUCKLES (P/N B1770)



PROPOSED MAST

3 COAX MOUNTING PLAN

EL-1 NOT TO SCALE

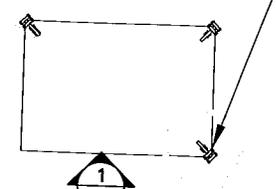


1 NORTHEAST ELEVATION

EL-1 SCALE: NOT TO SCALE

EXISTING (6) 1-1/4"
DIA. COAX CABLES
MOUNTED ON TOWER LEG

PROPOSED (6) 1-1/4"
DIA. COAX CABLES
MOUNTED ON TOWER LEG



1 EL-1

4 TOWER PLAN

EL-1 SCALE: NOT TO SCALE



TRUE
NORTH

REVISIONS		
00	3/25/09	REPORT
01	7/09/09	ISSUED FOR REVIEW

NATCOMM
CONSULTING ENGINEERS

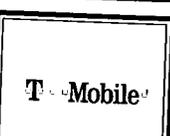
p: 203.488.0580 f: 203.488.8587
w: nat-eng.com e: info@nat-eng.com
63-2 N. Branford Rd. Branford, CT 06405

NORWALK RT.123
NU STRUCTURE #1102

10 WILLRUSS STREET

PROJECT NO: 08174.CO5

DRAWN BY: TJL
CHECKED BY: CFC
SCALE: AS NOTED



TOWER & MAST
ELEVATION

EL-1

REV	DATE	BY	CHKD	DESCRIPTION

DESIGNED BY:
DRAWN BY:
CHK'D BY:

PROFESSIONAL ENGINEER SEAL

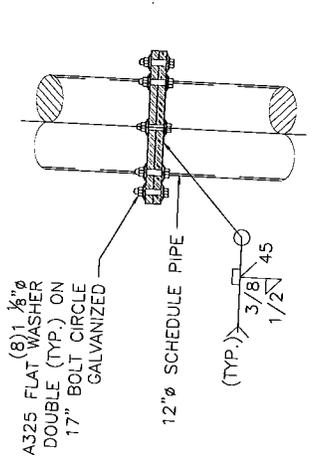
INTECOMM
111 W. PARK ST. SUITE 100
NORWALK, CT 06854
SP - Mobile

1 MOBILE PCS MAST INSTALLATION
NORWALK
CT-1-356
CL&P STRUCTURE #1102
10 WILLIAMS STREET
NORWALK, CT 06854

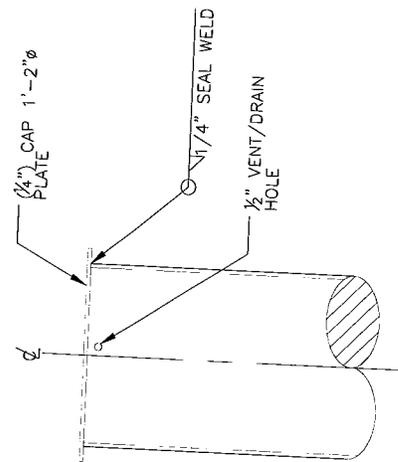
DATE: 7/02/99
SCALE: AS SHOWN
JOB NO. 08174.005

FLANGE CONNECTION
DETAILS

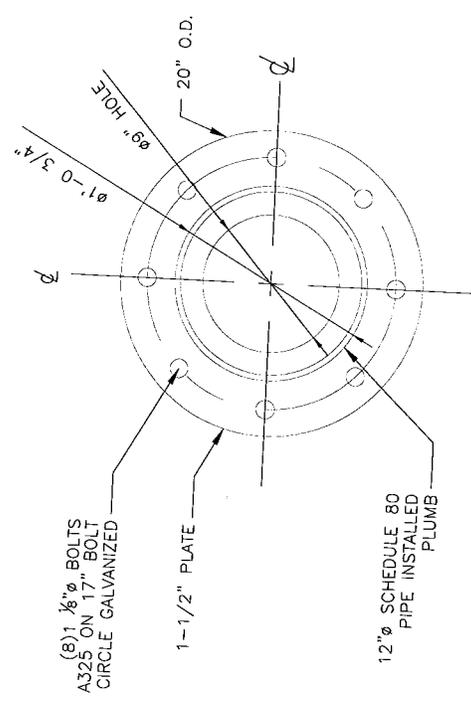
SHEET NO. S-2
Sheet No. 2 of 3



2 MAST FLANGE CONNECTION
SCALE: 3/4" = 1'-0"



3 TOP COVER PLATE
SCALE: 1 1/2" = 1'-0"



1 MAST FLANGE CONNECTION PLAN
SCALE: 1 1/2" = 1'-0"

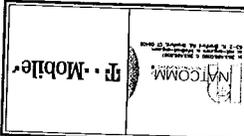
GENERAL NOTES:

1. ALL WORK SHALL BE IN ACCORDANCE WITH TIA/EIA-222 REVISION "E", "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES", ASCE MANUAL NO. 72 - "DESIGN OF STEEL TRANSMISSION POLE STRUCTURES SECOND EDITION", NESC C2-2002 AND NORTHEAST UTILITIES DESIGN CRITERIA.
2. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURE AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY TO MAINTAIN EXISTING SITE OPERATIONS, COORDINATE WORK WITH NORTHEAST UTILITIES.
3. DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
4. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA.
5. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
6. NO DRILLING, TAPPING OR WELDING ON CL&P OWNED EQUIPMENT

STRUCTURAL STEEL NOTES:

1. ALL STRUCTURAL STEEL IS DESIGNED BY ALLOWABLE STRESS DESIGN (ASD).
 - A. STRUCTURAL STEEL (W SHAPES)---ASTM A992, (FY = 50 KSI)
 - B. STRUCTURAL STEEL (OTHER SHAPES)---ASTM A36, (FY = 36 KSI)
 - C. STRUCTURAL HSS (RECTANGULAR SHAPES)---ASTM A500 GRADE B, (FY = 46 KSI)
 - D. STRUCTURAL HSS (ROUND SHAPES)---ASTM A500 GRADE B, (FY = 42 KSI)
 - C. CONNECTION BOLTS---ASTM A325-N
 - E. ANCHOR RODS---ASTM F 1554
 - E. WELDING ELECTRODE---ASTM E 70XX
 2. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE ENGINEER FOR REVIEW. SHOP DRAWINGS SHALL INCLUDE THE FOLLOWING: SECTION PROFILES, SIZES, CONNECTION ATTACHMENTS, REINFORCING, ANCHORAGE SIZE AND TYPE OF FASTENERS AND ACCESSORIES INCLUDE ERECTION DRAWINGS, ELEVATIONS AND DETAILS.
 3. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH THE LATEST PROVISIONS OF AISC MANUAL OF STEEL CONSTRUCTION.
 4. PROVIDE ALL PLATES, CLIP ANGLES, CLOSURE PIECES, STRAP ANCHORS, MISCELLANEOUS PIECES AND HOLES, REQUIRED TO COMPLETE THE STRUCTURE.
 5. FIT AND SHOP ASSEMBLE FABRICATIONS IN THE LARGEST PRACTICAL SECTIONS FOR DELIVERY TO SITE.
 6. INSTALL FABRICATIONS PLUMB AND LEVEL, ACCURATELY FITTED, AND FREE FROM DISTORTIONS OR DEFECTS.
 7. NOTIFY THE ENGINEER PRIOR TO FIELD CUTTING OR MODIFYING APPROVED FABRICATIONS.
 8. AFTER ERECTION OF STRUCTURES, TOUCHUP ALL WELDS, ABRASIONS AND NON-GALVANIZED SURFACES WITH A 95% ORGANIC ZINC RICH PAINT IN ACCORDANCE WITH ASTM 780.
 9. ALL STEEL MATERIAL (EXPOSED TO WEATHER) SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT DIPPED GALVANIZED) COATINGS" ON IRONS AND STEEL PRODUCTS.
 10. ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC COATING (HOT-DIP) ON IRON AND STEEL HARDWARE".
11. CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES APPEARANCE AND QUALITY OF WELDS, AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS "STANDARD QUALIFICATION PROCEDURES", ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND D1.1 WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "MANUAL OF STEEL CONSTRUCTION" 9TH EDITION, AT THE COMPLETION OF WELDING, ALL DAMAGE TO GALVANIZED COATING SHALL BE REPAIRED.
 12. THE ENGINEER SHALL BE NOTIFIED OF ANY INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON CONFORMING MATERIALS OR CONDITIONS TO REMEDY OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER REVIEW.
 13. STRUCTURAL CONNECTION BOLTS SHALL CONFORM TO ASTM A325 WITH NUTS AND PAL NUTS. ALL BOLTS TO BE TENSIONED IN ACCORDANCE WITH TABLE 4 OF THE AISC SPECIFICATION FOR STRUCTURAL JOINTS USING ASTM A325 OR A490 BOLTS.
 14. SHOP CONNECTIONS SHALL BE WELDED OR HIGH STRENGTH BOLTED.
 15. MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO TRANSFER LOAD OVER ENTIRE CROSS SECTION.
 16. LEVEL AND PLUMB INDIVIDUAL MEMBERS OF THE STRUCTURE TO AN ACCURACY OF 1:500, BUT NOT TO EXCEED 1/4" IN THE FULL HEIGHT OF THE COLUMN.
 17. COMMENCEMENT OF STRUCTURAL STEEL WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK.
 18. INSPECTION AND TESTING OF ALL WELDING AND HIGH STRENGTH BOLTING SHALL BE PERFORMED BY AN INDEPENDENT TESTING LABORATORY. THE INSPECTOR SHALL OBSERVE INSTALLATION OF BOLTS AND TEST WITH A CALIBRATED TORQUE WRENCH NOT LESS THAN 20% OF THE BOLTS AND NOT LESS THAN TWO BOLTS, SELECTED AT RANDOM, IN EACH CONNECTION.
 19. FOUR COPIES OF ALL INSPECTION TEST REPORTS SHALL BE SUBMITTED TO THE ENGINEER WITHIN TEN (10) WORKING DAYS OF THE DATE OF INSPECTION.

REV.	DATE	BY	DESCRIPTION	ISSUED FOR REVIEW
00	02/09/09	KAL	CFC	
01		KAYAN BR		
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T MOBILE PCS MAST INSTALLATION
NORWALK
CT-11-356
CL&P STRUCTURE #1102
DATE: 7/07/09
SCALE: AS SHOWN
JOB NO.: 08174.005

STRUCTURAL SPECIFICATIONS

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

**Development of Design Heights, Exposure Coefficients,
and Velocity Pressures Per TIA/EIA**

Wind Speeds

Basic Wind Speed, V
Basic Wind Speed with Ice, V_i

$V := 85$ mph (per NU Mast Design Criteria Exception 1)
 $V_i := 74$ mph (per TIA/EIA-222-F Section 2.3.16)

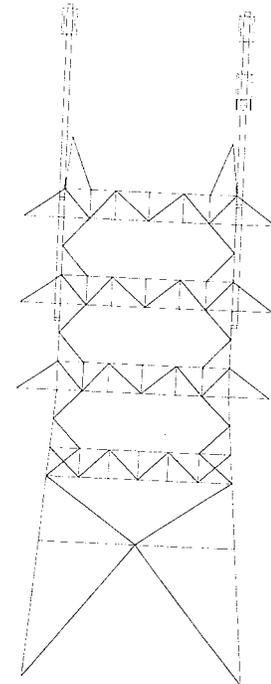
Heights above ground level, z

Mast, z_{mast} $z_{mast} := 90.0$ ft
Antenna, z_{ant} $z_{ant} := 104.0$ ft
Antenna2, z_{ant2} $z_{ant2} := 114.0$ ft
TMA, z_{TMA} $z_{TMA} := 104.0$ ft
Mount, z_{mnt} $z_{mnt} := 104.0$ ft
Mount2, z_{mnt2} $z_{mnt2} := 114.0$ ft
Coax Cable, z_{coax} $z_{coax} := 90.0$ ft

Exposure Coefficients, k_z

(per TIA/EIA-222-F Section 2.3.3)

Mast, $k_{z_{mast}}$ $k_{z_{mast}} := \left(\frac{z_{mast}}{33} \right)^{\frac{2}{7}} = 1.332$
Antenna, $k_{z_{ant}}$ $k_{z_{ant}} := \left(\frac{z_{ant}}{33} \right)^{\frac{2}{7}} = 1.388$
Antenna2, $k_{z_{ant2}}$ $k_{z_{ant2}} := \left(\frac{z_{ant2}}{33} \right)^{\frac{2}{7}} = 1.425$
TMA, $k_{z_{TMA}}$ $k_{z_{TMA}} := \left(\frac{z_{TMA}}{33} \right)^{\frac{2}{7}} = 1.388$
Mount, $k_{z_{mnt}}$ $k_{z_{mnt}} := \left(\frac{z_{mnt}}{33} \right)^{\frac{2}{7}} = 1.388$
Mount2, $k_{z_{mnt2}}$ $k_{z_{mnt2}} := \left(\frac{z_{mnt2}}{33} \right)^{\frac{2}{7}} = 1.425$
Coax Cable, $k_{z_{coax}}$ $k_{z_{coax}} := \left(\frac{z_{coax}}{33} \right)^{\frac{2}{7}} = 1.332$



Subject:

Location:

Rev. 1: 7/7/09

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Norwalk, CT

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

Velocity Pressure without ice, qz

(per TIA/EIA-222-F Section 2.3.3)

Mast, qz _{mast}	$qz_{mast} := 0.00256 \cdot Kz_{mast} \cdot V^2 = 24.636$
Antenna, qz _{ant}	$qz_{ant} := 0.00256 \cdot Kz_{ant} \cdot V^2 = 25.675$
Antenna2, qz _{ant2}	$qz_{ant2} := 0.00256 \cdot Kz_{ant2} \cdot V^2 = 26.357$
TMA, qz _{TMA}	$qz_{TMA} := 0.00256 \cdot Kz_{TMA} \cdot V^2 = 25.675$
Mount, qz _{mnt}	$qz_{mnt} := 0.00256 \cdot Kz_{mnt} \cdot V^2 = 25.675$
Mount2, qz _{mnt2}	$qz_{mnt2} := 0.00256 \cdot Kz_{mnt2} \cdot V^2 = 26.357$
Coax Cable, qz _{coax}	$qz_{coax} := 0.00256 \cdot Kz_{coax} \cdot V^2 = 24.636$

Velocity Pressure with ice, qzICE

(per TIA/EIA-222-F Section 2.3.3)

Mast, qzICE _{mast}	$qzICE_{mast} := 0.00256 \cdot Kz_{mast} \cdot V_i^2 = 18.672$
Antenna, qzICE _{ant}	$qzICE_{ant} := 0.00256 \cdot Kz_{ant} \cdot V_i^2 = 19.46$
Antenna2, qzICE _{ant2}	$qzICE_{ant2} := 0.00256 \cdot Kz_{ant2} \cdot V_i^2 = 19.977$
TMA, qzICE _{TMA}	$qzICE_{TMA} := 0.00256 \cdot Kz_{TMA} \cdot V_i^2 = 19.46$
Mount, qzICE _{mnt}	$qzICE_{mnt} := 0.00256 \cdot Kz_{mnt} \cdot V_i^2 = 19.46$
Mount2 qzICE _{mnt2}	$qzICE_{mnt2} := 0.00256 \cdot Kz_{mnt2} \cdot V_i^2 = 19.977$
Coax Cable, qzICE _{coax}	$qzICE_{coax} := 0.00256 \cdot Kz_{coax} \cdot V_i^2 = 18.672$

TIA/EIA Common Factors:

Gust Response Factor =	$G_H := 1.69$	(per TIA/EIA-222-F Section 2.3.4)
Gust Response Factor Multiplier =	$m := 1.25$	(per TIA/EIA-222-F Section 2.3.4.4)
Radial Ice Thickness =	$Ir := 0.50$	in (per TIA/EIA-222-F Section 2.3.1)
Radial Ice Density =	$Id := 56.00$	pcf

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

Development of Wind & Ice Load on PCS Mast

(per TIA/EIA-222-F-1996 Criteria)

PCS Mast Data:

Mast Shape =	Round
Mast Diameter =	$D_{mast} := 12.8$ in (Pipe 12" SCH. 80)
Mast Length =	$L_{mast} := 55$ ft
Mast Thickness =	$t_{mast} := 0.5$ in
Mast Aspect Ratio =	$A_{r_{mast}} := \frac{12L_{mast}}{D_{mast}} = 51.6$
Mast Force Coefficient =	$C_{a_{mast}} = 1.2$ (per TIA/EIA-222-F Table 3)
Velocity Coefficient =	$C := \left(\sqrt{K_{z_{mast}}} \right) \cdot V \cdot \frac{D_{mast}}{12} = 104.639$
Structure Force Coefficient =	$C_{F_{mast}} = 0.59$ (per TIA/EIA-222-F Table 1 for round pole)

Wind Load (without ice)

(per TIA/EIA-222-F-1996 Section 2.3.2)

*Assumes Mast is Shielded by Coax Cable
Antennas and TMAs Top 32' of Mast*

Mast Projected Surface Area =	$A_{mast} := \frac{D_{mast}}{12} = 1.067$ sq ft/ft
Total Mast Wind Force =	$qZ_{mast} \cdot G_H \cdot C_{F_{mast}} \cdot C_{a_{mast}} \cdot A_{mast} = 31$ plf BLC 5

Wind Load (with ice)

(per TIA/EIA-222-F-1996 Section 2.3.2)

*Assumes Mast is Shielded by Coax Cable
Antennas and TMAs Top 32' of Mast*

Mast Projected Surface Area w/ Ice =	$A_{ICE_{mast}} := \frac{(D_{mast} + 2 \cdot I_r)}{12} = 1.15$ sq ft/ft
Total Mast Wind Force w/ Ice =	$qz_{ICE_{mast}} \cdot G_H \cdot C_{F_{mast}} \cdot C_{a_{mast}} \cdot A_{ICE_{mast}} = 26$ plf BLC 4

Gravity Loads (without ice)

Weight of the mast =	Self Weight (Computed internally by Risa-3D) plf BLC 1
----------------------	---

Gravity Loads (ice only)

Ice Area per Linear Foot =	$A_{i_{mast}} := \frac{\pi}{4} \left[(D_{mast} + I_r \cdot 2)^2 - D_{mast}^2 \right] = 20.9$ sq in
----------------------------	---

Weight of Ice on Mast =	$W_{ICE_{mast}} := I_d \cdot \frac{A_{i_{mast}}}{144} = 8$ plf BLC 3
-------------------------	---



Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

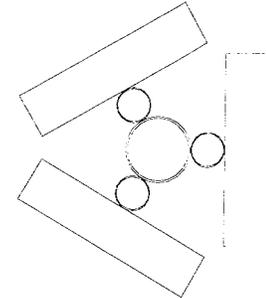
Development of Wind & Ice Load on Antennas

(per TIA/EIA-222-F-1996 Criteria)

Antenna Data:

(AT&T @ 104')

Antenna Model =	Powerwave 7770
Antenna Shape =	Flat
Antenna Height =	$L_{ant} := 55$ in
Antenna Width =	$W_{ant} := 11$ in
Antenna Thickness =	$T_{ant} := 5$ in
Antenna Weight =	$WT_{ant} := 35$ lbs
Number of Antennas =	$N_{ant} := 3$
Antenna Aspect Ratio =	$Ar_{ant} := \frac{L_{ant}}{W_{ant}} = 5.0$
Antenna Force Coefficient =	$Ca_{ant} = 1.4$



(per TIA/EIA-222-F-1996 Table 3)

Wind Load (without ice)

(per TIA/EIA-222-F-1996 Section 2.3.2)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna =	$SA_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 4.2$	sf
Antenna Projected Surface Area =	$A_{ant} := SA_{ant} \cdot N_{ant} = 12.6$	sf
Total Antenna Wind Force =	$F_{ant} := qz_{ant} \cdot G_H \cdot Ca_{ant} \cdot A_{ant} = 766$	lbs BLC 5

Wind Load (with ice)

(per TIA/EIA-222-F-1996 Section 2.3.2)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna w/ Ice =	$SA_{ICEant} := \frac{(L_{ant} + 1) \cdot (W_{ant} + 1)}{144} = 4.7$	sf
Antenna Projected Surface Area w/ Ice =	$A_{ICEant} := SA_{ICEant} \cdot N_{ant} = 14$	sf
Total Antenna Wind Force w/ Ice =	$F_{ICEant} := qz_{ICEant} \cdot G_H \cdot Ca_{ant} \cdot A_{ICEant} = 645$	lbs BLC 4

Gravity Load (without ice)

Weight of All Antennas =	$WT_{ant} \cdot N_{ant} = 105$	lbs BLC 2
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Gravity Load (ice only)

Volume of Each Antenna =	$V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 3025$	cu in
Volume of Ice on Each Antenna =	$V_{ice} := (L_{ant} + 1) \cdot (W_{ant} + 1) \cdot (T_{ant} + 1) - V_{ant} = 1007$	cu in
Weight of Ice on Each Antenna =	$W_{ICEant} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 33$	lbs
Weight of Ice on All Antennas =	$W_{ICEant} \cdot N_{ant} = 98$	lbs BLC 3

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

Development of Wind & Ice Load on Antennas

Antenna Data:

Antenna Model =
Antenna Shape =
Antenna Height =
Antenna Width =
Antenna Thickness =
Antenna Weight =
Number of Antennas =
Antenna Aspect Ratio =
Antenna Force Coefficient =

(per TIA/EIA-222-F-1996 Criteria)

(T-Mobile @ 114')

RFS APX16DWV-16DWVS-C-A20

Flat

$$L_{ant2} := 55.9 \text{ in}$$

$$W_{ant2} := 13.3 \text{ in}$$

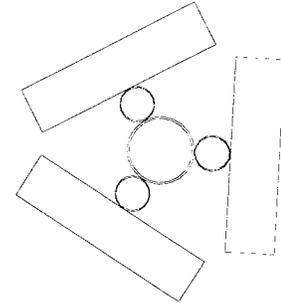
$$T_{ant2} := 3.15 \text{ in}$$

$$WT_{ant2} := 40.7 \text{ lbs}$$

$$N_{ant2} := 3$$

$$Ar_{ant2} := \frac{L_{ant2}}{W_{ant2}} = 4.2$$

$$Ca_{ant2} = 1.4$$



(per TIA/EIA-222-F-1996 Table 3)

Wind Load (without ice)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna =

$$SA_{ant2} := \frac{L_{ant2} \cdot W_{ant2}}{144} = 5.2 \text{ sf}$$

Antenna Projected Surface Area =

$$A_{ant2} := SA_{ant2} \cdot N_{ant2} = 15.5 \text{ sf}$$

Total Antenna Wind Force =

$$F_{ant2} := qz_{ant2} \cdot G_H \cdot Ca_{ant2} \cdot A_{ant2} = 966 \text{ lbs} \quad \text{BLC 5}$$

(per TIA/EIA-222-F-1996 Section 2.3.2)

Wind Load (with ice)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna w/ Ice =

$$SA_{ICEant2} := \frac{(L_{ant2} + 1) \cdot (W_{ant2} + 1)}{144} = 5.7 \text{ sf}$$

Antenna Projected Surface Area w/ Ice =

$$A_{ICEant2} := SA_{ICEant2} \cdot N_{ant2} = 17 \text{ sf}$$

Total Antenna Wind Force w/ Ice =

$$F_{ICEant2} := qz_{ICEant2} \cdot G_H \cdot Ca_{ant2} \cdot A_{ICEant2} = 801 \text{ lbs} \quad \text{BLC 4}$$

Gravity Load (without ice)

Weight of All Antennas =

$$WT_{ant2} \cdot N_{ant2} = 122 \text{ lbs} \quad \text{BLC 2}$$

Gravity Load (ice only)

Volume of Each Antenna =

$$V_{ant2} := L_{ant2} \cdot W_{ant2} \cdot T_{ant2} = 2342 \text{ cu in}$$

Volume of Ice on Each Antenna =

$$V_{ice} := (L_{ant2} + 1) \cdot (W_{ant2} + 1) \cdot (T_{ant2} + 1) - V_{ant2} = 1035 \text{ cu in}$$

Weight of Ice on Each Antenna =

$$W_{ICEant2} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 34 \text{ lbs}$$

Weight of Ice on All Antennas =

$$W_{ICEant2} \cdot N_{ant2} = 101 \text{ lbs} \quad \text{BLC 3}$$

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

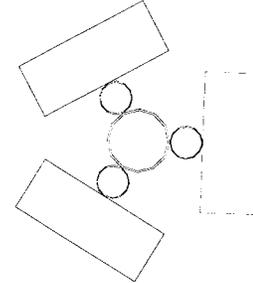
Development of Wind & Ice Load on TMA's

(per TIA/EIA-222-F-1996 Criteria)

TMA Data:

(AT&T @ 104')

TMA Model = Powerwave LGP214
 TMA Shape = Flat
 TMA Height = $L_{TMA} := 9.2$ in
 TMA Width = $W_{TMA} := 14.4$ in
 TMA Thickness = $T_{TMA} := 2.6$ in
 TMA Weight = $W_{TMA} := 14.1$ lbs
 Number of TMA's = $N_{TMA} := 6$
 TMA Aspect Ratio = $A_{rTMA} := \frac{L_{TMA}}{W_{TMA}} = 0.6$
 TMA Force Coefficient = $C_{aTMA} = 1.4$



(per TIA/EIA-222-F Table 3)

Wind Load (without ice)

(per TIA/EIA-222-F-1996 Section 2.3.2)

Assumes Maximum Possible Wind Pressure on TMA's

Surface Area for One TMA = $SA_{TMA} := \frac{L_{TMA} \cdot W_{TMA}}{144} = 0.9$ sf
 TMA Projected Surface Area = $A_{TMA} := SA_{TMA} \cdot N_{TMA} = 5.5$ sf
 Total TMA Wind Force = $F_{TMA} := qz_{TMA} \cdot G_H \cdot C_{aTMA} \cdot A_{TMA} = 335$ lbs **BLC 5**

Wind Load (with ice)

(per TIA/EIA-222-F-1996 Section 2.3.2)

Assumes Maximum Possible Wind Pressure on TMA's

Surface Area for One TMA w/ Ice = $SA_{ICETMA} := \frac{(L_{TMA} + 1) \cdot (W_{TMA} + 1)}{144} = 1.1$ sf
 TMA Projected Surface Area w/ Ice = $A_{ICETMA} := SA_{ICETMA} \cdot N_{TMA} = 6.5$ sf
 Total TMA Wind Force w/ Ice = $F_{iTMA} := qz_{ICE_{TMA}} \cdot G_H \cdot C_{aTMA} \cdot A_{ICETMA} = 301$ lbs **BLC 4**

Gravity Load (without ice):

$W_{TMA} \cdot N_{TMA} = 85$ lbs **BLC 2**

Weight of All TMA's =

Gravity Load (with ice)

$V_{TMA} := L_{TMA} \cdot W_{TMA} \cdot T_{TMA} = 344$ cu in

Volume of Each TMA =

$V_{ice} := (L_{TMA} + 1) \cdot (W_{TMA} + 1) \cdot (T_{TMA} + 1) - V_{TMA} = 221$ cu in

Volume of Ice on Each TMA =

$W_{ICETMA} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 7$ lbs

Weight of Ice on Each TMA =

$W_{ICETMA} \cdot N_{TMA} = 43$ lbs **BLC 3**

Weight of Ice on All TMA's

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

Development of Wind & Ice Load on Antenna Mounts

Mount Data:

Mount Type =
Mount Shape =
Pipe Mount Length =
2 inch Pipe Mount Linear Weight =
Pipe Mount Outside Diameter =
Number of Mounting Pipes =
Tri Sector Adapter Mount Weight =
Mount Aspect Ratio =
Mount Force Coefficient =

(per TIA/EIA-222-F-1996 Criteria)

(AT&T @ 104')

Microflex Tri-Sector Adapter
Mountw/ 3 Pipes

Round

$$L_{mnt} := 66 \quad \text{in}$$

$$W_{mnt} := 3.66 \quad \text{plf}$$

$$D_{mnt} := 2.375 \quad \text{in}$$

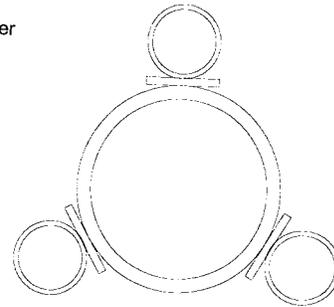
$$N_{mnt} := 3$$

$$W_{tsa.mnt} := 20 \quad \text{lbs}$$

$$Ar_{mnt} := \frac{L_{mnt}}{D_{mnt}} = 28$$

$$Ca_{mnt} = 1.2$$

(per TIA/EIA-222-F Table 3)



(per TIA/EIA-222-F-1996 Section 2.3.2)

Wind Load (without ice)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area =

$$A_{mnt} := 0.0$$

sf

Total Mount Wind Force =

$$F_{mnt} := qz_{mnt} \cdot G_H \cdot Ca_{mnt} \cdot A_{mnt} = 0$$

lbs **BLC 5**

Wind Load (with ice)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area w/ Ice =

$$A_{ICEmnt} := 0.0$$

sf

Total Mount Wind Force =

$$F_{imnt} := qz_{ICE} \cdot G_H \cdot Ca_{mnt} \cdot A_{ICEmnt} = 0$$

lbs **BLC 4**

Gravity Loads (without ice)

Weight Each Pipe Mount =

$$WT_{mnt} := W_{mnt} \cdot \frac{L_{mnt}}{12} = 20$$

lbs

Weight of All Mounts =

$$WT_{mnt} \cdot N_{mnt} + W_{tsa.mnt} = 80$$

lbs **BLC 2**

Gravity Loads (ice only)

Volume of Each Pipe =

$$V_{mnt} := \frac{\pi}{4} \cdot D_{mnt}^2 \cdot L_{mnt} = 292$$

cu in

Volume of Ice on Each Pipe =

$$V_{ice} := \left[\frac{\pi}{4} \cdot \left[(D_{mnt} + 1)^2 \right] \cdot (L_{mnt} + 1) \right] - V_{mnt} = 307$$

cu in

Weight of Ice each mount (incl, hardware) =

$$W_{ICEmnt} := \frac{V_{ice}}{1728} \cdot \rho_d = 10$$

lbs

Weight of Ice on All Mounts =

$$W_{ICEmnt} \cdot N_{mnt} + 5 = 35$$

lbs **BLC 3**

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

Development of Wind & Ice Load on Antenna Mounts

Mount Data:

Mount Type =
Mount Shape =
Pipe Mount Length =
2 inch Pipe Mount Linear Weight =
Pipe Mount Outside Diameter =
Number of Mounting Pipes =
Tri Sector Adapter Mount Weight =
Mount Aspect Ratio =
Mount Force Coefficient =

(per TIA/EIA-222-F-1996 Criteria)

(T-Mobile @ 114')

Microflex Tri-Sector Adapter
Mountw/ 3 Pipes

Round

$$L_{mnt2} := 66 \text{ in}$$

$$W_{mnt2} := 3.66 \text{ plf}$$

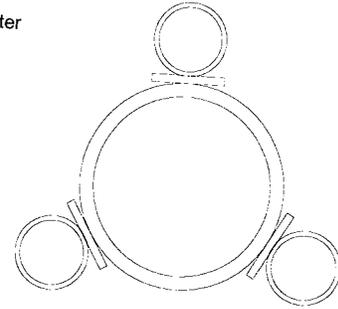
$$D_{mnt2} := 2.375 \text{ in}$$

$$N_{mnt2} := 3$$

$$W_{tsa.mnt2} := 20 \text{ lbs}$$

$$A_{r.mnt2} := \frac{L_{mnt2}}{D_{mnt2}} = 28$$

$$C_{a.mnt2} = 1.2$$



(per TIA/EIA-222-F Table 3)

(per TIA/EIA-222-F-1996 Section 2.3.2)

Wind Load (without ice)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area =

$$A_{mnt2} := 0.0$$

sf

Total Mount Wind Force =

$$F_{mnt2} := q_{z.mnt2} \cdot G_H \cdot C_{a.mnt2} \cdot A_{mnt2} = 0$$

lbs **BLC 5**

Wind Load (with ice)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area w/ Ice =

$$A_{ICEmnt2} := 0.0$$

sf

Total Mount Wind Force =

$$F_{i.mnt2} := q_{zICE.mnt2} \cdot G_H \cdot C_{a.mnt2} \cdot A_{ICEmnt2} = 0$$

lbs **BLC 4**

Gravity Loads (without ice)

Weight Each Pipe Mount =

(per TIA/EIA-222-F-1996)

$$W_{T.mnt2} := W_{mnt2} \cdot \frac{L_{mnt2}}{12} = 20$$

lbs

Weight of All Mounts =

$$W_{T.mnt2} \cdot N_{mnt2} + W_{tsa.mnt2} = 80$$

lbs **BLC 2**

Gravity Loads (Ice only)

Volume of Each Pipe =

$$V_{mnt2} := \frac{\pi}{4} \cdot D_{mnt2}^2 \cdot L_{mnt2} = 292$$

cu in

Volume of Ice on Each Pipe =

$$V_{ice} := \left[\frac{\pi}{4} \cdot (D_{mnt2} + 1)^2 \cdot (L_{mnt2} + 1) \right] - V_{mnt2} = 307$$

cu in

Weight of Ice each mount (incl. hardware) =

$$W_{ICEmnt2} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 10$$

lbs

Weight of Ice on All Mounts =

$$W_{ICEmnt2} \cdot N_{mnt2} + 5 = 35$$

lbs **BLC 3**

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174-CO.5

Development of Wind & Ice Load on Coax Cables

Coax Cable Data:

Shape =
Coax Type =
Coax Outside Diameter =
Weight of Coax per foot =
Total Number of Coax =
No. of Coax Projecting Outside Face of PCS Mast =
Coax Type =
Coax Outside Diameter =
Weight of Coax per foot =
Total Number of Coax =
No. of Coax Projecting Outside Face of PCS Mast =
Coax Cable Length =
Coax aspect ratio,
Coax Cable Force Factor Coefficient =

per TIA/EIA-222-F-96 Criteria

(T-Mobile & AT&T)

Round

HELIX 1-1/4" Φ

$D_{\text{coax1}} := 1.55$ in

$Wt_{\text{coax1}} := 0.66$ plf

$N_{\text{coax1}} := 12$ (6 T-Mobile & 6 AT&T)

$NP_{\text{coax1}} := 2$

HELIX 1/2" Φ

$D_{\text{coax2}} := 0.58$ in

$Wt_{\text{coax2}} := 0.25$ plf

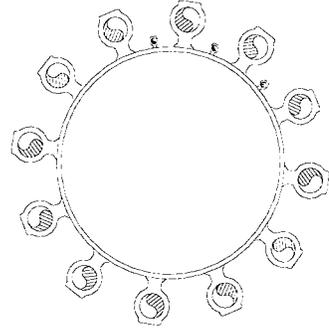
$N_{\text{coax2}} := 3$ (3 AT&T RET Cables)

$NP_{\text{coax2}} := 0$

$L_{\text{coax}} := 21$ ft

$$Ar_{\text{coax}} := \frac{(L_{\text{coax}} \cdot 12)}{D_{\text{coax1}}} = 162.6$$

$Ca_{\text{coax}} = 1.2$ TIA/EIA-222-F-96 Table 3



Wind Load (without ice)

Coax projected surface area =
Total Coax Wind Force =

per TIA/EIA-222-F-96 Section 2.3.2

$$A_{\text{coax}} := \frac{(NP_{\text{coax1}} \cdot D_{\text{coax1}} + D_{\text{mast}})}{12} = 1.3 \quad \text{sq ft/ft}$$

$$F_{\text{coax}} := Ca_{\text{coax}} \cdot qz_{\text{coax}} \cdot G_H \cdot A_{\text{coax}} = 66 \quad \text{plf} \quad \text{BLC 5}$$

Wind Load (with ice)

Coax projected surface area w/ Ice =
Total Coax Wind Force w/ Ice =

per TIA/EIA-222-F-96 Section 2.3.2

$$A_{\text{ICE}_{\text{coax}}} := \frac{(NP_{\text{coax1}} \cdot D_{\text{coax1}} + D_{\text{mast}} + 2 \cdot lr)}{12} = 1.4 \quad \text{sq ft/ft}$$

$$F_{\text{ICE}_{\text{coax}}} := Ca_{\text{coax}} \cdot qz_{\text{ICE}_{\text{coax}}} \cdot G_H \cdot A_{\text{ICE}_{\text{coax}}} = 53 \quad \text{plf} \quad \text{BLC 4}$$

Gravity Loads (without ice)

Weight of all cables w/o ice

$$WT_{\text{coax}} := Wt_{\text{coax1}} \cdot N_{\text{coax1}} + Wt_{\text{coax2}} \cdot N_{\text{coax2}} = 9 \quad \text{plf} \quad \text{BLC 2}$$

Gravity Loads (ice only)

Ice Area per Linear Foot =

$$A_{\text{ice}_{\text{coax}}} := \frac{\pi}{4} \left[(D_{\text{coax1}} + 2 \cdot lr)^2 - D_{\text{coax1}}^2 \right] = 3.2 \quad \text{sq in}$$

Ice Weight All Coax per foot =

$$WT_{\text{ice}_{\text{coax}}} := N_{\text{coax1}} \cdot Id \cdot \frac{A_{\text{ice}_{\text{coax}}}}{144} = 15 \quad \text{plf} \quad \text{BLC 3}$$

NATCOMM, INC.
Consulting Engineers
 63-2 North Branford Road
 Branford, CT 06405

Ph. 203-488-0580 / Fax. 203-488-8587

Subject: **Analysis of TIA/EIA Wind and Ice Loads for Design of
 PCS Mast Only
 Tabulated Load Cases**

Location: **Norwalk, CT**

Date: 3/23/09 Prepared by: T.J.L. Checked by: C.F.C. Job No. 08174.CO5

Load Case	Description
1	Self Weight (PCS Mast)
2	Weight of PCS Structure ⁽¹⁾ (no Ice)
3	Weight of Ice Only on PCS Mast + PCS Structure
4	TIA/EIA Wind with Ice on PCS Mast + PCS Structure
5	TIA/EIA Wind on PCS Mast + PCS Structure

Footnotes:
 (1) PCS Structure includes: Antennas, TMA's, Mounts, Coax Cable

NATCOMM, INC.
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 63-2 North Branford Road
 Branford, CT 06405
 Ph. 203-488-0580 / Fax. 203-488-8587

Subject: **Analysis of TIA/EIA Wind and Ice Loads for Design of PCS Mast Only**
 Load Combinations Table

Location: **Norwalk, CT**
 Date: 3/23/09

Prepared by: T.J.L. Checked by: C.F.C.

Job No. 08174.CO5

Load Combination	Description	Envelope	Wind	Solution	Factor	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor	BLC	Factor
1	TIA/EIA Wind + Ice on PCS Mast + PCS Structure	1		1	1	1	1	2	1	3	1	4	1	1
2	TIA/EIA Wind on PCS Mast + PCS Structure	1		1	1	1	2	1	5	1				

Footnotes:

(1) BLC = Basic Load Case

(2) PCS Structure includes: antennas, tma's, mounts, coax cable, and miscellaneous hardware

Global

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation	Yes
Include Warping	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Vertical Axis	Y

Hot Rolled Steel Code	AISC: ASD 9th
Cold Formed Steel Code	AISI 99: ASD
Wood Code	NDS 91/97: ASD
Wood Temperature	< 100F
Concrete Code	ACI 2002

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	PCA Load Contour
Parame Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections	Yes
Bad Framing Warnings	No
Unused Force Warnings	Yes

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (1E5 F)	Density[k/ft^3]	Yield[ksi]
1	A572 Gr.50	29000	11154	.3	.65	.49	50
2	A992	29000	11154	.3	.65	.49	50
3	A500 Gr.42	29000	11154	.3	.65	.49	42
4	A500 Gr. C	29000	11154	.3	.65	.49	50
5	A53 Gr. B	29000	11154	.3	.65	.49	35

Hot Rolled Steel Design Parameters

	Label	Shape	Lengt...	Lbyy[ft]	Lbzz[ft]	Lcomp top[ft]	Lcomp bot[ft]	Kyy	Kzz	Cm-yy	Cm-...	Cb	y sw...	z sw...	Function
1	M1	MAST	33												Lateral
2	M2	MAST	22												Lateral

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rules	A [in2]	Iyy [in4]	Izz [in4]	J [in4]
1	MAST	PIPE 12.0X	Column	Pipe	A53 Gr. B	Typical	17.9	339	339	678

Member Primary Data

	Label	I Joint	J Joint	K ...	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	BOTTOM CONN...	FLANGE ...			MAST	Column	Pipe	A53 Gr. B	Typical
2	M2	FLANGE CONNE...	TOPOFM...			MAST	Column	Pipe	A53 Gr. B	Typical

Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia...
1	BOTTOM_CONNECTION	0	0	0	0	
2	TOP_CONNECTION	0	21.5	0	0	
3	FLANGE_CONNECTION	0	33	0	0	

Joint Coordinates and Temperatures (Continued)

Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia...
4 ANTENNA CL1	0	42	0	0	
5 ANTENNA CL2	0	52	0	0	
6 TOPOFMAST	0	55	0	0	

Joint Boundary Conditions

Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]	Footing
1 BOTTOM_CONN...	Reaction	Reaction	Reaction				
2 TOP_CONNECTI...	Reaction	Reaction	Reaction				
3 FLANGE CONNE...							
4 ANTENNA CL1							
5 ANTENNA CL2							
6 TOPOFMAST							

Joint Loads and Enforced Displacements (BLC 2 : Weight of Antennas, Mounts)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1 ANTENNA CL1	L	Y	-105
2 ANTENNA CL2	L	Y	-122
3 ANTENNA CL1	L	Y	-085
4 ANTENNA CL1	L	Y	-08
5 ANTENNA CL2	L	Y	-08

Joint Loads and Enforced Displacements (BLC 3 : Weight of Ice Only)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1 ANTENNA CL1	L	Y	-098
2 ANTENNA CL2	L	Y	-101
3 ANTENNA CL1	L	Y	-043
4 ANTENNA CL1	L	Y	-035
5 ANTENNA CL2	L	Y	-035

Joint Loads and Enforced Displacements (BLC 4 : TIA/EIA Wind with Ice)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1 ANTENNA CL1	L	X	.645
2 ANTENNA CL2	L	X	.801
3 ANTENNA CL1	L	X	.301

Joint Loads and Enforced Displacements (BLC 5 : TIA/EIA Wind)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1 ANTENNA CL1	L	X	.766
2 ANTENNA CL2	L	X	.966
3 ANTENNA CL1	L	X	.335

Member Distributed Loads (BLC 2 : Weight of Antennas, Mounts)

Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...	Start Location[ft,%]	End Location[ft,%]
1 M1	Y	-009	-009	23	33
2 M2	Y	-009	-009	0	9
3 M2	Y	-005	-005	9	19

Member Distributed Loads (BLC 3 : Weight of Ice Only)

Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...	Start Location[ft,%]	End Location[ft,%]
1 M1	Y	-015	-015	23	33
2 M1	Y	-008	-008	0	0

Member Distributed Loads (BLC 3 : Weight of Ice Only) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,deg]	Start Location[ft,%]	End Location[ft,%]
3	M2	Y	-.015	-.015	0	9
4	M2	Y	-.008	-.008	9	19
5	M2	Y	-.008	-.008	0	0

Member Distributed Loads (BLC 4 : TIA/EIA Wind with Ice)

	Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,deg]	Start Location[ft,%]	End Location[ft,%]
1	M1	X	.026	.026	0	23
2	M1	X	.053	.053	23	33
3	M2	X	.053	.053	0	7
4	M2	X	.053	.053	11	17

Member Distributed Loads (BLC 5 : TIA/EIA Wind)

	Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,deg]	Start Location[ft,%]	End Location[ft,%]
1	M1	X	.031	.031	0	23
2	M1	X	.066	.066	23	33
3	M2	X	.066	.066	0	7
4	M2	X	.066	.066	11	17

Basic Load Cases

	BLC Description	Category	X Gra...	Y Grav...	Z Gra...	Joint	Point	Distributed	Area (Mem...	Surfa...
1	Self Weight (PCS Mast)	None		-1						
2	Weight of Antennas, Mounts	None								
3	Weight of Ice Only	None				5	3			
4	TIA/EIA Wind with Ice	None				5	5			
5	TIA/EIA Wind	None				3	4			
						3	4			

Load Combinations

	Description	Solve	PD...	SR...	BLCFa...							
1	TIA/EIA Wind + Ice	Yes			1	1	2	1	3	1	4	1
2	TIA/EIA Wind	Yes			1	1	2	1	5	1		
3	Self Weight				1	1						

Envelope Member Section Forces

Member	Sec		Axial[k]	lc	y Shear[k]	lc	z Shear[k]	lc	Torque[k-ft]	lc	y-y Mome...	lc	z-z Momen...	lc
M1	1	max	.741	1	-2.556	1	0	1	0	1	0	1	0	1
		min	.655	2	-3.08	2	0	1	0	1	0	1	0	1
	2	max	.172	1	-2.771	1	0	1	0	1	0	1	0	1
		min	.152	2	-3.336	2	0	1	0	1	0	1	26.466	2
	3	max	-.35	2	-2.985	1	0	1	0	1	0	1	21.975	1
		min	-.396	1	-3.592	2	0	1	0	1	0	1	55.041	2
	4	max	3.413	1	3.469	2	0	1	0	1	0	1	45.72	1
		min	2.52	2	2.873	1	0	1	0	1	0	1	61.801	2
	5	max	2.646	1	2.925	2	0	1	0	1	0	1	51.384	1
		min	1.943	2	2.436	1	0	1	0	1	0	1	35.424	2
M2	1	max	2.646	1	2.925	2	0	1	0	1	0	1	29.483	1
		min	1.943	2	2.436	1	0	1	0	1	0	1	35.424	2
	2	max	2.135	1	2.562	2	0	1	0	1	0	1	29.483	1
		min	1.559	2	2.144	1	0	1	0	1	0	1	20.335	2
	3	max	1.2	1	1.361	2	0	1	0	1	0	1	16.887	1
		min	.912	2	1.118	1	0	1	0	1	0	1	8.916	2
	4	max	.75	1	.999	2	0	1	0	1	0	1	7.362	1
		min	.55	2	.827	1	0	1	0	1	0	1	2.423	2

Envelope Member Section Forces (Continued)

Member	Sec	Axial[k]	lc y Shear[k]	lc z Shear[k]	lc Torque[k-ft]	lc y-y Mome...	lc z-z Momen...
19	5	max	0	1	0	1	0
20		min	0	1	0	1	0

Envelope Member Section Stresses

Member	Sec	Axial[kksi]	lc y Shear...	lc z Shear...	lc y-Top[kksi]	lc y-Bot[kksi]	lc z-Top[kksi]	lc z-Bot[kksi]
1	M1	1	max	.041	1	-.286	1	0
2			min	.037	2	-.344	2	0
3		2	max	.01	1	-.31	1	0
4			min	.009	2	-.373	2	0
5		3	max	-.02	2	-.334	1	0
6			min	-.022	1	-.401	2	0
7		4	max	.191	1	.388	2	0
8			min	.141	2	.321	1	0
9		5	max	.148	1	.327	2	0
10			min	.109	2	.272	1	0
11	M2	1	max	.148	1	.327	2	0
12			min	.109	2	.272	1	0
13		2	max	.119	1	.286	2	0
14			min	.087	2	.24	1	0
15		3	max	.067	1	.152	2	0
16			min	.051	2	.125	1	0
17		4	max	.042	1	.112	2	0
18			min	.031	2	.092	1	0
19		5	max	0	1	0	1	0
20			min	0	1	0	1	0

Envelope Joint Reactions

Joint	X [k]	lc Y [k]	lc Z [k]	lc MX [k-ft]	lc MY [k-ft]	lc MZ [k-ft]							
1	BOTTOM_CON... max	3.08	2	.741	1	0	1	0	1	0	1	0	
2		min	2.556	1	.655	2	0	1	0	1	0	1	0
3	TOP_CONNEC... max	-6.12	1	4.419	1	0	1	0	1	0	1	0	
4		min	-7.378	2	3.388	2	0	1	0	1	0	1	0
5	ANTENNA_CL1	max	NC	NC	NC	NC	NC	LOCKED	NC	NC	NC	NC	
6		min	NC	NC	NC	NC	NC	LOCKED	NC	NC	NC	NC	
7	Totals:	max	-3.564	1	5.16	1	0	1	0	1	0	1	0
8		min	-4.298	2	4.043	2	0	1	0	1	0	1	0

Envelope Joint Displacements

Joint	X [in]	lc Y [in]	lc Z [in]	lc X Rotation...	lc Y Rotation...	lc Z Rotation...							
1	BOTTOM_CO... max	0	1	0	2	0	1	0	1	0	1	3.632e-3	2
2		min	0	2	0	1	0	1	0	1	0	3.016e-3	1
3	TOP_CONNE... max	0	2	0	2	0	1	0	1	0	1	-6.269e-3	1
4		min	0	1	0	1	0	1	0	1	0	-7.548e-3	2
5	FLANGE_CO... max	1.744	2	0	2	0	1	0	1	0	1	-1.379e-2	1
6		min	1.449	1	0	1	0	1	0	1	0	-1.659e-2	2
7	ANTENNA_CL1	max	3.731	2	0	2	0	1	0	1	0	-1.698e-2	1
8		min	3.101	1	-.001	1	0	1	0	1	0	-1.964e-2	2
9	ANTENNA_CL2	max	6.154	2	-.001	2	0	1	0	1	0	-1.698e-2	1
10		min	5.114	1	-.002	1	0	1	0	1	0	-2.043e-2	2
11	TOPOFMAST	max	6.89	2	-.001	2	0	1	0	1	0	-1.698e-2	1
12		min	5.726	1	-.002	1	0	1	0	1	0	-2.043e-2	2

Company : Natcomm Inc
 Designer : tjf / cfc
 Job Number : 08174-CO.5

Proposed Mast on CL&P Tower # 1102

July 8, 2009
 4:09 PM
 Checked By: _____

Envelope AISC ASD Steel Code Checks

Member	Shape	Code Check	Loc[ft]	lc	Shear Check	Loc[ft]	lc	Fa	Ft	Fb	C	C	AS
1	M1	PIPE 12.0X	.719	21.656	2	.030	21.313	2	13...	21...	23.11	.6	.85H1-2
2	M2	PIPE 12.0X	.351	0	2	.023	0	2	16...	21...	23.11	.6	.85H1-2

Company : Natcomm Inc
 Designer : tj / cfc
 Job Number : 08174-CO.5

Proposed Mast on CL&P Tower # 1102

July 8, 2009
 4:12 PM
 Checked By: _____

Joint Reactions

LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	1 BOTTOM CONNECTION	2.556	.741	0	0	0	0
2	1 TOP CONNECTION	-6.12	4.419	0	0	0	0
3	1 ANTENNA CL1	NC	NC	NC	NC	0	0
4	1 Totals:	-3.564	5.16	0	NC	LOCKED	NC
5	1 COG (ft):	X: 0	Y: 31.291	Z: 0			

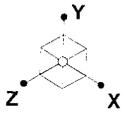
Company : Natcomm Inc
 Designer : tjf / cfc
 Job Number : 08174-CO.5

Proposed Mast on CL&P Tower # 1102

July 8, 2009
 4:13 PM
 Checked By: _____

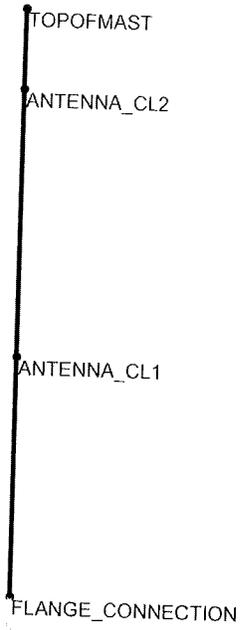
Joint Reactions

LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	2 BOTTOM CONNECTION	3.08	.655	0	0	0	0
2	2 TOP CONNECTION	-7.378	3.388	0	0	0	0
3	2 ANTENNA CL1	NC	NC	NC	NC	0	0
4	2 Totals:	-4.298	4.043	0	NC	LOCKED	NC
5	2 COG (ft):	X: 0	Y: 30.145	Z: 0			



Code Check

Black	No Calc
Dark Grey	> 1.0
Medium Grey	.90-1.0
Light Grey	.75-.90
White	.50-.75
Black	0-.50



TOP_CONNECTION

BOTTOM_CONNECTION

Solution: Envelope

Natcomm Inc

tjl / cfc

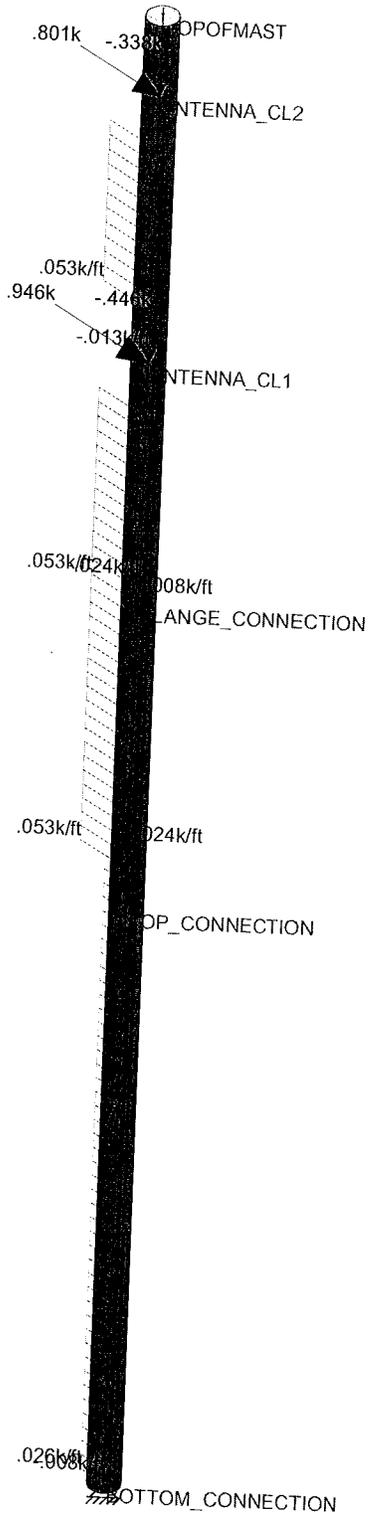
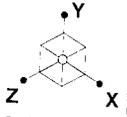
08174-CO.5

Proposed Mast on CL&P Tower # 1102

Unity Check

July 8, 2009 at 4:11 PM

Proposed Pipe Mast TIA-EIA.r3d



Loads: LC 1, TIA/EIA Wind + Ice

Natcomm Inc

tjl / cfc

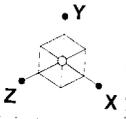
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Proposed Mast on CL&P Tower # 1102

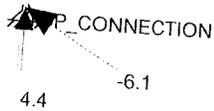
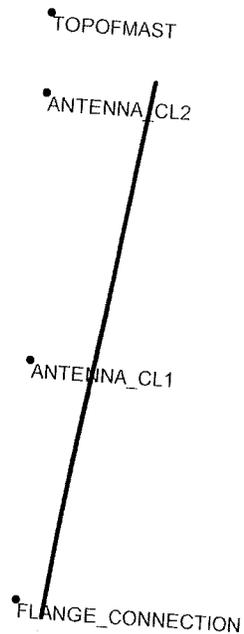
LC # 1 Loads

July 8, 2009 at 4:10 PM

Proposed Pipe Mast TIA-EIA.r3d



Code Check	
Black	No Calc
White	> 1.0
Light Gray	.90-1.0
Medium Gray	.75-.90
Dark Gray	.50-.75
Black	0-.50



Results for LC 1, TIA/EIA Wind + Ice
Reaction units are k and k-ft

Natcomm Inc

tjl / cfc

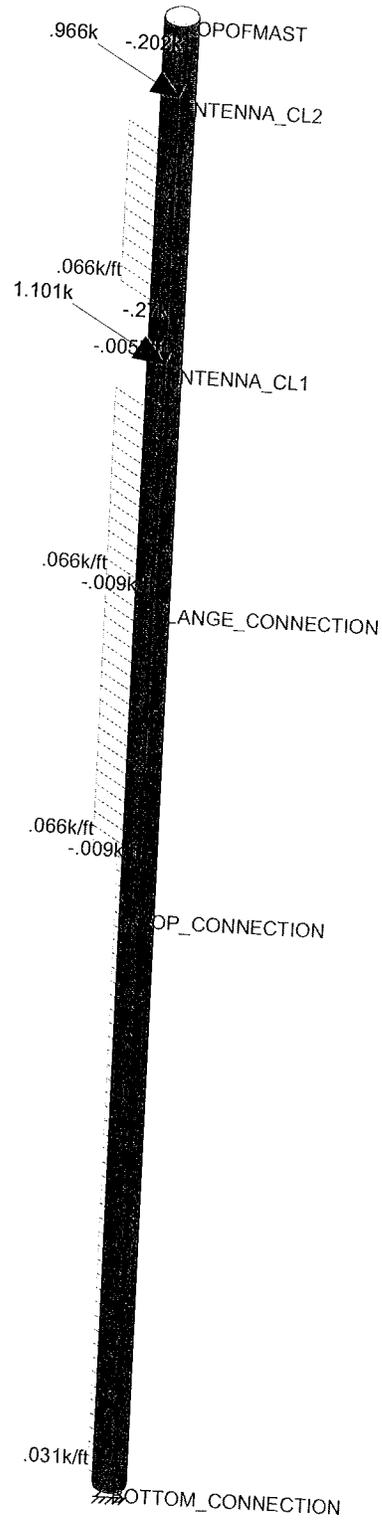
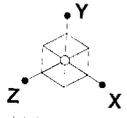
08174-CO.5

Proposed Mast on CL&P Tower # 1102

LC # 1 Reactions and Deflected Shape

July 8, 2009 at 4:12 PM

Proposed Pipe Mast TIA-EIA.r3d



Loads: LC 2, TIA/EIA Wind

Natcomm Inc

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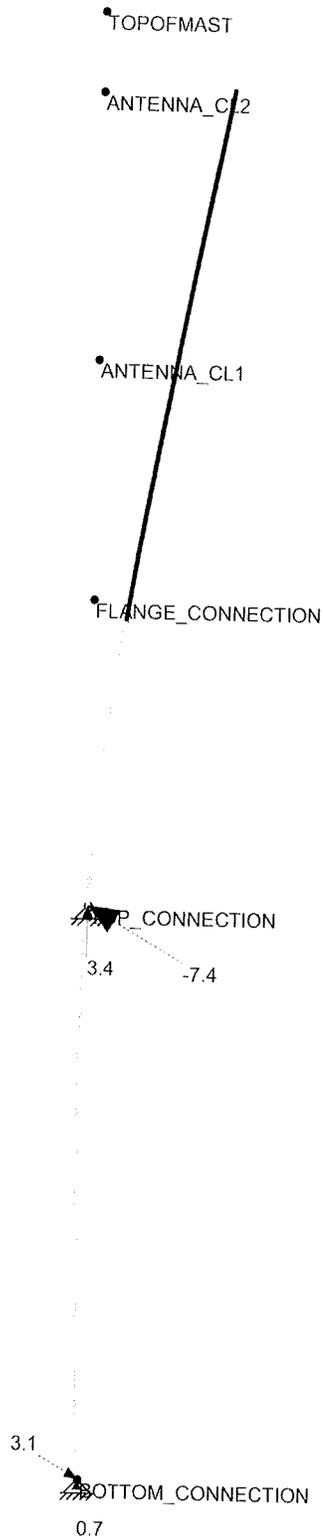
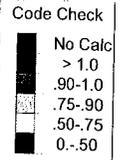
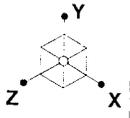
08174-CO.5

Proposed Mast on CL&P Tower # 1102

LC # 2 Loads

July 8, 2009 at 4:11 PM

Proposed Pipe Mast TIA-EIA.r3d



Results for LC 2, TIA/EIA Wind
 Reaction units are k and k-ft

Natcomm Inc

tjl / cfc

08174-CO.5

Proposed Mast on CL&P Tower # 1102

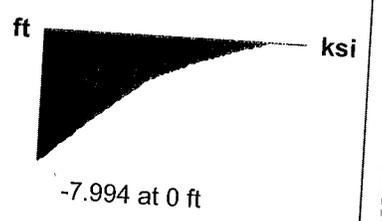
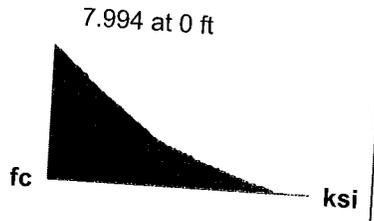
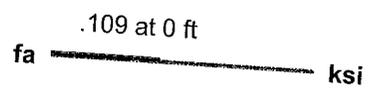
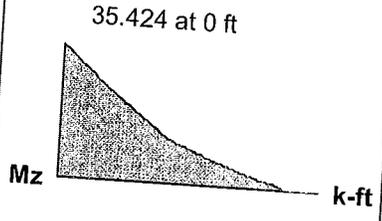
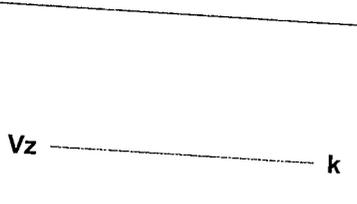
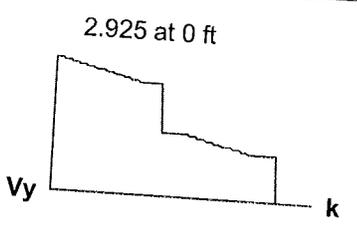
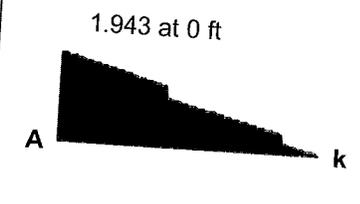
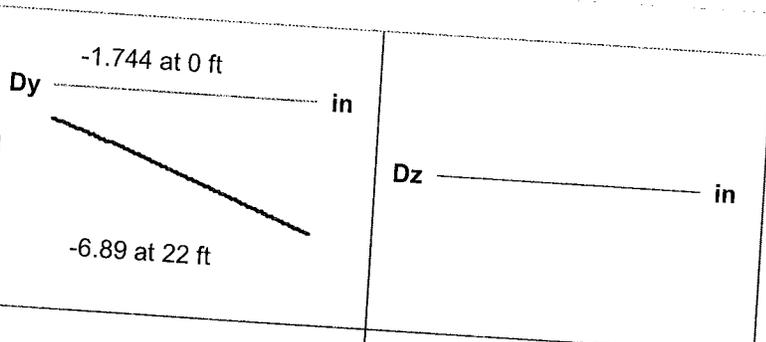
LC # 2 Reactions and Deflected Shape

July 8, 2009 at 4:13 PM

Proposed Pipe Mast TIA-EIA.r3d

Column: **M2**

Shape: **PIPE_12.0X**
 Material: **A53 Gr. B**
 Length: **22 ft**
 I Joint: **FLANGE_CONNECTION**
 J Joint: **TOPOFMAST**
 LC 2: **TIA/EIA Wind**
 Code Check: **0.351 (bending)**
 Report Based On 97 Sections



AISC ASD 9th Ed. Code Check

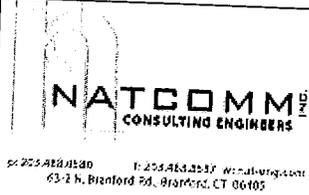
Max Bending Check **0.351**
 Location **0 ft**
 Equation **H1-2**

Max Shear Check **0.023 (s)**
 Location **0 ft**
 Max Defl Ratio **L/51**

Compact

Fy **35 ksi**
 Fa **16.963 ksi**
 Ft **21 ksi**
 Fby **23.1 ksi**
 Fbz **23.1 ksi**
 Fvy **14 ksi**
 Fvz **14 ksi**
 Cb **1.75**

	Y-Y	Z-Z
Cm	.6	.85
Lb	22 ft	22 ft
KL/r	60.664	60.664
Sway	No	No
L Comp Flange	22 ft	
Torque Length	NC	



Subject:

FLANGE BOLTS AND PLATE

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO5

Flange Bolt and Flange Plate Analysis:

Input Data:

Tower Reactions:

Overturning Moment =	OM := 35.5-ft-kips	(Input From Risa-3D LC #2)
Shear Force =	Shear := 3-kips	(Input From Risa-3D LC #2)
Axial Force =	Axial := 2-kips	(Input From Risa-3D LC #2)

Anchor Bolt Data:

Use ASTM A325

Number of Anchor Bolts =	N := 8	(User Input)
Diameter of Bolt Circle =	D_{bc} := 17.0-in	(User Input)
Bolt "Column" Distance =	l := 0-in	(User Input)
Bolt Ultimate Strength =	F_u := 120-ksi	(User Input)
Bolt Yield Strength =	F_y := 92-ksi	(User Input)
Bolt Modulus =	E := 29000-ksi	(User Input)
Diameter of Anchor Bolts =	D := 1.125-in	(User Input)
Threads per Inch =	n := 8	(User Input)

Base Plate Data:

Use ASTM A36

Plate Yield Strength =	$F_{y_{bp}}$:= 36-ksi	(User Input)
Base Plate Thickness =	t_{bp} := 1.5-in	(User Input)
Base Plate Diameter =	D_{bp} := 20-in	(User Input)
Outer Pole Diameter =	D_{pole} := 12.8-in	(User Input)

Geometric Layout Data:

Distance from Bolts to Centroid of Pole:

Radius of Bolt Circle = $R_{bc} := \frac{D_{bc}}{2} = 8.5\text{-in}$

Distance to Bolts = $i := 1..N$

$$d_i := \begin{cases} \theta \leftarrow 2 \cdot \pi \cdot \left(\frac{i}{N}\right) \\ d \leftarrow R_{bc} \cdot \sin(\theta) \end{cases}$$

$d_1 = 6.01\text{-in}$	$d_6 = -8.50\text{-in}$
$d_2 = 8.50\text{-in}$	$d_7 = -6.01\text{-in}$
$d_3 = 6.01\text{-in}$	$d_8 = -0.00\text{-in}$
$d_4 = 0.00\text{-in}$	
$d_5 = -6.01\text{-in}$	

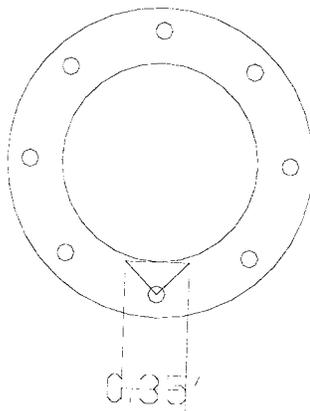
Critical Distances For Bending in Plate:

Outer Pole Radius = $R_{pole} := \frac{D_{pole}}{2} = 6.4\text{-in}$

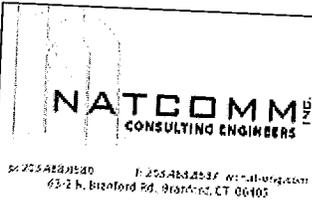
Moment Arms of Bolts about Neutral Axis =

$$MA_i := \text{if}(d_i \geq R_{pole}, d_i - R_{pole}, 0\text{in})$$

$MA_1 = 0.00\text{-in}$	$MA_6 = 0.00\text{-in}$
$MA_2 = 2.10\text{-in}$	$MA_7 = 0.00\text{-in}$
$MA_3 = 0.00\text{-in}$	$MA_8 = 0.00\text{-in}$
$MA_4 = 0.00\text{-in}$	
$MA_5 = 0.00\text{-in}$	



Effective Width = $W_{eff} := 4.2\text{-in}$



Subject:

FLANGE BOLTS AND PLATE

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO5

Anchor Bolt Analysis:

Calculated Anchor Bolt Properties:

Polar Moment of Inertia = $I_p := \sum_i (d_i)^2 = 289 \cdot \text{in}^2$

Gross Area of Bolt = $A_g := \frac{\pi}{4} \cdot D^2 = 0.994 \cdot \text{in}^2$

Net Area of Bolt = $A_n := \frac{\pi}{4} \left(D - \frac{0.9743 \cdot \text{in}}{n} \right)^2 = 0.79 \cdot \text{in}^2$

Net Diameter = $D_n := \frac{2 \cdot \sqrt{A_n}}{\sqrt{\pi}} = 1.003 \cdot \text{in}$

Radius of Gyration of Bolt = $r := \frac{D_n}{4} = 0.251 \cdot \text{in}$

Section Modulus of Bolt = $S_x := \frac{\pi \cdot D_n^3}{32} = 0.099 \cdot \text{in}^3$

Check Anchor Bolt Tension Force:

Maximum Tensile Force = $T_{\text{Max}} := \text{OM} \cdot \frac{R_{bc}}{I_p} - \frac{\text{Axial}}{N} = 12.3 \cdot \text{kips}$

Allowable Tensile Force Gross Area = $T_{\text{ALL.Gross}} := (0.33 \cdot A_g \cdot F_u) = 39.4 \cdot \text{kips}$

Allowable Tensile Force Net Area = $T_{\text{ALL.Net}} := (0.6 \cdot A_n \cdot F_y) = 43.6 \cdot \text{kips}$

Bolt Tension % of Capacity = $\frac{T_{\text{Max}}}{T_{\text{ALL.Net}}} = 0.281$

Condition1 = $\text{Condition1} := \text{if} \left(\frac{T_{\text{Max}}}{T_{\text{ALL.Gross}}} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$

Condition1 = "OK"



Subject:

FLANGE BOLTS AND PLATE

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO5

Base Plate Analysis:

Force from Bolts =

$$C_i := \frac{OM \cdot d_i}{l_p} + \frac{|Axial|}{N}$$

$C_1 = 9.1 \cdot \text{kips}$

$C_6 = -12.3 \cdot \text{kips}$

$C_2 = 12.8 \cdot \text{kips}$

$C_7 = -8.6 \cdot \text{kips}$

$C_3 = 9.1 \cdot \text{kips}$

$C_8 = 0.2 \cdot \text{kips}$

$C_4 = 0.3 \cdot \text{kips}$

$C_5 = -8.6 \cdot \text{kips}$

Maximum Bending Stress in Plate =

$$f_{bp} := \sum_i \frac{6(C_i \cdot M A_i)}{(W_{eff} t_{bp}^2)} = 17 \cdot \text{ksi}$$

Allowable Bending Stress in Plate =

$F_{bp} := 0.75 \cdot F_y = 27 \cdot \text{ksi}$

Plate Bending Stress % of Capacity =

$\frac{f_{bp}}{F_{bp}} = 0.631$

Condition3 =

Condition2 := if $\left(\frac{f_{bp}}{F_{bp}} < 1.00, "Ok", "Overstressed" \right)$

Condition2 = "Ok"

Subject:

Connection of Mast to CL&P Tower # 1102

Location:

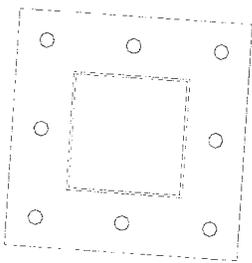
Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO.5

Mast Connection to CL&P Tower:

Mast To HSS Tube Connection:



Reactions:

Moment = Moment := 0-kips (Input From Risa-3D LC #2)
 Vertical = Vertical := 3.5-kips (Input From Risa-3D LC #2)
 Horizontal = Horizontal := 7.5-kips (Input From Risa-3D LC #2)

Bolt Data:

Bolt Type = ASTM A325 (User Input)
 Bolt Diameter = D := 0.75-in (User Input)
 Number of Bolts = $N_b := 8$ (User Input)
 Allowable Tensile Strength = $F_t := 19.9$ -kips (User Input)
 Allowable Shear Strength = $F_v := 10.6$ -kips (User Input)

Maximum Tensile Force = $f_t := \frac{\text{Horizontal}}{N_b} = 0.9$ -kips

Bolt Tension % of Capacity = $\frac{f_t}{F_t} = 4.71$ %

Check Bolt Tension = Bolt_Tension := if $\left(\frac{f_t}{F_t} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$

Bolt_Tension = "OK"

Maximum Shear Force = $f_v := \frac{\text{Vertical}}{N_b} = 0.4$ -kips

Bolt Shear % of Capacity = $\frac{f_v}{F_v} = 4.13$ %

Check Bolt Shear = Bolt_Shear := if $\left(\frac{f_v}{F_v} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$

Bolt_Shear = "OK"

Subject:

Connection of Mast to CL&P Tower # 1102

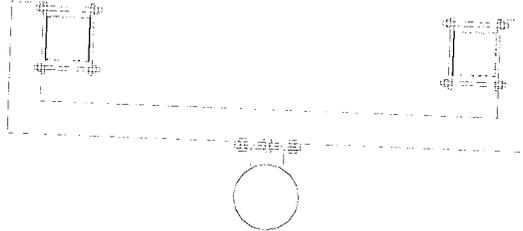
Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO.5

Connecting Tube



Reactions:

Moment = Moment := 0-kips (Input From Risa-3D LC #2)
 Vertical = Vertical := 3.5-kips (Input From Risa-3D LC #2)
 Horizontal = Horizontal := 7.5-kips (Input From Risa-3D LC #2)

Tube Data:

Tube Size = HSS 6x6x1/4 (User Input)
 Steel Grade = A500 Grade B (User Input)
 Section Modulus = $S_x := 9.54\text{-in}^3$ (User Input)
 Length of Tube = Length := 7-ft (User Input)

Allowable Bending Stress = $F_b := 0.66 \cdot 46\text{-ksi} = 30.4\text{-ksi}$

Maximum Moment in Tube = $M_{\max} := \frac{\text{Horizontal-Length}}{4} = 13.125\text{-kip-ft}$

Actual Bending Stress in Tube = $f_b := \frac{M_{\max}}{S_x} = 16.5\text{-ksi}$

Check Bending Tube Stress = $\text{Bending_Stress} := \text{if} \left(\frac{f_b}{F_b} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$

Bending_Stress = "OK"

Subject:

Connection of Mast to CL&P Tower # 1102

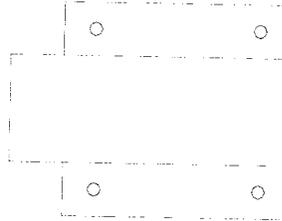
Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO.5

Tube To Tower Leg Connection:



Reactions:

Moment = Moment := 0-kips (Input From Risa-3D LC #2)
 Vertical = Vertical := 1.75-kips (Input From Risa-3D LC #2)
 Horizontal = Horizontal := 3.75-kips (Input From Risa-3D LC #2)

Bolt Data:

Bolt Type = ASTM A325 (User Input)
 Bolt Diameter = D := 0.75-in (User Input)
 Number of Bolts = $N_b := 4$ (User Input)
 Allowable Tensile Strength = $F_t := 19.9$ -kips (User Input)
 Allowable Shear Strength = $F_v := 10.6$ -kips (User Input)

Horizontal Shear Force = $f_{v_horz} := \frac{\text{Horizontal}}{N_b} = 0.9\text{-kips}$

Vertical Shear Force = $f_{v_vert} := \frac{\text{Vertical}}{N_b} = 0.4\text{-kips}$

Combined Shear Force = $f_{v_tot} := f_{v_horz} + f_{v_vert} = 1.4\text{-kips}$

Bolt Shear % of Capacity = $\frac{f_{v_tot}}{F_t} = 6.91\%$

Check Combined Vertical and Horizontal Bolt Shear = $\text{Bolt_Shear} := \text{if} \left(\frac{f_{v_tot}}{F_v} \leq 1.00, \text{"OK"}, \text{"Overstressed"} \right)$

Bolt_Shear = "OK"

Subject:

Load Analysis of Existing PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Basic Components

Heavy Wind Pressure = $p := 4.00$ psf
 Basic Windspeed = $V := 110$ mph (NESC 2007 Figure 250-1 & Table 250-1)
 Radial Ice Thickness = $Ir := 0.50$ in (NESC 2007 Figure 250-2(e))
 Radial Ice Density = $Id := 56.0$ pcf

Factors for Extreme Wind Calculation

Elevation of Top of PCS Mast Above Grade = $TME := 117$ ft
 Multiplier Gust Response Factor = $m := 1.25$ (Only for NESC Extreme case NU criteria)
 NESC Factor = $kv := 1.43$ (NESC 2007 Table 250-3 equation)
 Importance Factor = $I := 1.0$ (NESC Section 250.C.2)

Velocity Pressure Coefficient = $Kz := 2.01 \cdot \left(0.67 \cdot \frac{TME}{900} \right)^{\frac{2}{9.5}} = 1.202$ (NESC 2007 Table 250-2)

Exposure Factor = $Es := 0.346 \left[\frac{33}{(0.67 \cdot TME)} \right]^{\frac{1}{7}} = 0.306$ (NESC 2007 Table 250-3)

Response Term = $Bs := \frac{1}{\left(1 + 0.375 \cdot \frac{TME}{220} \right)} = 0.834$ (NESC 2007 Table 250-3)

Gust Response Factor = $Grf := \frac{\left[1 + \left(2.7 \cdot Es \cdot Bs \cdot \frac{1}{2} \right) \right]}{kv^2} = 0.858$ (NESC 2007 Table 250-3)

Wind Pressure = $qz := 0.00256 \cdot Kz \cdot V^2 \cdot Grf \cdot I = 31.9$ psf (NESC 2007 Section 250.C.2)

Shape Factors

Shape Factor for Round Members = $CdR := 1.3$
 Shape Factor for Round Members = $CdF := 1.6$
 Shape Factor for Coax Cables Attached to Outside of Pole = $Cd_{coax} := 1.45$

NUS Design Criteria Issued April 12, 2007

Overload Factors

Overload Factors for Wind Loads:

NESC Heavy Loading = 2.5
 NESC Extreme Loading = 1.0
 NU Design Criteria Table
 Apply in Risa-3D Analysis
 Apply in Risa-3D Analysis

Overload Factors for Vertical Loads:

NESC Heavy Loading = 1.5
 NESC Extreme Loading = 1.0
 Apply in Risa-3D Analysis
 Apply in Risa-3D Analysis



Subject:

Load Analysis of Existing PCS Mast on
CL&P Structure #1102

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No. 08174.CO.5

Development of Wind & Ice Load on PCS Mast

PCS Mast Data:

Mast Shape = Round
 Mast Diameter = $D_{mast} := 12.8$ in (Pipe 12" SCH. 80)
 Mast Length = $L_{mast} := 55$ ft
 Mast Thickness = $t_{mast} := 0.5$ in

Wind Load (NESC Extreme)

*Assumes Mast is Shielded by Coax Cable
and Antennas Top 32' of Mast*

Mast Projected Surface Area = $A_{mast} := \frac{D_{mast}}{12} = 1.067$ sq ft/ft
 Total Mast Wind Force (Below NU Structure) = $qz \cdot Cd_R \cdot A_{mast} = 44$ plf **BLC 5**

Wind Load (NESE Heavy)

*Assumes Mast is Shielded by Coax Cable
and Antennas Top 32' of Mast*

Mast Projected Surface Area w/ Ice = $A_{ICE_{mast}} := \frac{(D_{mast} + 2 \cdot I_r)}{12} = 1.15$ sq ft/ft
 Total Mast Wind Force w/ Ice = $p \cdot Cd_R \cdot A_{ICE_{mast}} = 6$ plf **BLC 4**

Gravity Loads (without ice)

Weight of the mast =

Self Weight (Computed internally by Risa-3D) plf **BLC 1**

Gravity Loads (ice only)

Ice Area per Linear Foot =

$A_{i_{mast}} := \frac{\pi}{4} [(D_{mast} + I_r \cdot 2)^2 - D_{mast}^2] = 20.9$ sq in

Weight of Ice on Mast =

$W_{ICE_{mast}} := I_d \cdot \frac{A_{i_{mast}}}{144} = 8$ plf **BLC 3**

Subject:

Load Analysis of Existing PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

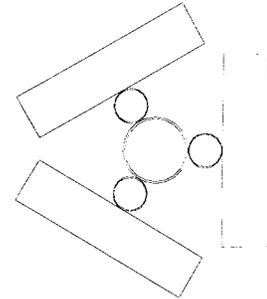
Rev. 1: 7/8/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on Antennas

Antenna Data:

Antenna Model =	RFS APX16PV-16PVL
Antenna Shape =	Flat
Antenna Height =	$L_{ant2} := 53$ in
Antenna Width =	$W_{ant2} := 12.9$ in
Antenna Thickness =	$T_{ant2} := 3.1$ in
Antenna Weight =	$WT_{ant2} := 39.6$ lbs
Number of Antennas =	$N_{ant2} := 3$



(T-Mobile @ 114')

Wind Load (NESC Extreme)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna =	$SA_{ant2} := \frac{L_{ant2} \cdot W_{ant2}}{144} = 4.7$	sf
Antenna Projected Surface Area =	$A_{ant2} := SA_{ant2} \cdot N_{ant2} = 14.2$	sf
Total Antenna Wind Force =	$F_{ant2} := qz \cdot Cd_F \cdot A_{ant2} \cdot m = 910$	lbs BLC 5

Wind Load (NESC Heavy)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna w/ Ice =	$SA_{ICEant2} := \frac{(L_{ant2} + 1)(W_{ant2} + 1)}{144} = 5.2$	sf
Antenna Projected Surface Area w/ Ice =	$A_{ICEant2} := SA_{ICEant2} \cdot N_{ant2} = 15.6$	sf
Total Antenna Wind Force w/ Ice =	$F_{i_{ant2}} := p \cdot Cd_F \cdot A_{ICEant2} = 100$	lbs BLC 4

Gravity Load (without Ice)

Weight of All Antennas =	$WT_{ant2} \cdot N_{ant2} = 119$	lbs BLC 2
--------------------------	----------------------------------	------------------

Gravity Load (Ice only)

Volume of Each Antenna =	$V_{ant2} := L_{ant2} \cdot W_{ant2} \cdot T_{ant2} = 2119$	cu in
Volume of Ice on Each Antenna =	$V_{ice} := (L_{ant2} + 1)(W_{ant2} + 1)(T_{ant2} + 1) - V_{ant2} = 958$	cu in
Weight of Ice on Each Antenna =	$W_{ICEant2} := \frac{V_{ice}}{1728} \cdot \rho_d = 31$	lbs
Weight of Ice on All Antennas =	$W_{ICEant2} \cdot N_{ant2} = 93$	lbs BLC 3

Subject:

Load Analysis of Existing PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

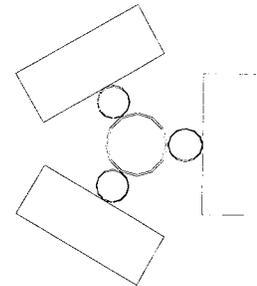
Rev. 1: 7/8/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on TMA's

TMA Data:

(T-Mobile @ 114')
TMA Model = Powerwave LGP214
TMA Shape = Flat
TMA Height = $L_{TMA} := 9.2$ in
TMA Width = $W_{TMA} := 14.4$ in
TMA Thickness = $T_{TMA} := 2.6$ in
TMA Weight = $W_{TMA} := 15$ lbs
Number of TMA's = $N_{TMA} := 6$



Wind Load (NESC Extreme)

Assumes Maximum Possible Wind Pressure on TMA's

Surface Area for One TMA = $SA_{TMA} := \frac{L_{TMA} \cdot W_{TMA}}{144} = 0.9$ sf
TMA Projected Surface Area = $A_{TMA} := SA_{TMA} \cdot N_{TMA} = 5.5$ sf
Total TMA Wind Force = $F_{TMA} := qz \cdot C_d \cdot A_{TMA} \cdot m = 353$ lbs **BLC 5**

Wind Load (NESC Heavy)

Assumes Maximum Possible Wind Pressure on TMA's

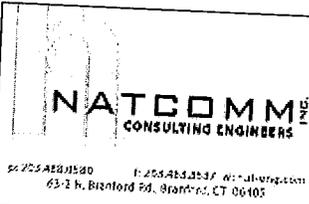
Surface Area for One TMA w/ Ice = $SA_{ICETMA} := \frac{(L_{TMA} + 1)(W_{TMA} + 1)}{144} = 1.1$ sf
TMA Projected Surface Area w/ Ice = $A_{ICETMA} := SA_{ICETMA} \cdot N_{TMA} = 6.5$ sf
Total TMA Wind Force w/ Ice = $F_{TMA} := p \cdot C_d \cdot A_{ICETMA} = 42$ lbs **BLC 4**

Gravity Load (without Ice)

Weight of All TMA's = $W_{TMA} \cdot N_{TMA} = 90$ lbs **BLC 2**

Gravity Load (Ice only)

Volume of Each TMA = $V_{TMA} := L_{TMA} \cdot W_{TMA} \cdot T_{TMA} = 344$ cu in
Volume of Ice on Each TMA = $V_{ice} := (L_{TMA} + 1)(W_{TMA} + 1)(T_{TMA} + 1) - V_{TMA} = 221$ cu in
Weight of Ice on Each TMA = $W_{ICETMA} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 7$ lbs
Weight of Ice on All TMA's = $W_{ICETMA} \cdot N_{TMA} = 43$ lbs **BLC 3**



Subject:

Load Analysis of Existing PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

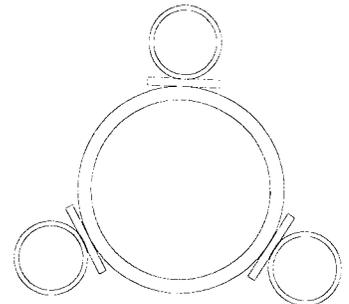
Rev. 1: 7/8/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on Antenna Mounts

Mount Data:

(T-Mobile @ 114')
 Mount Type: Microflex Tri-Sector Adapter
 Mountw/ 3 Pipes
 Mount Shape = Round
 Pipe Mount Length = $L_{mnt} := 66$ in
 2 inch Pipe Mount Linear Weight = $W_{mnt} := 3.66$ plf
 Pipe Mount Outside Diameter = $D_{mnt} := 2.375$ in
 Number of Mounting Pipes = $N_{mnt} := 3$
 Tri Sector Adapter Mount Weight = $W_{tsa.mnt} := 20$ lbs



Wind Load (NESC Extreme)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area =

$A_{mnt} := 0.0$ sf

Total Mount Wind Force =

$F_{mnt} := qz \cdot C_d \cdot F \cdot A_{mnt} \cdot m = 0$ lbs **BLC 5**

Wind Load (NESC Heavy)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area w/ Ice =

$A_{ICEmnt} := 0.0$ sf

Total Mount Wind Force =

$F_{mnt} := p \cdot C_d \cdot F \cdot A_{ICEmnt} = 0$ lbs **BLC 4**

Gravity Loads (without ice)

Weight Each Pipe Mount =

$WT_{mnt} := W_{mnt} \cdot \frac{L_{mnt}}{12} = 20$ lbs

Weight of All Mounts =

$WT_{mnt} \cdot N_{mnt} + W_{tsa.mnt} = 80$ lbs **BLC 2**

Gravity Loads (ice only)

Volume of Each Pipe =

$V_{mnt} := \frac{\pi}{4} \cdot D_{mnt}^2 \cdot L_{mnt} = 292$ cu in

Volume of Ice on Each Pipe =

$V_{ice} := \left[\frac{\pi}{4} \cdot \left[(D_{mnt} + 1)^2 \right] \cdot (L_{mnt} + 1) \right] - V_{mnt} = 307$ cu in

Weight of Ice each mount (incl. hardware) =

$W_{ICEmnt} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 10$ lbs

Weight of Ice on All Mounts =

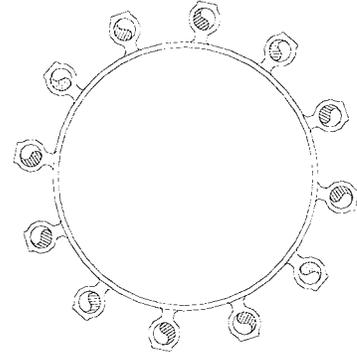
$W_{ICEmnt} \cdot N_{mnt} + 5 = 35$ lbs **BLC 3**

 <p>63-2 N. Branford Rd., Branford, CT 06405</p>	Subject:	Load Analysis of Existing PCS Mast on CL&P Structure #1102
	Location:	Norwalk, CT
	Rev. 1: 7/8/09	Prepared by: T.J.L Checked by: C.F.C. Job No. 08174.CO.5

Development of Wind & Ice Load on Coax Cables

Coax Cable Data:

Shape =	(T-Mobile)	Round
Coax Cable Length =	$L_{coax} := 21$	ft
Coax Type =	HELIX 1-1/4" Φ	
Coax Outside Diameter =	$D_{coax} := 1.55$	in
Weight of Coax per foot =	$Wt_{coax} := 0.66$	plf
Total Number of Coax =	$N_{coax} := 12$	
No. of Coax Projecting Outside Face of PCS Mast =	$NP_{coax} := 2$	



Wind Load (NESC Extreme)

Coax projected surface area =	$A_{coax} := \frac{(NP_{coax} D_{coax} + D_{mast})}{12} = 1.3$	sq ft/ft
Total Coax Wind Force (Above NU Structure) =	$F_{coax} := qz C_d C_{coax} A_{coax} m = 77$	plf BLC 5

Wind Load (NESC Heavy)

Coax projected surface area w/ Ice =	$A_{ICE_{coax}} := \frac{(NP_{coax} D_{coax} + D_{mast} + 2 \cdot lr)}{12} = 1.4$	sq ft/ft
Total Coax Wind Force w/ Ice =	$F_{i_{coax}} := p \cdot C_d C_{coax} A_{ICE_{coax}} = 8$	plf BLC 4

Gravity Loads (without ice)

Weight of all cables w/o ice	$WT_{coax} := Wt_{coax} \cdot N_{coax} = 8$	plf BLC 2
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Gravity Loads (ice only)

Ice Area per Linear Foot =	$A_{i_{coax}} := \frac{\pi}{4} [(D_{coax} + 2 \cdot lr)^2 - D_{coax}^2] = 3.2$	sq in
Ice Weight All Coax per foot =	$WT_{i_{coax}} := N_{coax} \cdot Id \cdot \frac{A_{i_{coax}}}{144} = 15$	plf BLC 3



Subject:

Load Analysis of Proposed PCS Mast on CL&P Structure #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L Checked by: C.F.C. Job No. 08174.CO.5

Basic Components

Heavy Wind Pressure = $p := 4.00$ psf
 Basic Windspeed = $V := 110$ mph (NES 2007 Figure 250-1 & Table 250-1)
 Radial Ice Thickness = $Ir := 0.50$ in (NES 2007 Figure 250-2(e))
 Radial Ice Density = $Id := 56.0$ pcf

Factors for Extreme Wind Calculation

Elevation of Top of PCS Mast Above Grade = $TME := 117$ ft
 Multiplier Gust Response Factor = $m := 1.25$
 NES Factor = $kv := 1.43$
 Importance Factor = $I := 1.0$ (Only for NES Extreme case NU criteria)
 (NES 2007 Table 250-3 equation)
 (NES Section 250.C.2)

Velocity Pressure Coefficient = $Kz := 2.01 \cdot \left(0.67 \cdot \frac{TME}{900}\right)^{\frac{2}{9.5}} = 1.202$ (NES 2007 Table 250-2)

Exposure Factor = $Es := 0.346 \left[\frac{33}{(0.67 \cdot TME)} \right]^{\frac{1}{7}} = 0.306$ (NES 2007 Table 250-3)

Response Term = $Bs := \frac{1}{\left(1 + 0.375 \cdot \frac{TME}{220}\right)} = 0.834$ (NES 2007 Table 250-3)

Gust Response Factor = $Grf := \frac{1 + \left(2.7 \cdot Es \cdot Bs^{\frac{1}{2}}\right)}{kv^2} = 0.858$ (NES 2007 Table 250-3)

Wind Pressure = $qz := 0.00256 \cdot Kz \cdot V^2 \cdot Grf \cdot I = 31.9$ psf (NES 2007 Section 250.C.2)

Shape Factors

Shape Factor for Round Members = $CdR := 1.3$
 Shape Factor for Round Members = $CdF := 1.6$
 Shape Factor for Coax Cables Attached to Outside of Pole = $Cd_{coax} := 1.45$

NUS Design Criteria Issued April 12, 2007

Overload Factors

Overload Factors for Wind Loads:

NES Heavy Loading = 2.5
 NES Extreme Loading = 1.0

NU Design Criteria Table

Apply in Risa-3D Analysis
 Apply in Risa-3D Analysis

Overload Factors for Vertical Loads:

NES Heavy Loading = 1.5
 NES Extreme Loading = 1.0

Apply in Risa-3D Analysis
 Apply in Risa-3D Analysis

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on PCS Mast

PCS Mast Data:

Mast Shape = Round
 Mast Diameter = $D_{mast} := 12.8$ in (Pipe 12" SCH.80)
 Mast Length = $L_{mast} := 55$ ft
 Mast Thickness = $t_{mast} := 0.5$ in

Wind Load (NESC Extreme)

*Assumes Mast is Shielded by Coax Cable
Antennas and TMA's Top 32' of Mast*

Mast Projected Surface Area = $A_{mast} := \frac{D_{mast}}{12} = 1.067$ sq ft/ft
 Total Mast Wind Force (Below NU Structure) = $qz \cdot C_d \cdot R \cdot A_{mast} = 44$ plf **BLC 5**

Wind Load (NESE Heavy)

*Assumes Mast is Shielded by Coax Cable
Antennas and TMA's Top 32' of Mast*

Mast Projected Surface Area w/ Ice = $A_{ICE_{mast}} := \frac{(D_{mast} + 2 \cdot I_r)}{12} = 1.15$ sq ft/ft
 Total Mast Wind Force w/ Ice = $p \cdot C_d \cdot R \cdot A_{ICE_{mast}} = 6$ plf **BLC 4**

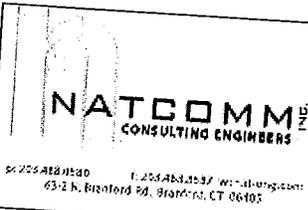
Gravity Loads (without ice)

Weight of the mast = Self Weight (Computed internally by Risa-3D) plf **BLC 1**

Gravity Loads (Ice only)

Ice Area per Linear Foot = $A_{i_{mast}} := \frac{\pi}{4} [(D_{mast} + I_r \cdot 2)^2 - D_{mast}^2] = 20.9$ sq in

Weight of Ice on Mast = $W_{ICE_{mast}} := I_d \cdot \frac{A_{i_{mast}}}{144} = 8$ plf **BLC 3**



Subject:

Load Analysis of Proposed PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

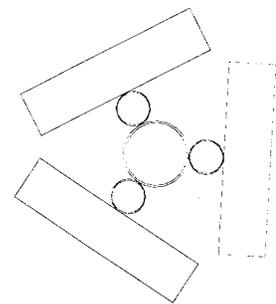
Rev. 1: 7/7/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on Antennas

Antenna Data:

(AT&T @ 104')
 Antenna Model = Powerwave 7770
 Antenna Shape = Flat
 Antenna Height = $L_{ant} := 55$ in
 Antenna Width = $W_{ant} := 11$ in
 Antenna Thickness = $T_{ant} := 5$ in
 Antenna Weight = $WT_{ant} := 35$ lbs
 Number of Antennas = $N_{ant} := 3$



Wind Load (NESC Extreme)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna = $SA_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 4.2$ sf
 Antenna Projected Surface Area = $A_{ant} := SA_{ant} \cdot N_{ant} = 12.6$ sf
 Total Antenna Wind Force = $F_{ant} := qz \cdot CdF \cdot A_{ant} \cdot m = 805$ lbs **BLC 5**

Wind Load (NESC Heavy)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna w/ Ice = $SA_{ICEant} := \frac{(L_{ant} + 1) \cdot (W_{ant} + 1)}{144} = 4.7$ sf
 Antenna Projected Surface Area w/ Ice = $A_{ICEant} := SA_{ICEant} \cdot N_{ant} = 14$ sf
 Total Antenna Wind Force w/ Ice = $F_{ant} := p \cdot CdF \cdot A_{ICEant} = 90$ lbs **BLC 4**

Gravity Load (without ice)

Weight of All Antennas = $WT_{ant} \cdot N_{ant} = 105$ lbs **BLC 2**

Gravity Load (ice only)

Volume of Each Antenna = $V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 3025$ cu in
 Volume of Ice on Each Antenna = $V_{ice} := (L_{ant} + 1) \cdot (W_{ant} + 1) \cdot (T_{ant} + 1) - V_{ant} = 1007$ cu in
 Weight of Ice on Each Antenna = $W_{ICEant} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 33$ lbs
 Weight of Ice on All Antennas = $W_{ICEant} \cdot N_{ant} = 98$ lbs **BLC 3**



Subject:

Load Analysis of Proposed PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

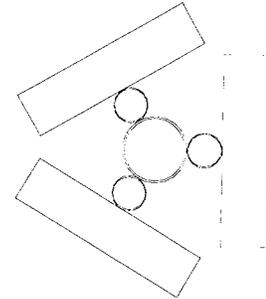
Rev. 1: 7/7/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on Antennas

Antenna Data:

(T-Mobile @ 114')
 Antenna Model = RFS APX16DWV-16DWVS-C-A20
 Antenna Shape = Flat
 Antenna Height = $L_{ant} := 55.9$ in
 Antenna Width = $W_{ant} := 13.3$ in
 Antenna Thickness = $T_{ant} := 3.15$ in
 Antenna Weight = $WT_{ant} := 40.7$ lbs
 Number of Antennas = $N_{ant} := 3$



Wind Load (NESC Extreme)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna = $SA_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 5.2$ sf
 Antenna Projected Surface Area = $A_{ant} := SA_{ant} \cdot N_{ant} = 15.5$ sf
 Total Antenna Wind Force = $F_{ant} := qz \cdot C_d \cdot F \cdot A_{ant} \cdot m = 990$ lbs **BLC 5**

Wind Load (NESC Heavy)

Assumes Maximum Possible Wind Pressure on Antennas

Surface Area for One Antenna w/ Ice = $SA_{ICEant} := \frac{(L_{ant} + 1)(W_{ant} + 1)}{144} = 5.7$ sf
 Antenna Projected Surface Area w/ Ice = $A_{ICEant} := SA_{ICEant} \cdot N_{ant} = 17$ sf
 Total Antenna Wind Force w/ Ice = $F_{ant} := p \cdot C_d \cdot F \cdot A_{ICEant} = 108$ lbs **BLC 4**

Gravity Load (without ice)

Weight of All Antennas = $WT_{ant} \cdot N_{ant} = 122$ lbs **BLC 2**

Gravity Load (ice only)

Volume of Each Antenna = $V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 2342$ cu in
 Volume of Ice on Each Antenna = $V_{ice} := (L_{ant} + 1)(W_{ant} + 1)(T_{ant} + 1) - V_{ant} = 1035$ cu in
 Weight of Ice on Each Antenna = $W_{ICEant} := \frac{V_{ice}}{1728} \cdot \rho_d = 34$ lbs
 Weight of Ice on All Antennas = $W_{ICEant} \cdot N_{ant} = 101$ lbs **BLC 3**

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

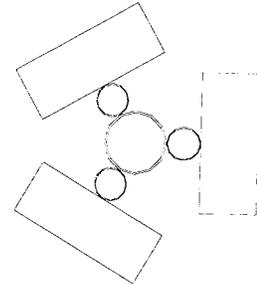
Rev. 1: 7/7/09

Prepared by: T.J.L. Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on TMA's

TMA Data:

	(AT&T @ 104')
TMA Model =	Powerwave LGP214
TMA Shape =	Flat
TMA Height =	$L_{TMA} := 9.2$ in
TMA Width =	$W_{TMA} := 14.4$ in
TMA Thickness =	$T_{TMA} := 2.6$ in
TMA Weight =	$W_{TMA} := 14.1$ lbs
Number of TMA's =	$N_{TMA} := 6$



Wind Load (NESC Extreme)

Assumes Maximum Possible Wind Pressure on TMA's

Surface Area for One TMA =	$SA_{TMA} := \frac{L_{TMA} \cdot W_{TMA}}{144} = 0.9$	sf
TMA Projected Surface Area =	$A_{TMA} := SA_{TMA} \cdot N_{TMA} = 5.5$	sf
Total TMA Wind Force =	$F_{TMA} := qz \cdot C_d \cdot A_{TMA} \cdot m = 353$	lbs BLC 5

Wind Load (NESC Heavy)

Assumes Maximum Possible Wind Pressure on TMA's

Surface Area for One TMA w/ Ice =	$SA_{ICETMA} := \frac{(L_{TMA} + 1) \cdot (W_{TMA} + 1)}{144} = 1.1$	sf
TMA Projected Surface Area w/ Ice =	$A_{ICETMA} := SA_{ICETMA} \cdot N_{TMA} = 6.5$	sf
Total TMA Wind Force w/ Ice =	$F_{i,TMA} := p \cdot C_d \cdot A_{ICETMA} = 42$	lbs BLC 4

Gravity Load (without ice)

Weight of All TMA's =	$W_{TMA} \cdot N_{TMA} = 85$	lbs BLC 2
-----------------------	------------------------------	------------------

Gravity Load (ice only)

Volume of Each TMA =	$V_{TMA} := L_{TMA} \cdot W_{TMA} \cdot T_{TMA} = 344$	cu in
Volume of Ice on Each TMA =	$V_{ice} := (L_{TMA} + 1) \cdot (W_{TMA} + 1) \cdot (T_{TMA} + 1) - V_{TMA} = 221$	cu in
Weight of Ice on Each TMA =	$W_{ICETMA} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 7$	lbs
Weight of Ice on All TMA's	$W_{ICETMA} \cdot N_{TMA} = 43$	lbs BLC 3

Subject:

Load Analysis of Proposed PCS Mast on CL&P Structure #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

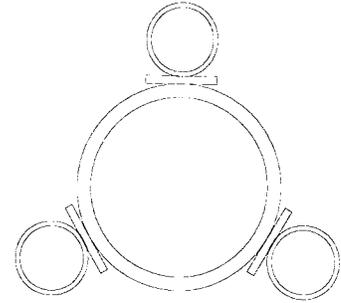
Prepared by: T.J.L Checked by: C.F.C. Job No. 08174.CO.5

Development of Wind & Ice Load on Antenna Mounts

Mount Data:

(AT&T @ 104')

Mount Type:	Microreflect Tri-Sector Adapter Mountw/ 3 Pipes
Mount Shape =	Round
Pipe Mount Length =	$L_{mnt} := 66$ in
2 inch Pipe Mount Linear Weight =	$W_{mnt} := 3.66$ plf
Pipe Mount Outside Diameter =	$D_{mnt} := 2.375$ in
Number of Mounting Pipes =	$N_{mnt} := 3$
Tri Sector Adapter Mount Weight =	$W_{tsa.mnt} := 20$ lbs



Wind Load (NESC Extreme)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area =	$A_{mnt} := 0.0$	sf
Total Mount Wind Force =	$F_{mnt} := qz \cdot C_d \cdot F \cdot A_{mnt} \cdot m = 0$	lbs BLC 5

Wind Load (NESC Heavy)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area w/ Ice =	$A_{ICEmnt} := 0.0$	sf
Total Mount Wind Force =	$F_{mnt} := p \cdot C_d \cdot F \cdot A_{ICEmnt} = 0$	lbs BLC 4

Gravity Loads (without ice)

(per TIA/EIA-222-F-1996)

Weight Each Pipe Mount =	$WT_{mnt} := W_{mnt} \cdot \frac{L_{mnt}}{12} = 20$	lbs
Weight of All Mounts =	$WT_{mnt} \cdot N_{mnt} + W_{tsa.mnt} = 80$	lbs BLC 2

Gravity Loads (ice only)

(per TIA/EIA-222-F-1996)

Volume of Each Pipe =	$V_{mnt} := \frac{\pi}{4} \cdot D_{mnt}^2 \cdot L_{mnt} = 292$	cu in
Volume of Ice on Each Pipe =	$V_{ice} := \left[\frac{\pi}{4} \cdot (D_{mnt} + 1)^2 \cdot (L_{mnt} + 1) \right] - V_{mnt} = 307$	cu in
Weight of Ice each mount (incl, hardware) =	$W_{ICEmnt} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 10$	lbs
Weight of Ice on All Mounts =	$W_{ICEmnt} \cdot N_{mnt} + 5 = 35$	lbs BLC 3

Subject:

Load Analysis of Proposed PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

Rev. 1: 7/7/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on Antenna Mounts

Mount Data:

(T-Mobile @ 114')

Mount Type:

Microfect Tri-Sector Adapter
Mountw/ 3 Pipes

Mount Shape =

Round

Pipe Mount Length =

$L_{mnt} := 66 \text{ in}$

2 inch Pipe Mount Linear Weight =

$W_{mnt} := 3.66 \text{ plf}$

Pipe Mount Outside Diameter =

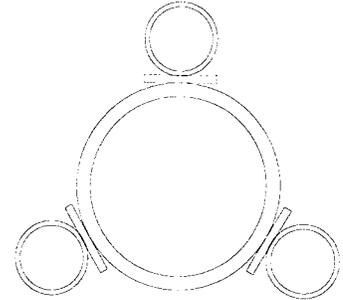
$D_{mnt} := 2.375 \text{ in}$

Number of Mounting Pipes =

$N_{mnt} := 3$

Tri Sector Adapter Mount Weight =

$W_{tsa.mnt} := 20 \text{ lbs}$



Wind Load (NESC Extreme)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area =

$A_{mnt} := 0.0 \text{ sf}$

Total Mount Wind Force =

$F_{mnt} := qz \cdot C_d F \cdot A_{mnt} \cdot m = 0 \text{ lbs BLC 5}$

Wind Load (NESC Heavy)

Assumes Mount is Shielded by Antenna

Mount Projected Surface Area w/ Ice =

$A_{ICEmnt} := 0.0 \text{ sf}$

Total Mount Wind Force =

$F_{mnt} := p \cdot C_d F \cdot A_{ICEmnt} = 0 \text{ lbs BLC 4}$

Gravity Loads (without ice)

(per TIA/EIA-222-F-1996)

Weight Each Pipe Mount =

$W_{Tmnt} := W_{mnt} \cdot \frac{L_{mnt}}{12} = 20 \text{ lbs}$

Weight of All Mounts =

$W_{Tmnt} \cdot N_{mnt} + W_{tsa.mnt} = 80 \text{ lbs BLC 2}$

Gravity Loads (ice only)

(per TIA/EIA-222-F-1996)

Volume of Each Pipe =

$V_{mnt} := \frac{\pi}{4} \cdot D_{mnt}^2 \cdot L_{mnt} = 292 \text{ cu in}$

Volume of Ice on Each Pipe =

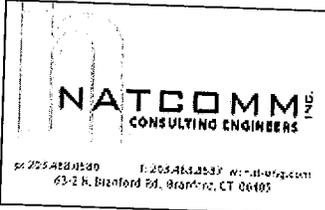
$V_{ice} := \left[\frac{\pi}{4} \cdot (D_{mnt} + 1)^2 \cdot (L_{mnt} + 1) \right] - V_{mnt} = 307 \text{ cu in}$

Weight of Ice each mount (incl. hardware) =

$W_{ICEmnt} := \frac{V_{ice}}{1728} \cdot \rho_{ice} = 10 \text{ lbs}$

Weight of Ice on All Mounts =

$W_{ICEmnt} \cdot N_{mnt} + 5 = 35 \text{ lbs BLC 3}$



Subject:

Load Analysis of Proposed PCS Mast on
CL&P Structure #1102

Location:

Norwalk, CT

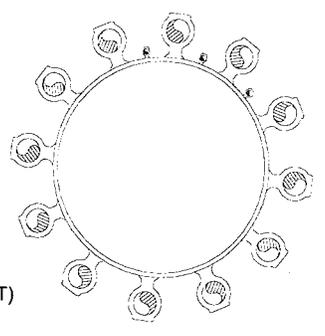
Rev. 1: 7/7/09

Prepared by: T.J.L Checked by: C.F.C. Job
No. 08174.CO.5

Development of Wind & Ice Load on Coax Cables

Coax Cable Data:

	(T-Mobile & AT&T)
Shape =	Round
Coax Cable Length =	$L_{coax} := 21$ ft
Coax Type =	HELIAX 1-1/4" ϕ
Coax Outside Diameter =	$D_{coax1} := 1.55$ in
Weight of Coax per foot =	$Wt_{coax1} := 0.66$ plf
Total Number of Coax =	$N_{coax1} := 12$ (6 T-Mobile 6 AT&T)
No. of Coax Projecting Outside Face of PCS Mast =	$NP_{coax1} := 2$
Coax Type =	HELIAX 1/2" ϕ
Coax Outside Diameter =	$D_{coax2} := 0.58$ in
Weight of Coax per foot =	$Wt_{coax2} := 0.25$ plf
Total Number of Coax =	$N_{coax2} := 3$ (3 AT&T)
No. of Coax Projecting Outside Face of PCS Mast =	$NP_{coax2} := 0$



Wind Load (NESC Extreme)

Coax projected surface area =	$A_{coax} := \frac{(NP_{coax1} \cdot D_{coax1} + D_{mast})}{12} = 1.3$	sq ft/ft
Total Coax Wind Force (Above NU Structure) =	$F_{coax} := qz \cdot Cd_{coax} \cdot A_{coax} \cdot m = 77$	plf BLC 5

Wind Load (NESC Heavy)

Coax projected surface area w/ Ice =	$A_{ICE_{coax}} := \frac{(NP_{coax1} \cdot D_{coax1} + D_{mast} + 2 \cdot lr)}{12} = 1.4$	sq ft/ft
Total Coax Wind Force w/ Ice =	$F_{i_{coax}} := p \cdot Cd_{coax} \cdot A_{ICE_{coax}} = 8$	plf BLC 4

Gravity Loads (without Ice)

Weight of all cables w/o ice	$WT_{coax} := Wt_{coax1} \cdot N_{coax1} + Wt_{coax2} \cdot N_{coax2} = 9$	plf BLC 2
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Gravity Loads (ice only)

Ice Area per Linear Foot =	$A_{i_{coax}} := \frac{\pi}{4} [(D_{coax1} + 2 \cdot lr)^2 - D_{coax1}^2] = 3.2$	sq in
Ice Weight All Coax per foot =	$WT_{i_{coax}} := N_{coax1} \cdot ld \cdot \frac{A_{i_{coax}}}{144} = 15$	plf BLC 3

NATCOMM, INC.
Consulting Engineers

63-2 North Branford Road
Branford, CT 06405

Ph. 203-488-0580 / Fax. 203-488-8587

Subject: **Analysis of NESC Heavy Wind and NESC Extreme
Wind for Obtaining PCS Mast Reactions Applied to CL&P Tower
Tabulated Load Cases**

Location: **Norwalk, CT**

Date: 3/23/09

Prepared by: T.J.L.

Checked by: C.F.C.

Job No. 08174.CO.5

Load Case

Description

- | Load Case | Description |
|-----------|--|
| 1 | Self Weight (PCS Mast) |
| 2 | Weight of Antennas, TMA's, Mounts, Coax Cables |
| 3 | Weight of Ice Only on PCS Structure ⁽¹⁾ |
| 4 | NESC Heavy Wind on PCS Structure |
| 5 | NESC Extreme Wind on PCS Structure |

Footnotes:

(1) PCS Structure includes: PCS Mast, Antennas, TMA's, Mounts, Coax Cable

NATCOMM, INC.
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 63-2 North Branford Road
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**Subject: Analysis of NESc Heavy Wind and NESc Extreme
 Wind for Obtaining PCS Mast Reactions Applied to CL&P Tower
 Load Combinations Table**
Location: Norwalk, CT

Date: 3/23/09 Prepared by: T.J.L. Checked by: C.F.C. Job No. 08174.CO.5

Load Combination	Description	Envelope	Wind	Soultion	Factor	P-Delta	BLC	Factor								
1	NESC Heavy Wind on PCS Structure	1	1	1	1.5	2	1.5	3	1.5	4	2.5					
2	NESC Extreme Wind on PCS Structure	1	1	1	1	2	1	5	1							

Footnotes:
 (1) BLC = Basic Load Case
 (2) PCS Structure includes: mast, antennas, tma's, mounts, coax cable, and miscellaneous hardware

Global

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation	Yes
Include Warping	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Vertical Axis	Y
Hot Rolled Steel Code	AISC: ASD 9th
Cold Formed Steel Code	AISI 99: ASD
Wood Code	NDS 91/97: ASD
Wood Temperature	< 100F
Concrete Code	ACI 2002
Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	PCA Load Contour
Parame Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections	Yes
Bad Framing Warnings	No
Unused Force Warnings	Yes

Hot Rolled Steel Properties

	Label	E [ksj]	G [ksj]	Nu	Therm (1E5 F)	Density[k/ft^3]	Yield[ksj]
1	A572 Gr.50	29000	11154	.3	.65	.49	50
2	A992	29000	11154	.3	.65	.49	50
3	A500 Gr.42	29000	11154	.3	.65	.49	50
4	A500 Gr. C	29000	11154	.3	.65	.49	42
5	A53 Gr. B	29000	11154	.3	.65	.49	50
							35

Hot Rolled Steel Design Parameters

	Label	Shape	Lengt...	Lbyy[ft]	Lbzz[ft]	Lcomp top[ft]	Lcomp bot[ft]	Kyy	Kzz	Cm-yy	Cm-...	Cb	y sw...	z sw...	Function
1	M1	MASt	55												Lateral

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Rules	A [in2]	Iyy [in4]	Izz [in4]	J [in4]
1	MASt	PIPE_12.0X	Column	Pipe	A53 Gr. B	Typical	17.9	339	339	678

Member Primary Data

	Label	I Joint	J Joint	K ...	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	BOTTOM_CONN...	TOPOFM...			MASt	Column	Pipe	A53 Gr. B	Typical

Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia...
1	BOTTOM_CONNECTION	0	0	0	0	
2	TOP_CONNECTION	0	21.5	0	0	
3	FLANGE_CONNECTION	0	33	0	0	
4	ANTENNA_CL1	0	52	0	0	
5	TOPOFMAST	0	55	0	0	

Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]	Footing
1	BOTTOM_CONN...	Reaction	Reaction	Reaction				
2	TOP_CONNECTI...	Reaction	Reaction	Reaction				
3	FLANGE CONNE...							
4	ANTENNA CL1							
5	TOPOFMAST							

Joint Loads and Enforced Displacements (BLC 2 : Weight of PCS Structure)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1	ANTENNA CL1	L	Y	
2	ANTENNA CL1	L	Y	-0.119
3	ANTENNA CL1	L	Y	-0.09
				-0.08

Joint Loads and Enforced Displacements (BLC 3 : Weight of Ice Only on PCS Struct)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1	ANTENNA CL1	L	Y	
2	ANTENNA CL1	L	Y	-0.093
3	ANTENNA CL1	L	Y	-0.043
				-0.035

Joint Loads and Enforced Displacements (BLC 4 : NESC Heavy Wind)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1	ANTENNA CL1	L	X	.1
2	ANTENNA CL1	L	X	.042

Joint Loads and Enforced Displacements (BLC 5 : NESC Extreme Wind)

	Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...
1	ANTENNA CL1	L	X	.91
2	ANTENNA CL1	L	X	.353

Member Distributed Loads (BLC 2 : Weight of PCS Structure)

	Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...	Start Location[ft,%]	End Location[ft,%]
1	M1	Y	-0.008	-0.008	23	52

Member Distributed Loads (BLC 3 : Weight of Ice Only on PCS Struct)

	Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...	Start Location[ft,%]	End Location[ft,%]
1	M1	Y	-0.008	-0.008	0	0
2	M1	Y	-0.015	-0.015	23	52

Member Distributed Loads (BLC 4 : NESC Heavy Wind)

	Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...	Start Location[ft,%]	End Location[ft,%]
1	M1	X	.006	.006	0	23
2	M1	X	.008	.008	23	50

Member Distributed Loads (BLC 5 : NESC Extreme Wind)

	Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...	Start Location[ft,%]	End Location[ft,%]
1	M1	X	.044	.044	0	23
2	M1	X	.077	.077	23	50

Basic Load Cases

BLC Description	Category	X Gra...	Y Grav...	Z Gra...	Joint	Point Distributed Area (Mem...	Surfa...
1 Self Weight (PCS Mast)	None		-1				
2 Weight of PCS Structure	None						
3 Weight of Ice Only on PCS Struct	None				3	1	
4 NESC Heavy Wind	None				3	2	
5 NESC Extreme Wind	None				2	2	

Load Combinations

Description	Solve	PD...	SR...	BLCFa...							
1 NESC Heavy Wind on PCS Mast and...	Yes			1	1.5	2	1.5	3	1.5	4	2.5
2 NESC Extreme Wind on PCS Mast a...	Yes			1	1	2	1	5	1		
3 Self Weight				1	1						

Envelope Member Section Forces

Member	Sec		Axial[k]	lc	y Shear[k]	lc	z Shear[k]	lc	Torque[k-ft]	lc	y-y Mome...	lc	z-z Momen...	lc
1	M1	1	max	1.111	1	-.72	1	0	1	0	1	0	1	0
2			min	.655	2	-2.771	2	0	1	0	1	0	1	0
3		2	max	-.183	2	-.926	1	0	1	0	1	0	1	42.267
4			min	-.31	1	-3.376	2	0	1	0	1	0	1	11.316
5		3	max	4.378	1	2.996	2	0	1	0	1	0	1	50.434
6			min	2.16	2	.805	1	0	1	0	1	0	1	13.76
7		4	max	2.482	1	1.937	2	0	1	0	1	0	1	16.525
8			min	1.213	2	.53	1	0	1	0	1	0	1	4.582
9		5	max	0	1	0	1	0	1	0	1	0	1	0
10			min	0	1	0	1	0	1	0	1	0	1	0

Envelope Member Section Stresses

Member	Sec		Axial[ksi]	lc	y Shear...	lc	z Shear...	lc	y-Top[ksi]	lc	y-Bot[ksi]	lc	z-Top[ksi]	lc	z-Bot[ksi]	lc
1	M1	1	max	.062	1	-.08	1	0	1	0	1	0	1	0	1	0
2			min	.037	2	-.31	2	0	1	0	1	0	1	0	1	0
3		2	max	-.01	2	-.103	1	0	1	-2.554	1	9.538	2	0	1	0
4			min	-.017	1	-.377	2	0	1	-9.538	2	2.554	1	0	1	0
5		3	max	.245	1	.335	2	0	1	-3.105	1	11.381	2	0	1	0
6			min	.121	2	.09	1	0	1	-11.381	2	3.105	1	0	1	0
7		4	max	.139	1	.216	2	0	1	-1.034	1	3.729	2	0	1	0
8			min	.068	2	.059	1	0	1	-3.729	2	1.034	1	0	1	0
9		5	max	0	1	0	1	0	1	0	1	0	1	0	1	0
10			min	0	1	0	1	0	1	0	1	0	1	0	1	0

Envelope Joint Reactions

Joint		X [k]	lc	Y [k]	lc	Z [k]	lc	MX [k-ft]	lc	MY [k-ft]	lc	MZ [k-ft]	lc
1	BOTTOM_CON...	max	2.771	2	1.111	1	0	1	0	1	0	1	0
2		min	.72	1	.655	2	0	1	0	1	0	1	0
3	TOP_CONNEC...	max	-1.96	1	6.264	1	0	1	0	1	0	1	0
4		min	-7.125	2	3.216	2	0	1	0	1	0	1	0
5	FLANGE_CON...	max	NC		NC		NC		NC		LOCKED		NC
6		min	NC		NC		NC		NC		LOCKED		NC
7	Totals:	max	-1.24	1	7.376	1	0	1					
8		min	-4.354	2	3.871	2	0	1					

Company : Natcomm Inc
 Designer : tj / cfc
 Job Number : 08174-CO.5

Existing Mast on CL&P Tower # 1102

July 8, 2009
 9:44 AM
 Checked By: _____

Envelope Joint Displacements

Joint	X [in]	lc	Y [in]	lc	Z [in]	lc	X Rotation...	lc	Y Rotation...	lc	Z Rotation ...	lc
1 BOTTOM_CO... max	0	1	0	2	0	1	0	1	0	1	3.364e-3	2
2 min	0	2	0	1	0	1	0	1	0	1	8.951e-4	1
3 TOP_CONNE... max	0	2	0	2	0	1	0	1	0	1	-1.906e-3	1
4 min	0	1	0	1	0	1	0	1	0	1	-7.086e-3	2
5 FLANGE_CO... max	1.649	2	0	2	0	1	0	1	0	1	-4.276e-3	1
6 min	.446	1	-.001	1	0	1	0	1	0	1	-1.578e-2	2
7 ANTENNA_CL1 max	5.921	2	-.001	2	0	1	0	1	0	1	-5.455e-3	1
8 min	1.607	1	-.002	1	0	1	0	1	0	1	-2.004e-2	2
9 TOPOFMAST max	6.643	2	-.001	2	0	1	0	1	0	1	-5.455e-3	1
10 min	1.803	1	-.002	1	0	1	0	1	0	1	-2.004e-2	2

Envelope AISC ASD Steel Code Checks

Member	Shape	Code Check	Loc[ft]	lc	Shear Check	Loc[ft]	lc	Fa	Ft	Fb	C	C	AS
1	M1 PIPE 12.0X	679	21.771	2	.030	21.198	2	6.4	21	23.1	1	6	85H1-2

Company : Natcomm Inc
 Designer : til / cfc
 Job Number : 08174-CO.5

Existing Mast on CL&P Tower # 1102

July 8, 2009
 9:47 AM
 Checked By: _____

Joint Reactions

LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	1 BOTTOM CONNECTION	.72	1.111	0	0	0	0
2	1 TOP CONNECTION	-1.96	6.264	0	0	0	0
3	1 FLANGE CONNECTION	NC	NC	NC	NC	0	0
4	1 Totals:	-1.24	7.376	0	NC	LOCKED	NC
5	1 COG (ft):	X: 0	Y: 31.149	Z: 0			

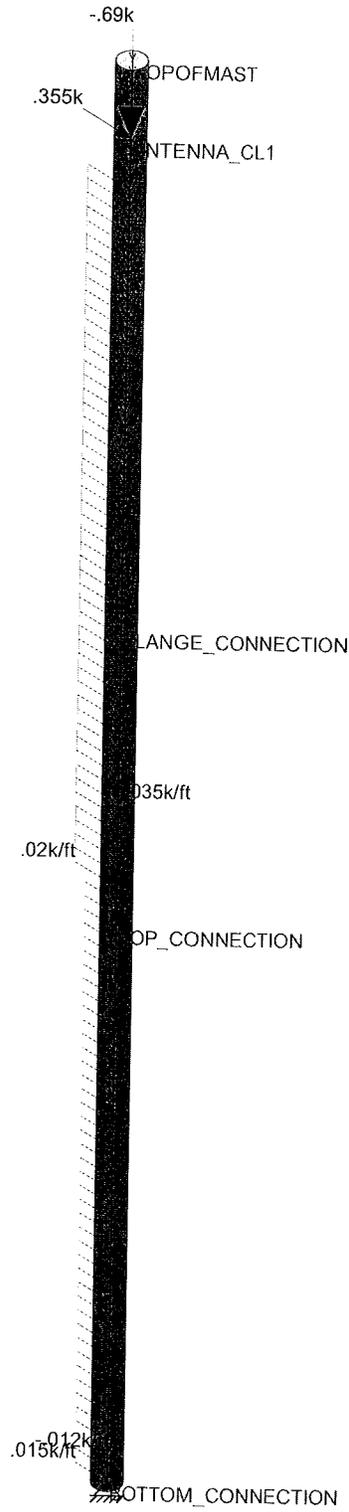
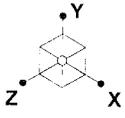
Company : Natcomm Inc
 Designer : tj / cfc
 Job Number : 08174-CO.5

Existing Mast on CL&P Tower # 1102

July 8, 2009
 9:48 AM
 Checked By: _____

Joint Reactions

LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	2	BOTTOM CONNECTION	2.771	.655	0	0	0
2	2	TOP CONNECTION	-7.125	3.216	0	0	0
3	2	FLANGE CONNECTION	NC	NC	NC	0	0
4	2	Totals:	-4.354	3.871	0	LOCKED	NC
5	2	COG (ft):	X: 0	Y: 29.928	Z: 0		



Loads: LC 1, NESC Heavy Wind on PCS Mast and PCS Structure

Natcomm Inc

Existing Mast on CL&P Tower # 1102

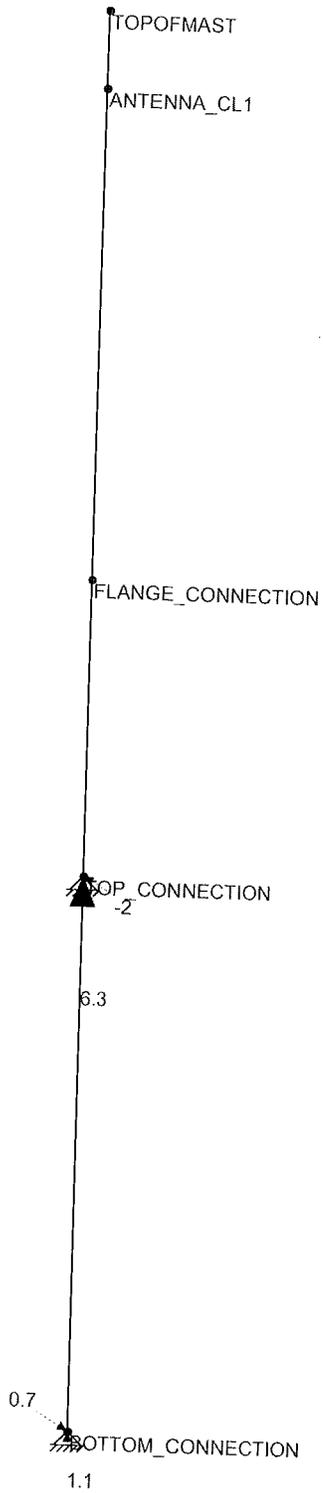
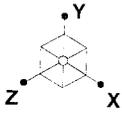
tjl / cfc

July 8, 2009 at 9:45 AM

08174-CO.5

LC # 1 Loads

Existing - Pipe Mast NESC.r3d



Results for LC 1, NESC Heavy Wind on PCS Mast and PCS Structure
Reaction units are k and k-ft

Natcomm Inc

tjl / cfc

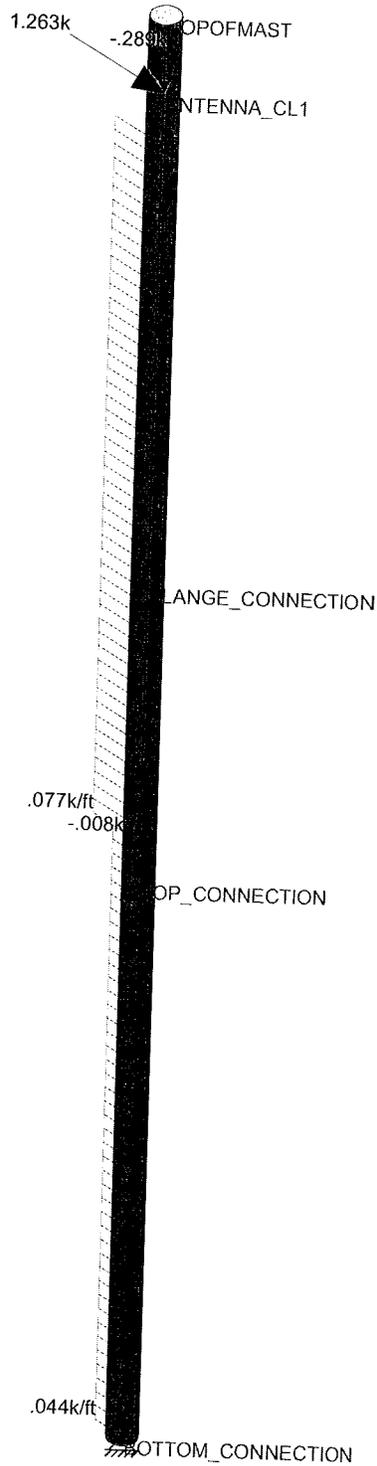
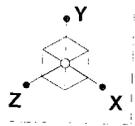
08174-CO.5

Existing Mast on CL&P Tower # 1102

LC # 1 Reactions

July 8, 2009 at 9:47 AM

Existing - Pipe Mast NESC.r3d



Loads: LC 2, NESC Extreme Wind on PCS Mast and PCS Structure

Natcomm Inc

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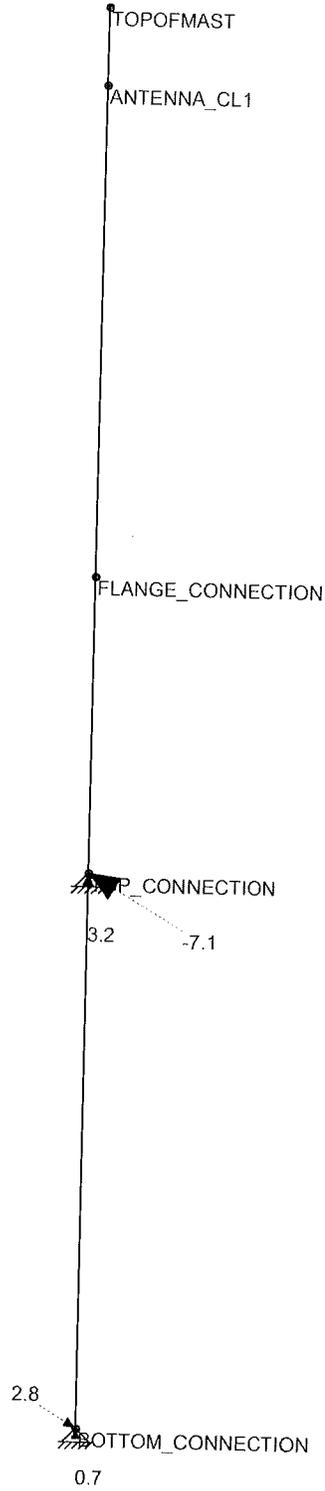
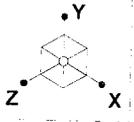
08174-CO.5

Existing Mast on CL&P Tower # 1102

LC # 2 Loads

July 8, 2009 at 9:46 AM

Existing - Pipe Mast NESC.r3d



Results for LC 2, NESC Extreme Wind on PCS Mast and PCS Structure
Reaction units are k and k-ft

Natcomm Inc

tjl / cfc

08174-CO.5

Existing Mast on CL&P Tower # 1102

LC # 2 Reactions

July 8, 2009 at 9:47 AM

Existing - Pipe Mast NESC.r3d

Global

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation	Yes
Include Warping	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Vertical Axis	Y
Hot Rolled Steel Code	AISC: ASD 9th
Cold Formed Steel Code	AISI 99: ASD
Wood Code	NDS 91/97: ASD
Wood Temperature	< 100F
Concrete Code	ACI 2002
Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	PCA Load Contour
Parame Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections	Yes
Bad Framing Warnings	No
Unused Force Warnings	Yes

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (1E5 F)	Density[k/ft^3]	Yield[ksi]
1	A572 Gr.50	29000	11154	.3	.65	.49	50
2	A992	29000	11154	.3	.65	.49	50
3	A500 Gr.42	29000	11154	.3	.65	.49	42
4	A500 Gr. C	29000	11154	.3	.65	.49	50
5	A53 Gr. B	29000	11154	.3	.65	.49	35

Hot Rolled Steel Design Parameters

Label	Shape	Lengt...	Lbyy[ft]	Lbzz[ft]	Lcomp top[ft]	Lcomp bot[ft]	Kyy	Kzz	Cm-yy	Cm-...	Cb	y sw...	z sw...	Function
1	M1	MASt	55											Lateral

Hot Rolled Steel Section Sets

Label	Shape	Type	Design List	Material	Design Rules	A [in2]	Iyy [in4]	Izz [in4]	J [in4]	
1	MASt	PIPE 12.0X	Column	Pipe	A53 Gr. B	Typical	17.9	339	339	678

Member Primary Data

Label	I Joint	J Joint	K...	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M1	BOTTOM CONN...	TOP OF...		MASt	Column	Pipe	A53 Gr. B	Typical

Joint Coordinates and Temperatures

Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia...
1	BOTTOM_CONNECTION	0	0	0	
2	TOP_CONNECTION	0	21.5	0	
3	FLANGE_CONNECTION	0	33	0	
4	ANTENNA_CL1	0	42	0	
5	ANTENNA_CL2	0	52	0	

Joint Coordinates and Temperatures (Continued)

Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia...
6 TOP_OF_MAST	0	55	0	0	

Joint Boundary Conditions

Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]	Footing
1 BOTTOM_CONN...	Reaction	Reaction	Reaction				
2 TOP_CONNECTI...	Reaction	Reaction	Reaction				
3 FLANGE CONNE...							
4 ANTENNA_CL1							
5 ANTENNA_CL2							

Joint Loads and Enforced Displacements (BLC 2 : Weight of PCS Structure)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...]
1 ANTENNA_CL1	L	Y	
2 ANTENNA_CL1	L	Y	-105
3 ANTENNA_CL1	L	Y	-085
4 ANTENNA_CL2	L	Y	-08
5 ANTENNA_CL2	L	Y	-122
			-08

Joint Loads and Enforced Displacements (BLC 3 : Weight of Ice Only on PCS Struct)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...]
1 ANTENNA_CL1	L	Y	
2 ANTENNA_CL1	L	Y	-098
3 ANTENNA_CL1	L	Y	-043
4 ANTENNA_CL2	L	Y	-035
5 ANTENNA_CL2	L	Y	-101
			-035

Joint Loads and Enforced Displacements (BLC 4 : NESG Heavy Wind)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...]
1 ANTENNA_CL1	L	X	
2 ANTENNA_CL1	L	X	.09
3 ANTENNA_CL2	L	X	.042
			.108

Joint Loads and Enforced Displacements (BLC 5 : NESG Extreme Wind)

Joint Label	L,D,M	Direction	Magnitude[(k,k-ft), (in,rad), (k*s^2/ft, k*ft...]
1 ANTENNA_CL1	L	X	
2 ANTENNA_CL1	L	X	.805
3 ANTENNA_CL2	L	X	.353
			.99

Member Distributed Loads (BLC 2 : Weight of PCS Structure)

Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...]	Start Location[ft,%]	End Location[ft,%]
1 M1	Y	-009	-009	23	52

Member Distributed Loads (BLC 3 : Weight of Ice Only on PCS Struct)

Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...]	Start Location[ft,%]	End Location[ft,%]
1 M1	Y	-008	-008	0	0
2 M1	Y	-015	-015	23	52

Member Distributed Loads (BLC 4 : NESG Heavy Wind)

Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,...]	Start Location[ft,%]	End Location[ft,%]
1 M1	X	.006	.006	0	23
2 M1	X	.008	.008	23	40

Member Distributed Loads (BLC 4 : NESC Heavy Wind) (Continued)

Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,deg]	Start Location[ft,%]	End Location[ft,%]
3 M1	X	.008	.008	44	50

Member Distributed Loads (BLC 5 : NESC Extreme Wind)

Member Label	Direction	Start Magnitude[k/ft,deg]	End Magnitude[k/ft,deg]	Start Location[ft,%]	End Location[ft,%]
1 M1	X	.044	.044	0	23
2 M1	X	.077	.077	23	40
3 M1	X	.077	.077	44	50

Basic Load Cases

BLC Description	Category	X Gra...	Y Grav...	Z Gra...	Joint	Point	Distributed Area (Mem... Surfa...
1 Self Weight (PCS Mast)	None						
2 Weight of PCS Structure	None		-1				
3 Weight of Ice Only on PCS Struct	None				5	1	
4 NESC Heavy Wind	None				5	2	
5 NESC Extreme Wind	None				3	3	

Load Combinations

Description	Solve	PD...	SR...	BLCFa...							
1 NESC Heavy Wind on PCS Mast and...	Yes			1	1.5	2	1.5	3	1.5	4	2.5
2 NESC Extreme Wind on PCS Mast a...	Yes			1	1	2	1	5	1		
3 Self Weight				1	1						

Envelope Member Section Forces

Member	Sec	Max/Min	Axial[k]	lc	y Shear[k]	lc	z Shear[k]	lc	Torque[k-ft]	lc	y-y Mome...	lc	z-z Momen...	lc
M1	1	max	1.111	1	-838	1	0	1	0	1	0	1	0	1
		min	.655	2	-3.195	2	0	1	0	1	0	1	0	1
	2	max	-.183	2	-1.044	1	0	1	0	1	0	1	0	1
		min	-.31	1	-3.8	2	0	1	0	1	0	1	48.086	2
	3	max	4.901	1	3.572	2	0	1	0	1	0	1	12.936	1
		min	2.368	2	.97	1	0	1	0	1	0	1	56.071	2
	4	max	2.984	1	2.61	2	0	1	0	1	0	1	15.303	1
		min	1.406	2	.72	1	0	1	0	1	0	1	14.167	2
	5	max	0	1	0	1	0	1	0	1	0	1	3.84	1
		min	0	1	0	1	0	1	0	1	0	1	0	1

Envelope Member Section Stresses

Member	Sec	Max/Min	Axial[ksj]	lc	y Shear...	lc	z Shear...	lc	y-Top[ksj]	lc	y-Bot[ksj]	lc	z-Top[ksj]	lc	z-Bot[ksj]	lc
M1	1	max	.062	1	-.094	1	0	1	0	1	0	1	0	1	0	1
		min	.037	2	-.357	2	0	1	0	1	0	1	0	1	0	1
	2	max	-.01	2	-.117	1	0	1	-2.919	1	10.851	2	0	1	0	1
		min	-.017	1	-.425	2	0	1	-10.851	2	2.919	1	0	1	0	1
	3	max	.274	1	.399	2	0	1	-3.453	1	12.653	2	0	1	0	1
		min	.132	2	.108	1	0	1	-12.653	2	3.453	1	0	1	0	1
	4	max	.167	1	.292	2	0	1	-.867	1	3.197	2	0	1	0	1
		min	.079	2	.08	1	0	1	-3.197	2	.867	1	0	1	0	1
	5	max	0	1	0	1	0	1	0	1	0	1	0	1	0	1
		min	0	1	0	1	0	1	0	1	0	1	0	1	0	1

Envelope Joint Reactions

Joint		X [k]	lc	Y [k]	lc	Z [k]	lc	MX [k-ft]	lc	MY [k-ft]	lc	MZ [k-ft]	lc
1 BOTTOM_CON...	max	3.195	2	1.111	1	0	1	0	1	0	1	0	1
	min	.838	1	.655	2	0	1	0	1	0	1	0	1
3 TOP_CONNEC...	max	-2.243	1	6.794	1	0	1	0	1	0	1	0	1
	min	-8.126	2	3.428	2	0	1	0	1	0	1	0	1
5 ANTENNA_CL1	max	NC		NC		NC		NC		0	1	0	1
	min	NC		NC		NC		NC		0	1	0	1
7 Totals:	max	-1.405	1	7.905	1	0	1	NC		LOCKED		NC	
	min	-4.931	2	4.083	2	0	1	NC		LOCKED		NC	

Envelope Joint Displacements

Joint		X [in]	lc	Y [in]	lc	Z [in]	lc	X Rotation...	lc	Y Rotation...	lc	Z Rotation ...	lc
1 BOTTOM_CO...	max	0	1	0	2	0	1	0	1	0	1	3.837e-3	2
	min	0	2	0	1	0	1	0	1	0	1	1.027e-3	1
3 TOP_CONNE...	max	0	2	0	2	0	1	0	1	0	1	-2.173e-3	1
	min	0	1	0	1	0	1	0	1	0	1	-8.045e-3	2
5 FLANGE_CO...	max	1.862	2	0	2	0	1	0	1	0	1	-4.81e-3	1
	min	.505	1	-.001	1	0	1	0	1	0	1	-1.771e-2	2
7 ANTENNA_CL1	max	3.982	2	0	2	0	1	0	1	0	1	-5.689e-3	1
	min	1.081	1	-.002	1	0	1	0	1	0	1	-2.093e-2	2
9 ANTENNA_CL2	max	6.562	2	-.001	2	0	1	0	1	0	1	-5.911e-3	1
	min	1.782	1	-.002	1	0	1	0	1	0	1	-2.175e-2	2
11 TOP_OF_MAST	max	7.346	2	-.001	2	0	1	0	1	0	1	-5.911e-3	1
	min	1.995	1	-.002	1	0	1	0	1	0	1	-2.175e-2	2

Envelope AISC ASD Steel Code Checks

Member	Shape	Code Check	Loc[ft]	lc	Shear Check	Loc[ft]	lc	Fa	Ft	Fb	C.C.	AS
1	M1 PIPE 12.0X	.767	21.771	2	.033	21.198	2	6.4	21	23.1	.6	.85H1-2

Company : Natcomm Inc
 Designer : tj / cfc
 Job Number : 08174-CO.5

Proposed Mast on CL&P Tower # 1102

July 8, 2009
 11:59 AM
 Checked By: _____

Joint Reactions

	LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	1	BOTTOM CONNECTION	.838	1.111	0	0	0	0
2	1	TOP CONNECTION	-2.243	6.794	0	0	0	0
3	1	ANTENNA CL1	NC	NC	NC	NC	LOCKED	NC
4	1	Totals:	-1.405	7.905	0			
5	1	COG (ft):	X: 0	Y: 31.619	Z: 0			

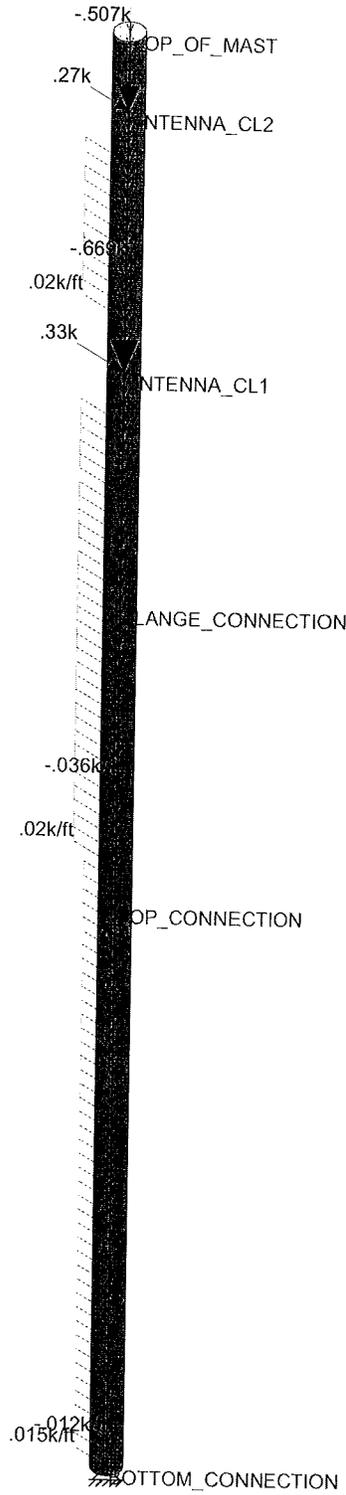
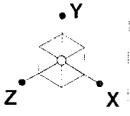
Company : Natcomm Inc
 Designer : tjl / cfc
 Job Number : 08174-CO.5

Proposed Mast on CL&P Tower # 1102

July 8, 2009
 11:59 AM
 Checked By: _____

Joint Reactions

LC	Joint Label	X [k]	Y [k]	Z [k]	MX [k-ft]	MY [k-ft]	MZ [k-ft]
1	2	BOTTOM CONNECTION	3.195	.655	0	0	0
2	2	TOP CONNECTION	-8.126	3.428	0	0	0
3	2	ANTENNA CL1	NC	NC	NC	0	0
4	2	Totals:	-4.931	4.083	0	NC	LOCKED
5	2	COG (ft):	X: 0	Y: 30.31	Z: 0		NC



Loads: LC 1, NESC Heavy Wind on PCS Mast and PCS Structure

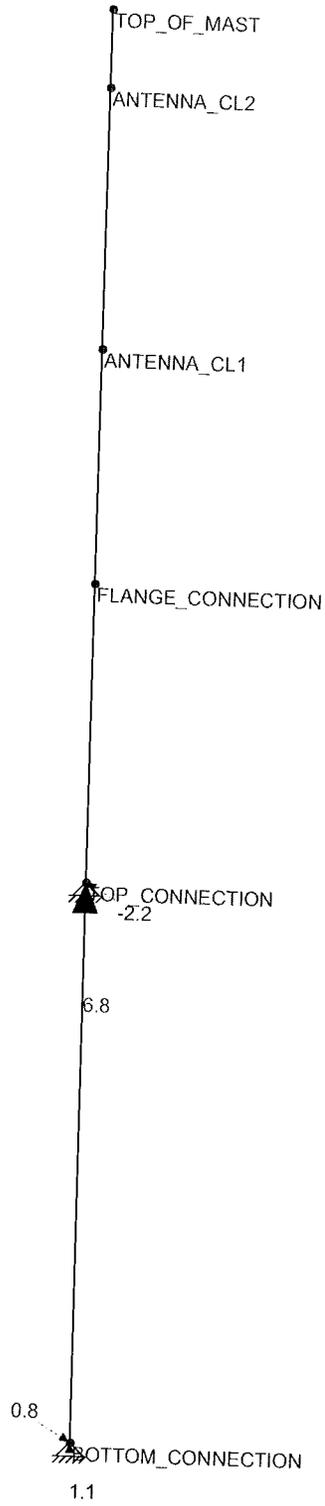
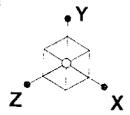
Natcomm Inc
 tjl / cfc
 08174-CO.5

Proposed Mast on CL&P Tower # 1102

LC # 1 Loads

July 8, 2009 at 11:58 AM

Proposed - Pipe Mast NESC.r3d



Results for LC 1, NESc Heavy Wind on PCS Mast and PCS Structure
 Reaction units are k and k-ft

Natcomm Inc

Proposed Mast on CL&P Tower # 1102

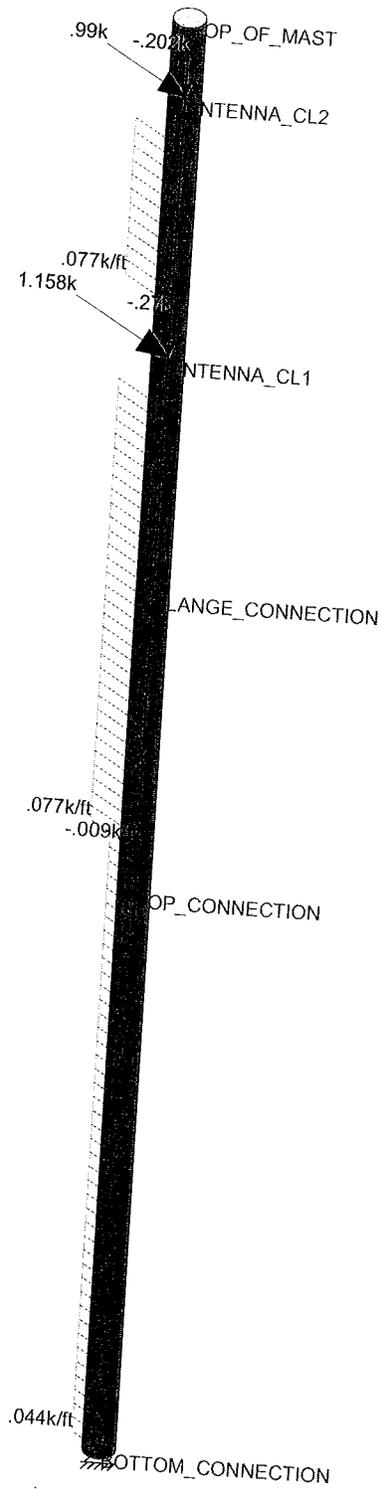
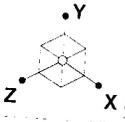
tjl / cfc

08174-CO.5

LC # 1 Reactions

July 8, 2009 at 11:59 AM

Proposed - Pipe Mast NESc.r3d



Loads: LC 2, NESC Extreme Wind on PCS Mast and PCS Structure

Natcomm Inc

Proposed Mast on CL&P Tower # 1102

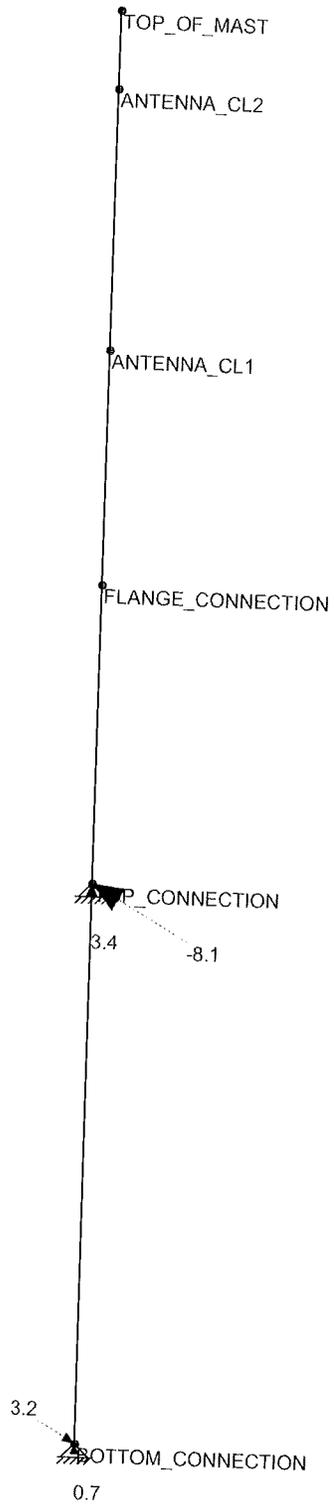
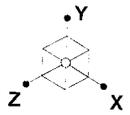
tjl / cfc

08174-CO.5

LC # 2 Loads

July 8, 2009 at 11:58 AM

Proposed - Pipe Mast NESC.r3d



Results for LC 2, NESC Extreme Wind on PCS Mast and PCS Structure
 Reaction units are k and k-ft

Natcomm Inc	Proposed Mast on CL&P Tower # 1102	July 8, 2009 at 11:59 AM
tjl / cfc		
08174-CO.5	LC # 2 Reactions	Proposed - Pipe Mast NESC.r3d



Subject:

Coax Cable Below Existing Mast on CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L Checked by: C.F.C.
Job No. 08174.CO.05

Coax Cable on CL&P Tower

Distance Between Coax Cable Attach Points =

Coaxial Cable Span
(from Top of Tower Down
Coax run on mast at 85' AGL
Coax attached to tower at 10' AGL) =

$$\text{CoaxSpan} := \begin{pmatrix} 10 \\ 10 \\ 10 \\ 10 \\ 15 \\ 20 \end{pmatrix} \text{ft} \quad (\text{User Input})$$

Coax Cable Type =	Helix 1-1/4" Φ	(User Input)
Diameter of Coax Cable =	$D_{\text{coax}} := 1.55\text{-in}$	(User Input)
Weight of Coax Cable =	$W_{\text{coax}} := 0.66\text{-plf}$	(User Input)
Number of Coax Cables =	$N_{\text{coax}} := 12$	(User Input) (T-Mobile)
Number of Coax Cables Projected =	$NP_{\text{coax}} := 6$	(User Input)
Extreme Wind Pressure =	$qz := 31.9\text{-psf}$	(User Input)
Heavy Wind Pressure =	$p := 4\text{-psf}$	(User Input)
Radial Ice Thickness =	$lr := 0.5\text{-in}$	(User Input)
Radial Ice Density =	$ld := 56\text{-pcf}$	(User Input)
Shape Factor =	$Cd_{\text{coax}} := 1.45$	(User Input)
Overload Factor for NESC Heavy Wind Load =	$OF_{\text{HW}} := 2.5$	(User Input)
Overload Factor for NESC Extreme Wind Load =	$OF_{\text{EW}} := 1.0$	(User Input)
Overload Factor for NESC Heavy Vertical Load =	$OF_{\text{HV}} := 1.5$	(User Input)
Overload Factor for NESC Extreme Vertical Load =	$OF_{\text{EV}} := 1.0$	(User Input)

Wind Area with Ice =

$$A_{\text{ice}} := (NP_{\text{coax}} \cdot D_{\text{coax}} + 2 \cdot lr) = 10.3\text{-in}$$

Wind Area without Ice =

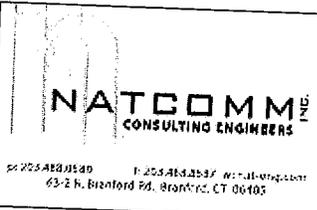
$$A := (NP_{\text{coax}} \cdot D_{\text{coax}}) = 9.3\text{-in}$$

Ice Area per Liner Ft =

$$A_{i_{\text{coax}}} := \frac{\pi}{4} \cdot [(D_{\text{coax}} + 2 \cdot lr)^2 - D_{\text{coax}}^2] = 0.022\text{ft}^2$$

Weight of Ice on All Coax Cables =

$$W_{i_{\text{ice}}} := A_{i_{\text{coax}}} \cdot ld \cdot N_{\text{coax}} = 15.027\text{-plf}$$



Subject:

Coax Cable Below Existing Mast on CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO.05

Heavy Vertical Load =

$$\text{HeavyVert} := \overrightarrow{[(N_{\text{coax}} \cdot W_{\text{coax}} + W_{\text{ice}}) \cdot \text{CoaxSpan} \cdot \text{OF}_{\text{HV}}]}$$

Heavy Transverse Load =

$$\text{HeavyTrans} := \overrightarrow{[p \cdot A_{\text{ice}} \cdot C_{d_{\text{coax}}} \cdot \text{CoaxSpan} \cdot \text{OF}_{\text{HW}}]}$$

$$\text{HeavyVert} = \begin{pmatrix} 344 \\ 344 \\ 344 \\ 344 \\ 516 \\ 688 \end{pmatrix} \text{ lb}$$

$$\text{HeavyTrans} = \begin{pmatrix} 124 \\ 124 \\ 124 \\ 124 \\ 187 \\ 249 \end{pmatrix} \text{ lb}$$

Extreme Vertical Load =

$$\text{ExtremeVert} := \overrightarrow{[N_{\text{coax}} \cdot W_{\text{coax}} \cdot \text{CoaxSpan} \cdot \text{OF}_{\text{EV}}]}$$

Extreme Transverse Load =

$$\text{ExtremeTrans} := \overrightarrow{[(qz \cdot A \cdot C_{d_{\text{coax}}}) \cdot \text{CoaxSpan} \cdot \text{OF}_{\text{EW}}]}$$

$$\text{ExtremeVert} = \begin{pmatrix} 79 \\ 79 \\ 79 \\ 79 \\ 119 \\ 158 \end{pmatrix} \text{ lb}$$

$$\text{ExtremeTrans} = \begin{pmatrix} 358 \\ 358 \\ 358 \\ 358 \\ 538 \\ 717 \end{pmatrix} \text{ lb}$$



Subject:

Coax Cable Below Proposed Mast on CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L Checked by: C.F.C.

Coax Cable on CL&P Tower

Distance Between Coax Cable Attach Points =

Coaxial Cable Span
(from Top of Tower Down
Coax run on mast at 85' AGL
Coax attached to tower at 10' AGL) =

$$\text{CoaxSpan} := \begin{pmatrix} 10 \\ 10 \\ 10 \\ 10 \\ 15 \\ 20 \end{pmatrix} \text{ft} \quad (\text{User Input})$$

Coax Cable Type = Helix 1-1/4" Φ (User Input)
 Diameter of Coax Cable = $D_{\text{coax1}} := 1.55\text{-in}$ (User Input)
 Weight of Coax Cable = $W_{\text{coax1}} := 0.66\text{-plf}$ (User Input)
 Number of Coax Cables = $N_{\text{coax1}} := 12$ (User Input) (6 T-Mobile 6 AT&T)
 Number of Coax Cables Projected = $NP_{\text{coax1}} := 6$ (User Input)

Coax Cable Type = Helix 1/2" Φ (User Input)
 Diameter of Coax Cable = $D_{\text{coax2}} := 0.58\text{-in}$ (User Input)
 Weight of Coax Cable = $W_{\text{coax2}} := 0.25\text{-plf}$ (User Input)
 Number of Coax Cables = $N_{\text{coax2}} := 3$ (User Input) (3 AT&T)
 Number of Coax Cables Projected = $NP_{\text{coax2}} := 0$ (User Input)

Extreme Wind Pressure = $qz := 31.9\text{-psf}$ (User Input)
 Heavy Wind Pressure = $p := 4\text{-psf}$ (User Input)
 Radial Ice Thickness = $Ir := 0.5\text{-in}$ (User Input)
 Radial Ice Density = $Id := 56\text{-pcf}$ (User Input)
 Shape Factor = $Cd_{\text{coax}} := 1.45$ (User Input)

Overload Factor for NESC Heavy Wind Load = $OF_{\text{HW}} := 2.5$ (User Input)
 Overload Factor for NESC Extreme Wind Load = $OF_{\text{EW}} := 1.0$ (User Input)
 Overload Factor for NESC Heavy Vertical Load = $OF_{\text{HV}} := 1.5$ (User Input)
 Overload Factor for NESC Extreme Vertical Load = $OF_{\text{EV}} := 1.0$ (User Input)

Subject:

Coax Cable Below Proposed Mast on
CL&P Tower #1102

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L Checked by: C.F.C.

Wind Area with Ice =

$$A_{ice} := (NP_{coax1} \cdot D_{coax1} + 2 \cdot lr) = 10.3 \text{ in}$$

Wind Area without Ice =

$$A := (NP_{coax1} \cdot D_{coax1}) = 9.3 \text{ in}$$

Ice Area per Liner Ft =

$$A_{i_{coax}} := \frac{\pi}{4} \cdot [D_{coax1} + 2 \cdot lr]^2 - D_{coax1}^2 = 0.022 \text{ ft}^2$$

Weight of Ice on All Coax Cables =

$$W_{ice} := A_{i_{coax}} \cdot ld \cdot N_{coax1} = 15.027 \text{ plf}$$

Heavy Vertical Load =

$$\text{HeavyVert} := [(N_{coax1} \cdot W_{coax1} + W_{ice}) \cdot \text{CoaxSpan} \cdot OF_{HV}]$$

Heavy Transverse Load =

$$\text{HeavyTrans} := (p \cdot A_{ice} \cdot C_{d_{coax}} \cdot \text{CoaxSpan} \cdot OF_{HW})$$

$$\text{HeavyVert} = \begin{pmatrix} 344 \\ 344 \\ 344 \\ 344 \\ 516 \\ 688 \end{pmatrix} \text{ lb}$$

$$\text{HeavyTrans} = \begin{pmatrix} 124 \\ 124 \\ 124 \\ 124 \\ 187 \\ 249 \end{pmatrix} \text{ lb}$$

Extreme Vertical Load =

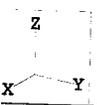
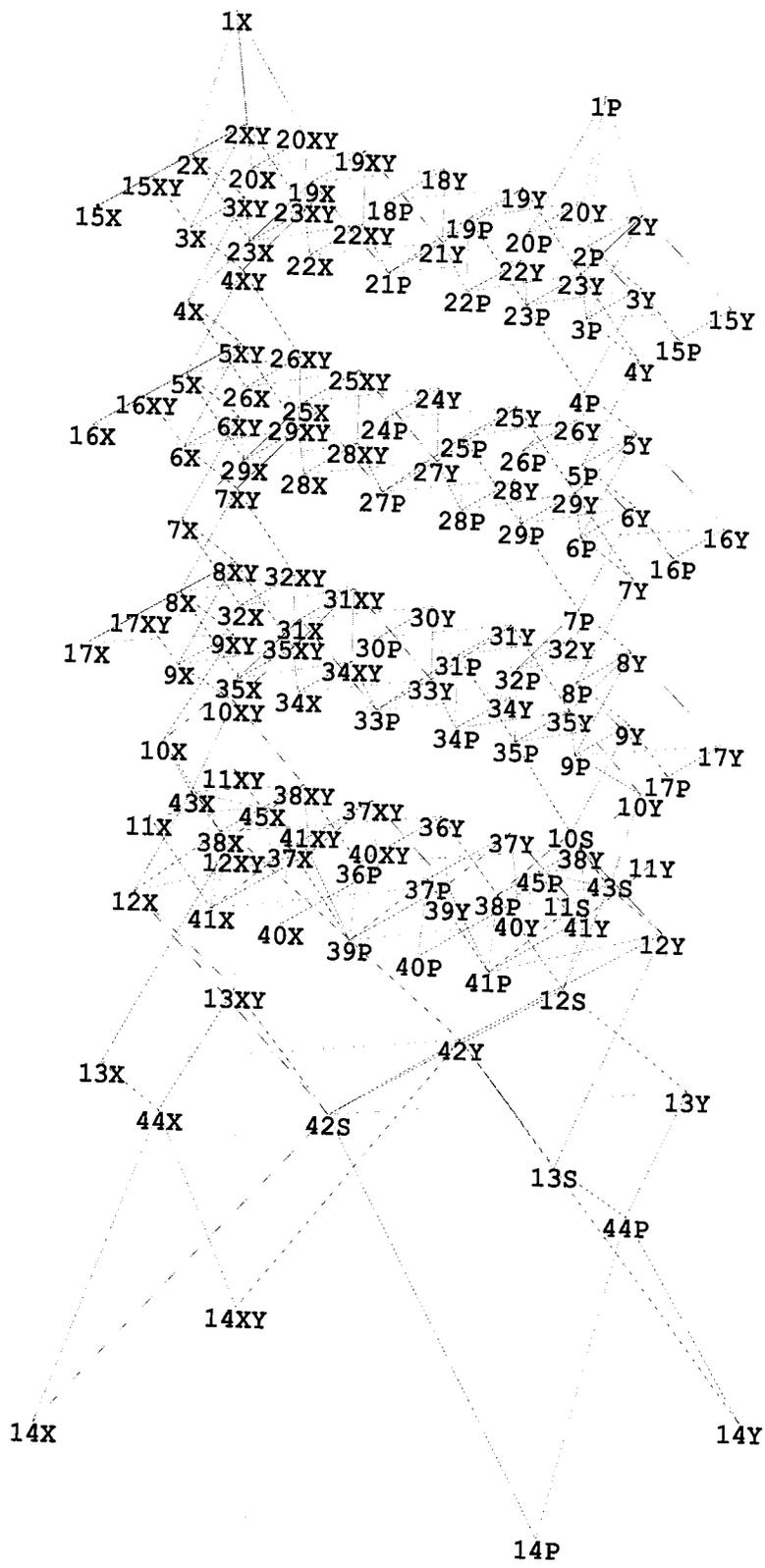
$$\text{ExtremeVert} := [(N_{coax1} \cdot W_{coax1} + N_{coax2} \cdot W_{coax2}) \cdot \text{CoaxSpan} \cdot OF_{EV}]$$

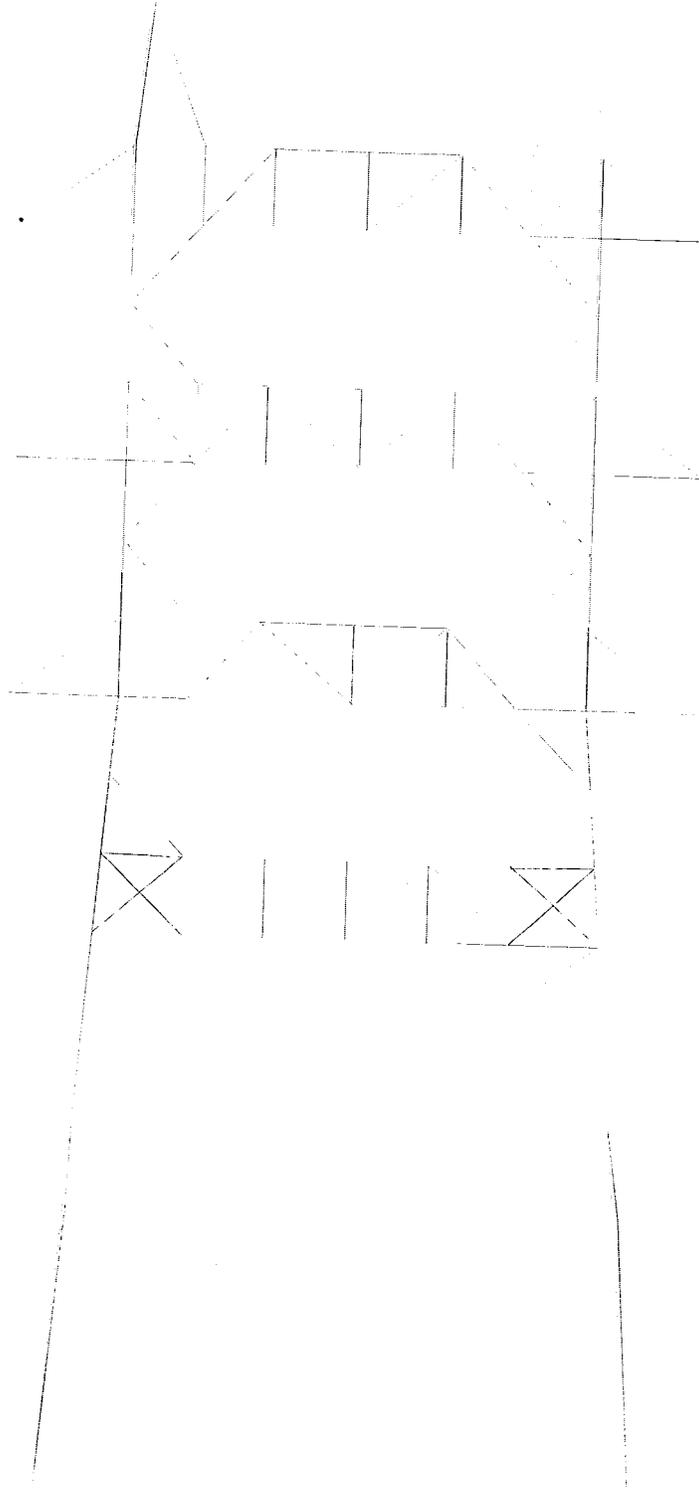
Extreme Transverse Load =

$$\text{ExtremeTrans} := [(qz \cdot A \cdot C_{d_{coax}}) \cdot \text{CoaxSpan} \cdot OF_{EW}]$$

$$\text{ExtremeVert} = \begin{pmatrix} 87 \\ 87 \\ 87 \\ 87 \\ 130 \\ 173 \end{pmatrix} \text{ lb}$$

$$\text{ExtremeTrans} = \begin{pmatrix} 358 \\ 358 \\ 358 \\ 358 \\ 538 \\ 717 \end{pmatrix} \text{ lb}$$





Z
X Y

Usage Legend	
■	0 ≤ % < 25
■	25 ≤ % < 50
■	50 ≤ % < 75
■	75 ≤ % < 100
■	100 ≤ %

Project Name : Nowalk Tower #1102
 Project Notes: T-MOBILE PCS
 Project File : J:\Jobs\0817400.WI - HPC-T-Mobile\CO05 - Ctl1356-Cl&P Tower - Rte 123\Engineering\Structural\Rev (1)\Calcs\Pls-Tower\norwalk1102.tow
 Date run : 11:36:05 AM Wednesday, July 08, 2009
 by : Tower Version 9.04
 Licensed to : Natcomm

Successfully performed nonlinear analysis

KL/R value of 213.20 exceeds maximum of 200.00 for member "94P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "94X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "96P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "96X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "101P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "109P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "117P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "125P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "126AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "126BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "127P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "127X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "128AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "128BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "129P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "129X" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "130AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "130BP" ??
 KL/R value of 223.50 exceeds maximum of 200.00 for member "131P" ??
 KL/R value of 223.50 exceeds maximum of 200.00 for member "132AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "132BP" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "133P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "133X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "134AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "134BP" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "135P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "135X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "136AP" ??
 KL/R value of 223.50 exceeds maximum of 200.00 for member "137P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "138AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "138BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "139P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "139X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "140AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "140BP" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "141P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "141X" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "142AP" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "142BP" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "144P" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "144X" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "144Y" ??
 KL/R value of 203.04 exceeds maximum of 200.00 for member "144Z" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "150P" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "151P" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "151X" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "151Y" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "151Z" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "154P" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "154X" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "154Y" ??
 KL/R value of 368.56 exceeds maximum of 200.00 for member "154Z" ??
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156P" ??
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156X" ??
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156Y" ??
 Clamp insulator "C33" has a structure attach joint "14X" that is fixed with respect to translation ??

Clamp insulator "C40" has a structure attach joint "14Y" that is fixed with respect to translation ??
 The model has 59 warnings. ??

Member check option: ASCE 10
 Connection rupture check: Not Checked
 Crossing diagonal check: Fixed

Loads from file: j:\jobs\0817400.wi - hpc-t-mobile\co05 - cttl1356-clsp tower - rte 123\engineering\structural\rev (1)\calcs\pis-tower\norwalk1102.lca
 *** Analysis Results:

Maximum element usage is 92.14% for Angle "156XY" in load case "NESC Broken Wire"
 Maximum insulator usage is 23.70% for Clamp "C5" in load case "NESC Broken Wire"

Summary of Joint Support Reactions For All Load Cases:

Load Case	Joint Label	Long. Force (kips)	Tran. Force (kips)	Vert. Force (kips)	Shear Force (kips)	Trans. Force (kips)	Long. Moment (ft-k)	Tran. Moment (ft-k)	Vert. Moment (ft-k)	Bending Moment (ft-k)	Found. Usage %
NESC Heavy	14P	23.13	-32.46	123.91	39.86	0.13	0.15	0.04	0.20	0.00	0.00
NESC Heavy	14X	14.36	-22.60	-66.21	26.77	0.31	0.03	-0.01	0.31	0.00	0.00
NESC Heavy	14Y	-14.25	-22.63	-64.94	26.74	0.34	-0.07	-0.01	0.35	0.00	0.00
NESC Extreme	14P	-21.67	-34.55	124.72	40.14	0.15	-0.21	-0.05	0.26	0.00	0.00
NESC Extreme	14X	20.45	-29.66	-92.79	36.03	0.36	0.10	0.01	0.38	0.00	0.00
NESC Extreme	14Y	-20.16	-30.25	-91.97	36.35	0.44	-0.07	-0.02	0.44	0.00	0.00
NESC Broken Wire	14P	21.37	-35.25	119.71	41.22	0.36	-0.25	-0.07	0.44	0.00	0.00
NESC Broken Wire	14X	-23.62	-36.67	-123.65	43.62	0.17	0.12	-0.01	0.21	0.00	0.00
NESC Broken Wire	14Y	9.33	-20.93	-58.34	22.91	0.44	0.13	-0.04	0.46	0.00	0.00
NESC Broken Wire	14X	-18.20	-22.71	-87.42	29.10	0.20	0.03	-0.03	0.20	0.00	0.00
NESC Broken Wire	14Y	21.23	-26.96	112.14	34.32	0.11	-0.28	-0.09	0.30	0.00	0.00

Summary of Joint Support Reactions For All Load Cases in Direction of Leg:

Load Case	Support Origin Joint	Leg Force In Member (kips)	Residual Shear (kips)	Horizontal Force (kips)	Total Horizontal Force (kips)	Residual Shear (kips)	Long. Moment (ft-k)	Total Long. Moment (ft-k)	Residual Shear (kips)	Total Shear Force (kips)			
NESC Heavy	14P	13S	128.238	22.316	22.379	-23.13	-32.46	123.91	17.289	14.36	-22.60	-66.21	
NESC Heavy	14X	13X	-69.313	17.207	17.432	-14.25	-22.63	-64.94	22.742	23.02	-22.63	-64.94	
NESC Heavy	14Y	13Y	-68.052	17.347	22.682	-21.67	-34.55	124.72	24.811	-21.67	-34.55	124.72	
NESC Extreme	14P	13S	129.040	24.750	24.811	-20.16	-30.25	-91.97	22.260	20.45	-29.66	-92.79	
NESC Extreme	14X	13X	-97.042	22.144	22.781	-23.62	-36.67	-123.65	25.541	21.37	-35.25	-119.71	
NESC Extreme	14Y	13Y	-96.231	22.781	25.481	-20.16	-30.25	-91.97	26.070	17.826	-23.62	-36.67	123.65
NESC Broken Wire	14P	13S	124.020	22.781	17.826	9.33	-20.93	-58.34	15.581	17.777	18.20	-22.71	-87.42
NESC Broken Wire	14X	13X	134.281	25.481	15.581	-18.20	-22.71	-87.42	17.830	21.23	-26.96	112.14	
NESC Broken Wire	14Y	13Y	-90.813	17.777	17.830	21.23	-26.96	112.14	17.830	21.23	-26.96	112.14	

Overturning Moment Summary For All Load Cases:

Load Case	Transverse Moment (ft-k)	Longitudinal Moment (ft-k)	Resultant Moment (ft-k)
NESC Heavy	7243.450	-27.144	7243.501
NESC Extreme	8096.535	-6.532	8096.538
NESC Broken Wire	7010.317	870.569	7064.165

*** Overall summary for all load cases - Usage = Maximum Stress / Allowable Stress
 Printed capacities do not include the strength factor entered for each loadcase.

Group Summary (Compression Portion):

Group Label	Group Desc.	Angle Type	Steel Size	Max Strength (ksi)	Max Usage %	Comp. Member	Comp. Force (kips)	Comp. Control Load Case	Comp. Capacity (kips)	L/R Comp. Capacity (kips)	Comp. Shear Capacity (kips)	Comp. Conn. Bearing Capacity (kips)	RLX	RLY	RLZ	L/R Length Member (ft)	Curve No.	No. Bolts	Comp. No.	Of Bolts
1	L1	SAE	2.5X2.5X0.1875	33.0	40.35	1Y	-7.122NESC	Broke	17.669	27.200	0.000	24.469	0.500	0.500	0.500	117.68	9.708	3	2	
2	L2	SAE	5X5X0.375	33.0	9.36	2XY	-9.974NESC	Heavy	106.517	0.000	0.000	0.000	1.000	1.000	1.000	60.61	5.000	1	0	
3	L3	SAE	5X5X0.375	33.0	14.96	3X	-15.940NESC	Broke	106.517	0.000	0.000	0.000	1.000	1.000	1.000	60.61	5.000	1	0	
4	L4	SAE	5X5X0.375	33.0	28.78	4P	-30.659NESC	Broke	106.517	0.000	0.000	0.000	1.000	1.000	1.000	60.61	5.000	1	0	
5	L5	SAE	5X5X0.375	33.0	24.75	5X	-26.358NESC	Broke	106.517	136.000	0.000	244.687	1.000	1.000	1.000	60.61	5.000	1	0	
6	L6	SAE	8X8X0.5	33.0	14.46	6X	-35.453NESC	Broke	245.252	0.000	0.000	0.000	1.000	1.000	1.000	37.74	5.000	1	0	
7	L7	SAE	8X8X0.5	33.0	23.49	7P	-57.613NESC	Broke	245.252	0.000	0.000	0.000	1.000	1.000	1.000	37.74	5.000	1	0	
8	L8	SAE	8X8X0.5	33.0	17.99	8X	-39.514NESC	Broke	312.662	0.000	0.000	0.000	1.000	1.000	1.000	37.74	5.000	1	0	
9	L9	SAE	8X8X0.5	50.0	14.14	9X	-44.203NESC	Broke	312.662	0.000	0.000	0.000	1.000	1.000	1.000	38.54	5.107	1	0	
10	L10	SAE	8X8X0.5	50.0	27.07	10P	-84.643NESC	Broke	312.662	0.000	0.000	0.000	1.000	1.000	1.000	38.54	5.107	1	0	
11	L11	SAE	8X8X0.5	50.0	25.31	11P	-79.126NESC	Broke	312.662	0.000	0.000	0.000	1.000	1.000	1.000	38.54	5.107	1	0	
12	L12	SAE	8X8X0.5	50.0	30.88	12P	-94.942NESC	Broke	307.458	0.000	0.000	0.000	1.000	1.000	1.000	43.67	11.573	1	0	
13	L13	SAE	8X8X0.5	50.0	31.58	13P	-96.407NESC	Broke	305.312	0.000	0.000	0.000	1.000	1.000	1.000	43.67	11.573	1	0	
14	PEAK	SAE	2.5X2.5X0.1875	33.0	46.99	14X	-4.871NESC	Broke	16.686	27.200	0.000	24.469	0.500	0.500	0.500	124.50	10.271	1	28	
15	TTTC	SAE	3X3X0.25	33.0	29.99	16X	-15.146NESC	Broke	32.243	0.000	0.000	0.000	1.000	1.000	1.000	91.22	4.500	3	2	
16	TTTC	SAE	3X3X0.25	33.0	46.99	16X	-15.146NESC	Broke	32.243	0.000	0.000	0.000	1.000	1.000	1.000	91.22	4.500	3	2	
17	ARMTT	SAE	4X4X0.25	33.0	40.98	20X	-11.146NESC	Broke	53.785	40.800	0.000	48.937	1.000	1.000	1.000	67.92	4.500	3	0	
18	MTTC	SAE	4X4X0.25	33.0	18.91	20X	-11.146NESC	Broke	53.785	40.800	0.000	48.937	1.000	1.000	1.000	67.92	4.500	3	0	
19	MTTC	SAE	4X4X0.25	33.0	68.27	22XY	-27.978NESC	Broke	50.000	40.800	0.000	81.562	1.000	1.000	1.000	105.66	7.000	3	0	
20	ARMTT	SAE	4X4X0.25	33.0	44.02	24XY	-31.806NESC	Broke	208.793	122.400	0.000	61.172	1.000	1.000	1.000	106.19	7.000	3	0	
21	BTTC	SAE	4X4X0.25	33.0	12.34	25P	-23.022NESC	Extre	146.334	27.200	27.200	293.625	1.000	1.000	1.000	39.62	5.250	3	0	
22	BTTC	SAE	4X4X0.25	33.0	71.18	28XY	-4.236NESC	Extre	57.974	68.000	54.400	24.469	1.000	1.000	1.000	58.19	5.722	3	0	
23	ARMTT	SAE	4X4X0.3125	33.0	40.12	28XY	-4.236NESC	Extre	57.974	68.000	54.400	24.469	1.000	1.000	1.000	58.19	5.722	3	0	
24	ARMTT	SAE	4X4X0.3125	33.0	70.50	28XY	-4.236NESC	Extre	57.974	68.000	54.400	24.469	1.000	1.000	1.000	58.19	5.722	3	0	
25	BTTC	SAE	4X4X0.3125	33.0	74.75	28XY	-4.236NESC	Extre	57.974	68.000	54.400	24.469	1.000	1.000	1.000	58.19	5.722	3	0	
26	BTTC	SAE	4X4X0.3125	33.0	76.47	30P	-21.002NESC	Extre	47.728	0.000	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	2	
27	W1	SAE	2X2X0.1875	33.0	15.23	30P	-21.002NESC	Extre	47.728	0.000	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	2	
28	W2	SAE	2X2X0.1875	33.0	30.95	34X	-5.002NESC	Extre	47.728	0.000	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	2	
29	W3	SAE	4X4X0.3125	33.0	40.12	36X	-5.002NESC	Extre	47.728	0.000	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	2	
30	W4	SAE	4X4X0.3125	33.0	70.50	40XY	-5.002NESC	Extre	47.728	0.000	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	2	
31	W5	SAE	4X4X0.25	33.0	74.75	40XY	-5.002NESC	Extre	47.728	0.000	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	2	
32	W6	SAU	4X3.5X0.25	33.0	76.47	61X	-25.193NESC	Broke	46.740	54.400	54.400	81.562	1.000	1.000	1.000	152.28	5.000	6	2	
33	W7	SAE	3.5X3.5X0.25	33.0	72.86	61X	-25.193NESC	Broke	46.740	54.400	54.400	81.562	1.000	1.000	1.000	152.28	5.000	6	2	
34	W8	SAE	3X3X0.1875	33.0	79.53	63P	-24.208NESC	Broke	32.946	40.800	40.800	65.250	1.000	1.000	1.000	101.54	6.727	3	4	
35	W9	SAE	3X3X0.3125	33.0	53.04	55X	-12.146NESC	Broke	33.327	27.200	27.200	48.937	1.000	1.000	1.000	101.54	6.727	3	4	
36	W10	SAU	3X2.5X0.25	33.0	52.88	59I	-15.866NESC	Extre	29.912	40.800	40.800	24.469	1.000	1.000	1.000	116.31	6.727	3	3	
37	W11	SAE	4X4X0.25	33.0	63.17	65P	-26.138NESC	Extre	26.226	27.200	27.200	61.172	1.000	1.000	1.000	137.05	6.727	3	2	
38	W12	SAE	3.5X3.5X0.25	33.0	49.58	70XY	-19.158NESC	Extre	41.379	54.400	54.400	65.250	1.000	1.000	1.000	137.05	6.727	3	2	
39	KB1	SAE	4X4X0.375	33.0	61.78	71Y	-29.572NESC	Extre	38.640	40.800	40.800	48.937	1.000	1.000	1.000	101.54	6.727	3	4	
40	KB2	SAE	4X4X0.375	33.0	74.06	49P	-36.526NESC	Broke	60.729	68.000	68.000	122.344	1.000	1.000	1.000	86.46	5.000	3	3	
41	KB3	SAE	3X3X0.3125	33.0	65.19	47P	-30.644NESC	Extre	41.379	54.400	54.400	122.344	1.000	1.000	1.000	102.44	6.727	3	4	
42	B1	BAR	2 x 0.1875	33.0	44.07	45P	-19.498NESC	Broke	29.912	40.800	40.800	65.250	1.000	1.000	1.000	101.54	6.727	3	5	
43	DB1	SAE	3.5X3X0.25	33.0	79.38	44Y	0.000	0.072	0.072	27.200	27.200	61.172	1.000	1.000	1.000	137.05	6.727	3	4	
44	DB2	DAE	4X3X0.4375	33.0	84.52	51X	-38.885NESC	Broke	48.988	54.400	54.400	24.469	1.000	1.000	1.000	137.05	6.727	6	3	
45	RB1	SAE	3X3X0.1875	33.0	9.75	52P	-6.546NESC	Broke	55.071	81.600	81.600	65.250	0.540	0.540	0.540	191.63	8.602	6	2	
46	X1	SAU	7X4X0.4375	33.0	9.58	53XY	-1.187NESC	Extre	12.168	40.800	40.800	171.281	0.250	0.250	0.250	144.77	19.905	6	2	
47	X2	SAE	2X2X0.1875	33.0	9.98	77P	-7.965NESC	Extre	128.184	149.600	149.600	36.703	0.500	0.500	0.500	189.13	30.734	5	3	
48	X3	SAE	2X2X0.1875	33.0	30.65	79X	-1.226NESC	Broke	12.292	27.200	27.200	34.015	0.500	0.500	0.500	172.60	17.145	5	3	
49	X4	SAE	3X3X0.3125	33.0	20.33	80XY	-7.926NESC	Broke	25.861	27.200	27.200	24.469	0.750	0.750	0.750	59.10	7.354	2	11	
50	X5	SAE	2.5X2.5X0.25	33.0	10.08	83XY	-8.097NESC	Broke	43.226	40.800	40.800	32.625	0.750	0.750	0.750	131.00	8.602	5	2	
51	D1	SAE	2.5X2.5X0.25	33.0	28.57	86X	-1.738NESC	Broke	21.099	27.200	27.200	32.625	0.750	0.750	0.750	105.12	8.602	2	3	
52	X14	SAU	2.5X2X0.1875	33.0	84.39	88P	-4.146NESC	Broke	14.513	27.200	27.200	61.172	1.000	1.000	1.000	128.74	9.407	5	2	
53	DB3	SAU	3X2X0.25	33.0	28.33	89P	-3.165NESC	Extre	3.750	27.200	27.200	24.469	1.000	1.000	1.000	163.28	8.110	5	2	
54	H1	SAE	3X3X0.1875	33.0	21.13	90Y	0.000	0.000	0.000	40.800	40.800	48.937	1.000	1.000	1.000	288.77	18.752	6	2	
55	H1	SAE	2.5X2.5X0.1875	33.0	13.59	93P	-0.054NESC	Broke	6.868	40.800	40.800	48.937	1.000	1.000	1.000	288.77	18.752	6	2	
56	H2	SAE	2X2X0.1875	33.0	11.59	93P	-1.547NESC	Extre	11.388	40.800	40.800	36.703	1.000	1.000	1.000	288.77	18.752	6	2	
57	H3	SAE	3.5X3.5X0.3125	33.0	8.07	96X	-0.945NESC	Extre	4.471	13.600	13.600	24.469	1.000	1.000	1.000	282.33	22.092	5	3	
58	H16	SAU	3.5X3X0.25	33.0	3.69	97P	-3.216NESC	Heavy	39.830	40.800	40.800	24.469	1.000	1.000	1.000	169.70	7.000	6	2	
59	H17	SAU	3.5X3X0.25	33.0	14.74	98X	-2.472NESC	Extre	35.037	40.800	40.800	12.234	1.000	1.000	1.000	213.20	7.000	6	2	
60	H18	SAU	3.5X3X0.25	33.0	46.39	99X	-2.516NESC	Extre	25.022	27.200	27.200	48.937	1.000	1.000	1.000	121.74	7.000	4	1	
61	H2	SAE	3.5X3.5X0.25	33.0	3.12	100X	-7.594NESC	Extre	16.369	40.800	40.800	32.625	1.000	1.000	1.000	102.97	5.415	3	3	
62	X7	SAE	2X2X0.1875	33.0	29.78	101P	-0.113NESC	Broke	4.471	13.600	13.600	48.937	1.000	1.000	1.000	137.77	12.744	5	2	
63	H5	SAE	2.5X2.5X0.25	33.0	25.13	118P	-3.070NESC	Broke	10.309	13.600	13.600	48.937	1.000	1.000	1.000	188.06	17.082	5	3	
64	X8	SAE																		

Group Label	Group Desc.	Angle Type	Steel Strength (ksi)	Max Usage %	Max In Member Tens. %	Force Control	Tension Section Capacity (kips)	Net Tens. Section Capacity (kips)	Shear Capacity (kips)	Conn. Tens. Bearing Capacity (kips)	Conn. Tens. Rupture Capacity (kips)	Length of Member (ft)	No. of Bolts	No. of Holes	Hole Diameter (in)
65	H1	SAE 2.5X2.5X0.1875	33.0	13.06	13.06	121P	-1.48NESC Extre	11.388	27.200	24.469	1.000	1.000	1.000	169.70	7.000
66	X8	SAE 2X2X0.25	33.0	20.75	20.75	122P	-2.82NESC Extre	16.440	13.600	16.312	0.750	0.500	0.500	127.70	8.322
67	X6	SAE 2X2X0.25	33.0	75.78	75.78	107X	-8.83NESC Extre	11.659	13.600	16.312	0.750	0.500	0.500	151.91	9.899
68	H4	SAU 3.5X2.5X0.25	33.0	36.70	36.70	108X	-4.91NESC Extre	36.936	13.600	16.312	0.750	0.500	0.500	77.21	7.000
69	H2	SAE 2.5X2.5X0.1875	33.0	34.97	34.97	131P	-1.56NESC Extre	4.471	13.600	12.234	1.000	1.000	1.000	213.20	7.000
70	D2	SAE 2.5X2.5X0.1875	33.0	17.21	1.03	132AP	-0.053NESC Extre	5.168	13.600	12.234	1.000	1.000	1.000	213.20	7.000
71	H2	SAE 2.5X2.5X0.1875	33.0	35.45	35.45	133X	-1.56NESC Extre	4.471	13.600	12.234	1.000	1.000	1.000	213.20	7.000
72	D2	SAE 2.5X2.5X0.1875	33.0	15.65	0.53	134BP	-0.034NESC Extre	6.344	13.600	12.234	1.000	1.000	1.000	213.20	7.000
73	H2	SAE 2.5X2.5X0.1875	33.0	79.28	79.28	129P	-3.545NESC Extre	4.471	13.600	12.234	1.000	1.000	1.000	213.20	7.000
74	D2	SAE 2.5X2.5X0.1875	33.0	15.52	1.55	130BP	-0.098NESC Extre	6.344	13.600	12.234	1.000	1.000	1.000	213.20	7.000
75	H10	SAE 3.5X3.5X0.25	33.0	7.15	0.00	143P	0.000	18.774	13.600	32.625	1.000	1.000	1.000	201.74	8.322
76	X10	SAE 2X2X0.1875	33.0	52.13	52.13	144X	-2.574NESC Extre	4.933	27.200	24.469	0.750	0.500	0.500	185.88	10.750
77	H9	SAE 2X2X0.1875	33.0	8.60	7.92	145X	-0.74NESC Extre	11.348	27.200	24.469	0.750	0.500	0.500	228.84	15.027
78	H13	SAE 3X3X0.25	33.0	16.08	16.08	146BX	0.000	29.570	40.800	48.937	1.000	1.000	1.000	108.95	5.375
79	X9	SAU 2.5X1.5X0.25	33.0	8.60	8.60	147Y	-1.82NESC Extre	11.348	40.800	48.937	0.500	0.500	0.500	163.54	7.587
80	X8	SAU 2.5X1.5X0.25	33.0	16.08	16.08	148Y	-0.684NESC Extre	3.237	27.200	24.469	0.750	0.500	0.500	255.02	12.666
81	H8	SAE 2X2X0.25	33.0	8.57	0.00	149X	0.000	11.417	13.600	12.234	0.750	0.500	0.500	192.88	12.666
82	H15	SAE 3X3X0.25	33.0	5.48	5.48	150P	-0.414NESC Extre	12.534	27.200	24.469	0.500	0.500	0.500	163.54	7.587
83	H14	SAE 2X2X0.1875	33.0	21.14	21.14	151Y	-0.684NESC Extre	3.237	13.600	12.234	0.750	0.500	0.500	255.02	12.666
84	H14	SAE 2X2X0.1875	33.0	3.57	3.57	152P	-0.066NESC Extre	5.462	13.600	12.234	0.750	0.500	0.500	192.88	12.666
85	H13	SAE 3X3X0.25	33.0	2.81	1.67	153X	-0.685NESC Extre	19.149	27.200	24.469	0.500	0.500	0.500	163.54	7.587
86	X11	SAE 2X2X0.1875	33.0	2.87	0.10	154Y	-0.075NESC Extre	4.513	13.600	12.234	0.750	0.500	0.500	192.88	12.666
87	H19	SAE 3X3X0.25	33.0	92.14	92.14	155P	-0.010NESC Extre	10.549	13.600	12.234	0.750	0.500	0.500	212.19	13.934
88	X13	SAE 2X2X0.1875	33.0	92.14	92.14	156XY	-1.378NESC Extre	1.496	13.600	12.234	0.500	0.500	0.500	171.97	17.082

Group Summary (Tension Portion):

Group Label	Group Desc.	Angle Type	Steel Strength (ksi)	Max Usage %	Max In Member Tens. %	Force Control	Tension Section Capacity (kips)	Net Tens. Section Capacity (kips)	Shear Capacity (kips)	Conn. Tens. Bearing Capacity (kips)	Conn. Tens. Rupture Capacity (kips)	Length of Member (ft)	No. of Bolts	No. of Holes	Hole Diameter (in)
1	L1	SAE 2.5X2.5X0.1875	33.0	40.35	17.56	1X	3.849NESC Extre	21.917	27.200	24.469	0.000	9.708	2	1.000	0.875
2	L2	SAE 5X5X0.375	33.0	9.36	5.48	2P	5.483NESC Extre	100.072	0.000	0.000	0.000	5.000	0	1.760	0.875
3	L3	SAE 5X5X0.375	33.0	14.96	4.10	3P	3.394NESC Extre	82.747	0.000	0.000	0.000	5.000	0	3.360	0.875
4	L4	SAE 5X5X0.375	33.0	28.78	19.33	4X	15.993NESC Extre	82.747	0.000	0.000	0.000	5.000	0	3.360	0.875
5	L5	SAE 5X5X0.375	33.0	24.75	4.10	5XY	3.112NESC Extre	75.817	136.000	244.687	0.000	5.000	0	3.360	0.875
6	L6	SAE 8X8X0.5	33.0	14.46	4.53	6XY	10.500NESC Extre	231.928	0.000	0.000	0.000	5.000	10	4.000	0.875
7	L7	SAE 8X8X0.5	33.0	23.49	21.20	7XY	49.175NESC Extre	198.000	0.000	0.000	0.000	5.000	0	1.650	0.875
8	L8	SAE 8X8X0.5	33.0	17.99	17.99	8XY	35.614NESC Extre	355.562	0.000	0.000	0.000	5.000	0	1.650	0.875
9	L9	SAE 8X8X0.5	50.0	14.14	10.92	9XY	38.870NESC Extre	300.000	0.000	0.000	0.000	5.000	10	4.000	0.875
10	L10	SAE 8X8X0.5	50.0	27.07	24.02	10XY	72.046NESC Extre	355.562	0.000	0.000	0.000	5.000	0	1.650	0.875
11	L11	SAE 8X8X0.5	50.0	25.31	21.05	11XY	63.140NESC Extre	300.000	0.000	0.000	0.000	5.000	0	1.650	0.875
12	L12	SAE 8X8X0.5	50.0	30.88	24.16	12XY	72.472NESC Extre	300.000	0.000	0.000	0.000	5.000	0	1.650	0.875
13	L13	SAE 8X8X0.5	50.0	31.58	22.29	13XY	66.855NESC Extre	300.000	0.000	0.000	0.000	5.000	0	1.650	0.875
14	PEAK	SAE 2.5X2.5X0.1875	33.0	29.98	29.98	14Y	6.571NESC Extre	21.917	27.200	24.469	0.000	10.271	2	1.000	0.875
15	TTC	SAE 3X3X0.25	33.0	46.99	46.05	17Y	12.527NESC Extre	36.271	27.200	24.469	0.000	10.271	2	1.000	0.875
16	TTC	SAE 3X3X0.25	33.0	40.98	37.08	19XY	13.499NESC Extre	36.271	27.200	24.469	0.000	10.271	2	1.000	0.875
17	ARMTC	SAE 4X4X0.25	33.0	18.91	6.99	39Y	1.902NESC Extre	51.121	27.200	32.625	0.000	4.500	2	1.000	0.875
18	MTC	SAE 4X4X0.25	33.0	68.27	64.41	22P	32.930NESC Extre	51.121	27.200	32.625	0.000	4.500	2	1.000	0.875
19	MTC	SAE 4X4X0.25	33.0	44.02	41.18	25X	21.053NESC Extre	51.121	27.200	32.625	0.000	4.500	2	1.000	0.875
20	ARMTC	SAE 4X4X0.25	33.0	12.94	4.28	40Y	1.747NESC Extre	51.121	27.200	32.625	0.000	4.500	2	1.000	0.875
21	BTC	SAE 4X4X0.3125	33.0	71.18	70.67	28P	44.633NESC Extre	49.952	40.800	48.937	0.000	4.500	0	1.000	0.875
22	BTC	SAE 4X4X0.3125	33.0	51.27	41.39	30XY	22.513NESC Extre	55.038	40.800	48.937	0.000	4.500	0	1.000	0.875
23	ARMTC	SAE 4X4X0.3125	33.0	12.19	4.66	41Y	1.900NESC Extre	61.697	40.800	48.937	0.000	4.500	0	1.000	0.875
24	BTC	SAE 4X4X0.3125	33.0	15.23	14.26	34P	30.967NESC Extre	21.917	40.800	48.937	0.000	4.500	0	1.000	0.875
25	BTC	SAE 8X8X0.5	33.0	30.95	30.95	38X	37.889NESC Extre	131.794	122.400	61.172	0.000	7.000	3	1.180	0.875
26	W1	SAE 6X6X0.5	33.0	40.77	33.29	58Y	5.389NESC Extre	16.214	293.625	61.172	0.000	5.250	3	1.180	0.875
27	W2	SAE 2X2X0.1875	33.0	40.12	35.77	73P	24.321NESC Extre	16.214	122.400	61.172	0.000	7.000	3	1.180	0.875
28	W3	SAE 4X4X0.375	33.0	40.12	35.77	73P	24.321NESC Extre	16.214	122.400	61.172	0.000	7.000	3	1.180	0.875
29	W4	SAE 4X4X0.3125	33.0	70.50	62.04	76P	21.826NESC Extre	70.324	24.469	24.469	0.000	5.722	9	3.000	0.875
30	W5	SAE 4X4X0.25	33.0	74.75	52.48	67P	33.749NESC Extre	63.159	68.000	24.469	0.000	5.000	2	1.000	0.875
31	W6	SAU 4X3.5X0.25	33.0	76.47	52.48	69XY	26.045NESC Extre	59.748	54.400	24.469	0.000	5.000	2	1.000	0.875
32	W7	SAE 3.5X3.5X0.25	33.0	72.86	48.32	61P	25.918NESC Extre	49.627	54.400	24.469	0.000	5.000	2	1.000	0.875
33	W8	SAE 3X3X0.1875	33.0	79.53	51.92	63XY	19.715NESC Extre	44.531	54.400	24.469	0.000	5.000	2	1.000	0.875
34	W9	SAE 3X3X0.3125	33.0	53.04	40.82	55P	12.703NESC Extre	43.696	40.800	24.469	0.000	6.727	4	1.230	0.875
35	W10	SAU 3X2.5X0.25	33.0	52.88	48.71	59X	16.655NESC Extre	27.500	40.800	24.469	0.000	6.727	3	1.420	0.875
36	W11	SAE 4X4X0.25	33.0	63.17	57.90	64P	13.249NESC Extre	44.745	40.800	24.469	0.000	6.727	2	1.000	0.875
						65X	27.570NESC Extre	47.613	27.200	24.469	0.000	6.727	2	1.000	0.875
									54.400	65.250	0.000	6.727	4	1.540	0.875

37	W12	SAE	3.5X3.5X0.25	46.93	70Y	19.147NESC Extre	43.696	40.800	48.937	0.000	5.000	3	1.000	0.875
38	W13	SAE	4X4X0.375	45.44	71XY	30.358NESC Extre	66.816	68.000	122.344	0.000	7.000	5	1.860	0.875
39	KB1	SAE	4X4X0.375	48.49	50P	32.975NESC Extre	75.197	68.000	122.344	0.000	7.066	5	1.000	0.875
40	KB2	SAE	4X4X0.25	60.81	47X	28.931NESC Extre	47.613	54.400	65.250	0.000	6.727	4	1.540	0.875
41	KB3	SAE	3X3X0.3125	33.0 65.19	47X	19.282NESC Extre	44.745	40.800	61.172	0.000	6.727	4	1.000	0.875
42	B1	BAR	2 x 0.1875	47.26	45XY	2.761NESC Extre	6.265	27.200	24.469	0.000	8.602	2	1.000	0.875
43	DB1	DAS	3.5X3X0.25	48.74	43P	26.514NESC Extre	72.542	54.400	65.250	0.000	19.905	2	1.000	0.875
44	DB2	DAS	4X3X0.4375	47.99	51Y	39.158NESC Extre	121.751	81.600	171.281	0.000	30.734	3	2.000	0.875
45	HB1	SAE	3X3X0.1875	5.64	52XY	1.852NESC Extre	27.500	40.800	36.703	0.000	17.145	3	2.000	0.875
46	X1	SAU	7X4X0.4375	9.58	53Y	9.878NESC Extre	103.105	149.600	314.015	0.000	7.354	11	3.000	0.875
47	X2	SAE	2X2X0.1875	6.37	79P	1.033NESC Extre	16.214	27.200	24.469	0.000	8.602	2	1.000	0.875
48	X3	SAE	2.5X2.5X0.25	29.34	81X	8.034NESC Extre	28.846	27.200	32.625	0.000	8.602	2	1.000	0.875
49	X4	SAE	3X3X0.3125	20.33	84X	8.296NESC Extre	44.745	40.800	61.172	0.000	8.602	3	1.000	0.875
50	X5	SAE	2.5X2.5X0.25	10.08	86Y	2.742NESC Extre	28.846	27.200	32.625	0.000	9.407	2	1.000	0.875
51	D14	SAE	3X3X0.1875	12.22	88XY	2.990NESC Extre	28.846	27.200	32.625	0.000	8.602	3	1.000	0.875
52	X14	SAU	2.5X2X0.1875	11.57	89X	2.220NESC Extre	27.500	27.200	24.469	0.000	8.602	2	1.000	0.875
53	DB3	SAU	3X2X0.25	28.35	90XY	8.177NESC Extre	19.184	40.800	48.937	0.000	17.082	2	1.000	0.875
54	DB4	SAE	3X3X0.1875	21.13	91X	5.810NESC Extre	28.846	40.800	48.937	0.000	18.752	3	1.000	0.875
55	H1	SAE	2.5X2.5X0.1875	13.59	92P	2.090NESC Extre	27.500	40.800	36.703	0.000	22.092	3	1.000	0.875
56	H2	SAE	2X2X0.1875	9.54	96P	1.796NESC Extre	16.214	27.200	24.469	0.000	7.000	2	1.000	0.875
57	H3	SAE	3.5X3.5X0.25	14.66	97X	1.483NESC Extre	53.952	40.800	61.172	0.000	7.000	1	1.000	0.875
58	H16	SAE	3.5X3X0.25	3.69	98P	1.469NESC Extre	39.835	40.800	48.937	0.000	5.415	3	1.000	0.875
59	H17	SAU	3.5X3X0.25	3.69	99P	4.010NESC Extre	39.835	40.800	48.937	0.000	7.000	3	1.000	0.875
60	H18	SAE	3.5X3.5X0.25	14.74	99P	0.000	43.696	40.800	32.625	0.000	12.744	2	1.000	0.875
61	H2	SAE	2X2X0.1875	0.00	100X	0.214NESC Extre	16.214	40.800	48.937	0.000	17.082	2	1.000	0.875
62	X7	SAE	2X2X0.1875	3.12	117P	0.000	16.214	13.600	12.234	0.000	7.000	3	1.000	0.875
63	H5	SAE	2.5X2.5X0.25	29.78	110X	3.033NESC Extre	16.214	13.600	12.234	0.000	7.000	3	1.000	0.875
64	X8	SAE	2X2X0.25	25.13	119P	3.938NESC Extre	28.846	27.200	32.625	0.000	9.220	1	1.000	0.875
65	H1	SAE	2.5X2.5X0.1875	24.10	120X	3.057NESC Extre	28.846	27.200	32.625	0.000	7.000	2	1.000	0.875
66	X8	SAE	2X2X0.25	13.06	121X	1.689NESC Extre	21.917	13.600	16.312	0.000	8.322	1	1.000	0.875
67	X6	SAE	2X2X0.25	7.71	122X	7.029NESC Extre	21.917	13.600	16.312	0.000	7.000	2	1.000	0.875
68	H4	SAU	3.5X2.5X0.25	13.02	122X	1.771NESC Extre	21.917	13.600	16.312	0.000	8.322	1	1.000	0.875
69	H2	SAE	2X2X0.1875	79.28	107XY	0.000NESC Extre	16.214	13.600	16.312	0.000	9.899	1	1.000	0.875
70	D2	SAE	2.5X2.5X0.1875	36.70	124X	0.000NESC Extre	16.214	13.600	16.312	0.000	7.000	1	1.000	0.875
71	H2	SAE	2X2X0.1875	34.97	131P	0.000NESC Extre	16.214	13.600	16.312	0.000	7.000	1	1.000	0.875
72	D2	SAE	2.5X2.5X0.1875	17.21	132BP	2.105NESC Extre	16.214	13.600	16.312	0.000	7.000	1	1.000	0.875
73	H2	SAE	2X2X0.1875	0.00	139X	0.000	16.214	13.600	12.234	0.000	9.220	1	1.000	0.875
74	D2	SAE	2.5X2.5X0.1875	15.65	134AP	1.915NESC Extre	21.917	13.600	12.234	0.000	7.000	1	1.000	0.875
75	H10	SAE	3.5X3.5X0.25	13.01	129X	1.592NESC Extre	16.214	13.600	12.234	0.000	8.322	1	1.000	0.875
76	X10	SAE	3.5X3.5X0.25	15.52	136BP	1.899NESC Extre	21.917	13.600	12.234	0.000	8.322	1	1.000	0.875
77	H9	SAE	2X2X0.1875	7.15	143P	1.944NESC Extre	43.696	27.200	32.625	0.000	10.750	2	1.000	0.875
78	H13	SAE	2X2X0.1875	1.16	144P	0.189NESC Extre	16.214	27.200	24.469	0.000	15.027	2	1.000	0.875
79	X9	SAU	3X3X0.25	7.92	145X	0.000	16.214	27.200	24.469	0.000	10.750	2	1.000	0.875
80	X9	SAU	2.5X1.5X0.25	8.60	146BX	3.118NESC Extre	36.271	40.800	48.937	0.000	5.375	3	1.000	0.875
81	H8	SAE	2.5X1.5X0.25	0.00	147Y	0.000	21.421	40.800	48.937	0.000	7.589	3	1.000	0.875
82	H15	SAE	2X2X0.25	8.57	148Y	0.000	21.421	40.800	48.937	0.000	7.589	3	1.000	0.875
83	X12	SAE	3X3X0.1875	5.48	149P	1.836NESC Extre	27.500	27.200	32.625	0.000	5.315	2	1.000	0.875
84	H14	SAE	2X2X0.1875	0.00	150P	0.000	27.500	27.200	32.625	0.000	5.315	2	1.000	0.875
85	H13	SAE	2X2X0.1875	21.14	151XY	0.951NESC Extre	16.214	13.600	12.234	0.000	16.452	2	1.000	0.875
86	X11	SAE	3X3X0.25	0.00	152X	0.000	16.214	13.600	12.234	0.000	12.666	2	1.000	0.875
87	H19	SAE	2X2X0.1875	3.57	153P	0.024NESC Extre	36.271	27.200	32.625	0.000	13.934	1	1.000	0.875
88	X13	SAE	3X3X0.1875	2.81	154P	0.344NESC Extre	16.214	13.600	12.234	0.000	17.082	1	1.000	0.875
			2X2X0.1875	2.87	155P	0.754NESC Extre	27.500	13.600	12.234	0.000	24.202	1	1.000	0.875
				92.14	156Y	0.000	16.214	13.600	12.234	0.000	24.202	1	1.000	0.875

*** Maximum Stress Summary for Each Load Case

Summary of Maximum Usages by Load Case:

Load Case	Maximum Element Usage %	Element Label	Element Type
NESC Heavy	83.15	89P	Angle
NESC Extreme	84.39	89P	Angle
NESC Broken Wire	92.14	156XY	Angle

Summary of Insulator Usages:

Insulator Label	Insulator Type	Insulator Maximum Usage %	Load Case	Maximum Weight (lbs)
C1	Clamp	12.00	NESC Heavy	0.0
C2	Clamp	8.27	NESC Heavy	0.0
C3	Clamp	7.43	NESC Heavy	0.0
C4	Clamp	7.43	NESC Heavy	0.0
C5	Clamp	23.70	NESC Broken Wire	0.0
C6	Clamp	7.43	NESC Heavy	0.0
C7	Clamp	7.43	NESC Heavy	0.0
C8	Clamp	7.43	NESC Heavy	0.0
C9	Clamp	7.43	NESC Heavy	0.0
C10	Clamp	7.43	NESC Heavy	0.0
C11	Clamp	7.43	NESC Heavy	0.0
C12	Clamp	7.43	NESC Heavy	0.0
C13	Clamp	7.43	NESC Heavy	0.0
C14	Clamp	7.43	NESC Heavy	0.0
C15	Clamp	7.46	NESC Heavy	0.0
C16	Clamp	7.46	NESC Heavy	0.0
C17	Clamp	7.46	NESC Heavy	0.0
C18	Clamp	7.46	NESC Heavy	0.0
C19	Clamp	7.48	NESC Heavy	0.0
C20	Clamp	7.48	NESC Heavy	0.0
C21	Clamp	7.48	NESC Heavy	0.0
C22	Clamp	7.48	NESC Heavy	0.0
C23	Clamp	7.49	NESC Heavy	0.0
C24	Clamp	7.49	NESC Heavy	0.0
C25	Clamp	7.49	NESC Heavy	0.0
C26	Clamp	7.49	NESC Heavy	0.0
C27	Clamp	9.20	NESC Heavy	0.0
C28	Clamp	1.39	NESC Extreme	0.0
C29	Clamp	2.68	NESC Heavy	0.0
C30	Clamp	1.86	NESC Heavy	0.0
C31	Clamp	2.20	NESC Heavy	0.0
C32	Clamp	3.99	NESC Heavy	0.0
C33	Clamp	2.50	NESC Heavy	0.0
C34	Clamp	10.21	NESC Heavy	0.0
C35	Clamp	1.47	NESC Extreme	0.0
C36	Clamp	2.69	NESC Extreme	0.0
C37	Clamp	1.86	NESC Heavy	0.0
C38	Clamp	2.20	NESC Heavy	0.0
C39	Clamp	3.99	NESC Heavy	0.0
C40	Clamp	2.50	NESC Heavy	0.0
C41	Clamp	8.48	NESC Heavy	0.0
C42	Clamp	9.48	NESC Extreme	0.0
C43	Clamp	2.34	NESC Extreme	0.0
C44	Clamp	2.71	NESC Extreme	0.0

*** Weight of structure (lbs):
 Weight of Angles*Section DLF: 31305.4
 Total: 31305.4
 *** End of Report

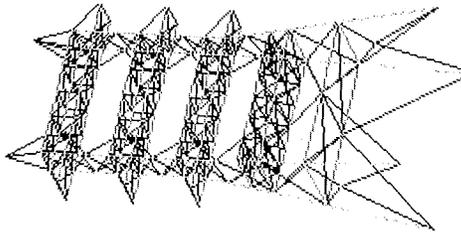
 * TOWER - Analysis and Design - Copyright Power Line Systems, Inc. 1986-2006 *

Project Name : Nowalk Tower #1102
 Project Notes: T-MOBILE PCS
 Project File : J:\Jobs\0817400.WI - HPC-T-Mobile\CO05 - CT11356-CL&P Tower - Rte 123\Engineering\Structural\Rev (1)\Calcs\Pis-Tower\norwalk1102.tow
 Date run : 11:36:03 AM Wednesday, July 08, 2009
 by : Tower Version 9.04
 Licensed to : Natcomm

Successfully performed nonlinear analysis

KL/R value of 213.20 exceeds maximum of 200.00 for member "94P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "94X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "96P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "96X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "101P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "109P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "117P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "125P" ??
 KL/R value of 223.50 exceeds maximum of 200.00 for member "126AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "126BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "127P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "127X" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "128AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "128BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "129P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "129X" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "130AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "130BP" ??
 KL/R value of 223.50 exceeds maximum of 200.00 for member "131P" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "132AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "132BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "133P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "133X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "134AP" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "134BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "135P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "135X" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "136AP" ??
 KL/R value of 223.50 exceeds maximum of 200.00 for member "136BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "137P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "138AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "138BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "139P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "139X" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "140AP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "140BP" ??
 KL/R value of 213.20 exceeds maximum of 200.00 for member "141P" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "141X" ??
 KL/R value of 201.74 exceeds maximum of 200.00 for member "142AP" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "142BP" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "144P" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "144X" ??
 KL/R value of 202.97 exceeds maximum of 200.00 for member "144Y" ??
 KL/R value of 203.04 exceeds maximum of 200.00 for member "144Y" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "150P" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "151P" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "151X" ??
 KL/R value of 250.54 exceeds maximum of 200.00 for member "151Y" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "151Y" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "154P" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "154X" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "154XY" ??
 KL/R value of 212.19 exceeds maximum of 200.00 for member "154Y" ??

KL/R value of 368.56 exceeds maximum of 200.00 for member "156P" ??
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156X" ??
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156Y" ??
 Clamp insulator "C33" has a structure attach joint "14Xy" that is fixed with respect to translation ??
 Clamp insulator "C40" has a structure attach joint "14y" that is fixed with respect to translation ??
 The model has 59 warnings. ??



Nonlinear convergence parameters: Use Standard Parameters
 Member check option: ASCE 10
 Connection rupture check: Not Checked
 Crossing diagonal check: Fixed

Joints Geometry:

Joint Label	Symmetry Code	X Coord. (ft)	Y Coord. (ft)	Z Coord. (ft)	X Disp.		Y Disp.		Z Disp.		X Rot.		Y Rot.		Z Rot.	
					Rest.	Free	Rest.	Free	Rest.	Free	Rest.	Free	Rest.	Free	Rest.	Free
1P	X-Symmetry	0		14	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
2P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
3P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
4P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
5P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
6P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
7P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
8P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
9P	XY-Symmetry	3.5		15	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
14P	XY-Symmetry	13.07	19.07	0	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
15P	XY-Symmetry	3.5		22	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
16P	XY-Symmetry	3.5		22	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
17P	XY-Symmetry	3.5		22	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
18P	Y-Symmetry	3.5		0	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
19P	XY-Symmetry	3.5		6	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
20P	XY-Symmetry	3.5		6	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
21P	Y-Symmetry	3.5	10.5	85	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
22P	XY-Symmetry	3.5		0	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
23P	XY-Symmetry	3.5		6	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
24P	Y-Symmetry	3.5	10.5	80	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
25P	XY-Symmetry	3.5		0	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
26P	XY-Symmetry	3.5		6	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
27P	Y-Symmetry	3.5	10.5	70	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
28P	XY-Symmetry	3.5		0	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
				65	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free
				65	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free	Free

Joint Label	Symmetry Code	Origin Joint	End Joint	Fraction	Elevation	X Disp.	Y Disp.	Z Disp.	X Rot. Rest.	Y Rot. Rest.	Z Rot. Rest.
25Y											
26X											
26XY											
26Y											
27Y											
28X											
28XY											
28Y											
29X											
29Y											
30Y											
31X											
31XY											
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35XY											
35Y											
36Y											
37X											
37XY											
37Y											
38X											
38XY											
38Y											
39Y											
40X											
40XY											
40Y											
41X											
41XY											
41Y											
44X											
44XY											
45X											

Secondary Joints:

Joint Label	Symmetry Code	Origin Joint	End Joint	Fraction	Elevation	X Disp.	Y Disp.	Z Disp.	X Rot. Rest.	Y Rot. Rest.	Z Rot. Rest.
10S											
11S											
12S											
13S											
42S											
43S											
10X											
10XY											
10Y											
11X											
11XY											
11Y											
12X											
12XY											
12Y											
13X											
13XY											
13Y											
42Y											
43X											

Steel Material Properties:

Material Label	Modulus of Elasticity (ksi)	Yield Stress (ksi)	Ultimate Stress (ksi)	Member Stress All.		Member Rupture Bearing		Member Bearing	
				Fu	Fy	Hyp. 1	Hyp. 2	Hyp. 1	Hyp. 2
A7	2.9e+004	33	58	0	0	0	0	0	0
A440-50	2.9e+004	50	60	0	0	0	0	0	0

Bolt Properties:

Bolt Label	Diameter (in)	Hole Diameter (in)	Ultimate Shear Capacity (kips)	Default End Spacing (in)	Shear Capacity (kips)	Member Rupture Bearing Hyp. 1 (ksi)	Member Rupture Bearing Hyp. 2 (ksi)	Member Bearing Hyp. 1 (ksi)	Member Bearing Hyp. 2 (ksi)
3/4 A394	0.75	0.875	13.6	1.35	1.8	0	0	0	0

Number Bolts Used By Type:

Bolt Type	Number
3/4 A394	1549

Angle Properties:

Angle Type	Label	Group	Angle Size (in)	Long Leg (in)	Short Leg (in)	Thick. Leg (in)	Unit Weight (lbs/ft)	Gross Area (in ²)	w/t Ratio	Radius of Gyration (in)	Number of Angles	Wind Dist. (in)	Short Edge Dist. (in)	Long Edge Dist. (in)	Section Modulus (in ³)	Optimize Factor
SAE	8X8X0.5		8	8	0.5	26.4	7.75	13.75	2.5	1.59	1	8	4	0	1.0000	
SAE	6X6X0.5		6	6	0.5	19.6	5.75	10	1.86	1.86	1	6	3	0	1.0000	
SAE	5X5X0.375		5	5	0.375	12.3	3.61	11	1.56	0.99	1	5	2.5	0	1.0000	
SAE	4X4X0.375		4	4	0.375	9.8	2.86	8.67	1.23	0.788	1	4	2	0	1.0000	
SAE	4X4X0.3125		4	4	0.3125	8.2	2.4	10.6	1.24	0.791	1	4	2	0	1.0000	
SAE	4X4X0.25		4	4	0.25	6.6	1.94	13.5	1.25	0.795	1	4	2	0	1.0000	
SAE	3.5X3.5X0.3125		3.5	3.5	0.3125	7.2	2.09	11.5	1.08	0.69	1	3.5	1.75	0	1.0000	
SAE	3.5X3.5X0.25		3.5	3.5	0.25	5.8	1.69	11.5	0.922	0.684	1	3.5	1.75	0	1.0000	
SAE	3X3X0.3125		3	3	0.3125	6.1	1.78	7.6	0.93	0.589	1	3	1.5	0	1.0000	
SAE	3X3X0.25		3	3	0.25	4.9	1.44	9.75	0.939	0.592	1	3	1.5	0	1.0000	
SAE	2.5X2.5X0.1875		2.5	2.5	0.1875	3.71	1.09	13.33	0.789	0.491	1	2.5	1.25	0	1.0000	
SAE	2.5X2.5X0.1875		2.5	2.5	0.1875	4.1	1.19	7.75	0.778	0.495	1	2.5	1.25	0	1.0000	
SAE	2X2X0.25		2	2	0.25	3.19	0.94	10.67	0.609	0.391	1	2	1	0	1.0000	
SAU	7X4X0.1875		2	2	0.1875	2.44	0.71	8	0.617	0.376	1	2	1	0	1.0000	
SAU	4X3.5X0.25		4	4	0.4375	15.8	4.62	13.86	2.26	1.12	0.876	1	7	2	0	1.0000
SAU	3.5X3X0.25		3.5	3	0.25	6.2	1.81	13.25	1.27	1.07	0.734	1	4	1.75	0	1.0000
SAU	3.5X2.5X0.25		3.5	2.5	0.25	5.4	1.56	11.25	1.11	0.914	1	3.5	1.5	0	1.0000	
SAU	3X2.5X0.25		3	2.5	0.25	4.9	1.44	11.25	1.12	0.735	0.584	1	3.5	1.25	0	1.0000
SAU	3X2X0.25		3	2	0.25	4.5	1.31	9.5	0.945	0.574	0.528	1	3	1.25	0	1.0000
SAU	2.5X2X0.1875		2.5	2	0.1875	4.1	1.19	10.67	0.957	0.435	0.435	1	3	1	0	1.0000
SAU	2.5X1.5X0.25		2.5	1.5	0.25	3.19	0.94	7.75	0.793	0.6	0.427	1	2.5	1	0	1.0000
DAS	4X3X0.4375		3.5	3	0.4375	19.6	5.74	7.14	0.794	0.415	0.324	1	2.5	0.75	0	1.0000
DAS	3.5X3X0.25		3.5	3	0.25	10.8	3.13	11.25	0.871	1.95	0.871	2	4	1.5	0	1.0000
BAR	2 x 0.1875		2	0.1875	0.1875	1.28	0.375	0	0.577	0.054	0.054	1	2	0	1.0000	

Angle Groups:

Group Label	Description	Angle Type	Material Type	Element Type	Group Type	Optimize Group	Allow. Angle (in)	Add. Width For Optimize (in)
1	L1	SAE 2.5X2.5X0.1875	A7	Truss	Other	None	0.000	0.000

2	I2	SAE	5X5X0.375	A7	Beam	Leg	None	0.000
3	I3	SAE	5X5X0.375	A7	Beam	Leg	None	0.000
4	L4	SAE	5X5X0.375	A7	Beam	Leg	None	0.000
5	L5	SAE	5X5X0.375	A7	Beam	Leg	None	0.000
6	L6	SAE	8X8X0.5	A7	Beam	Leg	None	0.000
7	L7	SAE	8X8X0.5	A7	Beam	Leg	None	0.000
8	L8	SAE	8X8X0.5	A7	Beam	Leg	None	0.000
9	L9	SAE	8X8X0.5	A7	Beam	Leg	None	0.000
10	L10	SAE	8X8X0.5	A440-50	Beam	Leg	None	0.000
11	L11	SAE	8X8X0.5	A440-50	Beam	Leg	None	0.000
12	L12	SAE	8X8X0.5	A440-50	Beam	Leg	None	0.000
13	L13	SAE	8X8X0.5	A440-50	Beam	Leg	None	0.000
14	PEAK	SAE	2.5X2.5X0.1875	A7	Beam	Leg	None	0.000
15	TTC	SAE	3X3X0.25	A7	Truss	Other	None	0.000
16	TTC	SAE	3X3X0.25	A7	Beam	Other	None	0.000
17	ARMTI	SAE	4X4X0.25	A7	Beam	Other	None	0.000
18	MTTC	SAE	4X4X0.25	A7	Beam	Other	None	0.000
19	MTBC	SAE	4X4X0.25	A7	Beam	Other	None	0.000
20	ARMMT	SAE	4X4X0.25	A7	Beam	Other	None	0.000
21	BTC	SAE	4X4X0.3125	A7	Beam	Other	None	0.000
22	BTC	SAE	4X4X0.3125	A7	Beam	Other	None	0.000
23	ARMBT	SAE	4X4X0.3125	A7	Beam	Other	None	0.000
24	BTTTC	SAE	8X8X0.5	A7	Beam	Other	None	0.000
25	BTTBC	SAE	6X6X0.5	A7	Beam	Other	None	0.000
26	W1	SAE	2X2X0.1875	A7	Beam	Other	None	0.000
27	W2	SAE	4X4X0.375	A7	Truss	Other	None	0.000
28	W3	SAE	4X4X0.3125	A7	Truss	Other	None	0.000
29	W4	SAE	4X4X0.3125	A7	Truss	Other	None	0.000
30	W5	SAE	4X4X0.25	A7	Truss	Other	None	0.000
31	W6	SAU	4X3.5X0.25	A7	Truss	Other	None	0.000
32	W7	SAE	3.5X3.5X0.25	A7	Truss	Other	None	0.000
33	W8	SAE	3X3X0.1875	A7	Truss	Other	None	0.000
34	W9	SAE	3X3X0.3125	A7	Truss	Other	None	0.000
35	W10	SAU	3X2.5X0.25	A7	Truss	Other	None	0.000
36	W11	SAE	4X4X0.25	A7	Truss	Other	None	0.000
37	W12	SAE	3.5X3.5X0.25	A7	Truss	Other	None	0.000
38	W13	SAE	4X4X0.375	A7	Truss	Other	None	0.000
39	KB1	SAE	4X4X0.375	A7	Truss	Other	None	0.000
40	KB2	SAE	4X4X0.25	A7	Truss	Other	None	0.000
41	KB3	SAE	3X3X0.3125	A7	Truss	Other	None	0.000
42	B1	BAR	2 x 0.1875	A7	T-Only	Other	None	0.000
43	DB1	DAS	3.5X3X0.25	A7	Truss	Other	None	0.000
44	DB2	DAS	4X3X0.4375	A7	Truss	Other	None	0.000
45	HBI	SAE	3X3X0.1875	A7	Beam	Other	None	0.000
46	X1	SAU	7X4X0.4375	A7	Truss	Other	None	0.000
47	X2	SAE	2X2X0.1875	A7	Truss	Other	None	0.000
48	X3	SAE	2.5X2.5X0.25	A7	Truss	Other	None	0.000
49	X4	SAE	3X3X0.3125	A7	Truss	Other	None	0.000
50	X5	SAE	2.5X2.5X0.25	A7	Truss	Other	None	0.000
51	D1	SAE	3X3X0.1875	A7	Truss	Other	None	0.000
52	X14	SAU	2.5X2X0.1875	A7	T-Only	Other	None	0.000
53	DB3	SAU	3X2X0.25	A7	T-Only	Other	None	0.000
54	DB4	SAE	3X3X0.1875	A7	T-Only	Other	None	0.000
55	H1	SAE	2.5X2.5X0.1875	A7	Truss	Other	None	0.000
56	H2	SAE	2X2X0.1875	A7	Truss	Other	None	0.000
57	H3	SAE	3.5X3.5X0.3125	A7	Truss	Other	None	0.000
58	H16	SAU	3.5X3X0.25	A7	Beam	Other	None	0.000
59	H17	SAU	3.5X3X0.25	A7	Beam	Other	None	0.000
60	H18	SAE	3.5X3.5X0.25	A7	Beam	Other	None	0.000
61	H2	SAE	2X2X0.1875	A7	Truss	Other	None	0.000
62	X7	SAE	2X2X0.1875	A7	Truss	Other	None	0.000
63	H5	SAE	2.5X2.5X0.25	A7	Truss	Other	None	0.000
64	X8	SAE	2X2X0.25	A7	Truss	Other	None	0.000
65	H1	SAE	2.5X2.5X0.1875	A7	Truss	Other	None	0.000
66	X8	SAE	2X2X0.25	A7	Truss	Other	None	0.000
67	X6	SAE	2X2X0.25	A7	Truss	Other	None	0.000
68	H4	SAU	3.5X2.5X0.25	A7	Truss	Other	None	0.000
69	H2	SAE	2X2X0.1875	A7	Truss	Other	None	0.000
70	D2	SAE	2.5X2.5X0.1875	A7	Truss	Other	None	0.000

Member Group Section Label	Symmetry Code	Origin Joint Code	End Joint Code	Ecc. Code	Rest. Code	Ratio			Bolt Type	# Bolts	# Holes	# Shear Planes	Connect Leg			End Dist.	Boit Rest. Spacing Coef.
						R1X	R1Y	R1Z					Short Edge Dist.	Long Edge Dist.	End Dist.		
1P	XY-Symmetry	1P	2P	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
1X	X-GenXY	1X	2X	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
1XY	XY-GenXY	1X	2XY	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
1Y	Y-GenXY	1P	2Y	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
2P	XY-Symmetry	2P	3P	1	6	1	1	1	1 3/4 A394	0	1.76	1	Both	0	0	0	0
2X	X-GenXY	2X	3X	1	6	1	1	1	1 3/4 A394	0	1.76	1	Both	0	0	0	0
2XY	XY-GenXY	2X	3XY	1	6	1	1	1	1 3/4 A394	0	1.76	1	Both	0	0	0	0
2Y	Y-GenXY	2Y	3Y	1	6	1	1	1	1 3/4 A394	0	1.76	1	Both	0	0	0	0
3P	XY-Symmetry	3P	4P	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
3X	X-GenXY	3X	4X	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
3XY	XY-GenXY	3X	4XY	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
3Y	Y-GenXY	3Y	4Y	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
4P	XY-Symmetry	4P	5P	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
4X	X-GenXY	4X	5X	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
4XY	XY-GenXY	4X	5XY	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
4Y	Y-GenXY	4Y	5Y	1	6	1	1	1	1 3/4 A394	0	3.36	1	Both	0	0	0	0
5P	XY-Symmetry	5P	6P	1	6	1	1	1	1 3/4 A394	10	4	1	Both	0	0	0	0
5X	X-GenXY	5X	6X	1	6	1	1	1	1 3/4 A394	10	4	1	Both	0	0	0	0
5XY	XY-GenXY	5X	6XY	1	6	1	1	1	1 3/4 A394	10	4	1	Both	0	0	0	0
5Y	Y-GenXY	5Y	6Y	1	6	1	1	1	1 3/4 A394	10	4	1	Both	0	0	0	0
6P	XY-Symmetry	6P	7P	1	6	1	1	1	1 3/4 A394	10	4	1	Both	0	0	0	0
6X	X-GenXY	6X	7X	1	6	1	1	1	1 3/4 A394	0	1.65	1	Both	0	0	0	0
6XY	XY-GenXY	6X	7XY	1	6	1	1	1	1 3/4 A394	0	1.65	1	Both	0	0	0	0
6Y	Y-GenXY	6Y	7Y	1	6	1	1	1	1 3/4 A394	0	1.65	1	Both	0	0	0	0
7P	XY-Symmetry	7P	8P	1	6	1	1	1	1 3/4 A394	0	1.65	1	Both	0	0	0	0
7X	X-GenXY	7X	8X	1	6	1	1	1	1 3/4 A394	0	1.65	1	Both	0	0	0	0
7XY	XY-GenXY	7X	8XY	1	6	1	1	1	1 3/4 A394	0	1.65	1	Both	0	0	0	0
7Y	Y-GenXY	7Y	8Y	1	6	1	1	1	1 3/4 A394	0	1.65	1	Both	0	0	0	0
8P	XY-Symmetry	8P	9P	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
8X	X-GenXY	8X	9X	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
8XY	XY-GenXY	8X	9XY	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
8Y	Y-GenXY	8Y	9Y	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
9P	XY-Symmetry	9P	10P	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
9X	X-GenXY	9X	10X	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
9XY	XY-GenXY	9X	10XY	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
9Y	Y-GenXY	9Y	10Y	1	6	1	1	1	1 3/4 A394	10	4	2	Both	0	0	0	0
10P	XY-Symmetry	10S	11S	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
10X	X-GenXY	10X	11X	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
10XY	XY-GenXY	10X	11XY	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
10Y	Y-GenXY	10Y	11Y	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
11P	XY-Symmetry	11S	12S	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
11X	X-GenXY	11X	12X	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
11XY	XY-GenXY	11X	12XY	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
11Y	Y-GenXY	11Y	12Y	1	6	1	1	1	1 3/4 A394	0	1.46	2	Both	0	0	0	0
12P	XY-Symmetry	12S	13S	1	6	0.5	0.5	0.5	0.5 3/4 A394	0	4	1	Both	0	0	0	0
12X	X-GenXY	12X	13X	1	6	0.5	0.5	0.5	0.5 3/4 A394	0	4	1	Both	0	0	0	0
12XY	XY-GenXY	12X	13XY	1	6	0.5	0.5	0.5	0.5 3/4 A394	0	4	1	Both	0	0	0	0
12Y	Y-GenXY	12Y	13Y	1	6	0.5	0.5	0.5	0.5 3/4 A394	0	4	1	Both	0	0	0	0
13P	XY-Symmetry	13S	14P	1	6	0.25	0.25	0.25	0.25 3/4 A394	0	4	1	Both	0	0	0	0
13X	X-GenXY	13X	14X	1	6	0.25	0.25	0.25	0.25 3/4 A394	0	4	1	Both	0	0	0	0
13XY	XY-GenXY	13X	14XY	1	6	0.25	0.25	0.25	0.25 3/4 A394	0	4	1	Both	0	0	0	0
13Y	Y-GenXY	13Y	14Y	1	6	0.25	0.25	0.25	0.25 3/4 A394	0	4	1	Both	0	0	0	0
14P	XY-Symmetry	14P	20P	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
14X	X-GenXY	14X	20X	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
14XY	XY-GenXY	14X	20XY	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
14Y	Y-GenXY	14Y	20Y	3	5	0.5	0.5	0.5	0.5 3/4 A394	2	1	1	Long only	0	0	0	0
15P	XY-Symmetry	18P	19P	3	4	1	1	1	1 3/4 A394	4	2	1	Long only	0	0	0	0
15X	X-GenXY	18X	19X	3	4	1	1	1	1 3/4 A394	4	2	1	Long only	0	0	0	0
15XY	XY-GenXY	18X	19XY	3	4	1	1	1	1 3/4 A394	4	2	1	Long only	0	0	0	0
15Y	Y-GenXY	18Y	19Y	3	4	1	1	1	1 3/4 A394	4	2	1	Long only	0	0	0	0
16P	XY-Symmetry	19P	20P	3	4	1	1	1	1 3/4 A394	0	1	1	Long only	0	0	0	0
16X	X-GenXY	19X	20X	3	4	1	1	1	1 3/4 A394	0	1	1	Long only	0	0	0	0
16XY	XY-GenXY	19X	20XY	3	4	1	1	1	1 3/4 A394	0	1	1	Long only	0	0	0	0
16Y	Y-GenXY	19Y	20Y	3	4	1	1	1	1 3/4 A394	0	1	1	Long only	0	0	0	0

40P	20	40.528	L/F	40.800	Shear	106	7.00	40.528	40.800	48.937	49.952	0.000	0.000	Automatic
40X	20	40.528	L/F	40.800	Shear	106	7.00	40.528	40.800	48.937	49.952	0.000	0.000	Automatic
40Y	20	40.528	L/F	40.800	Shear	106	7.00	40.528	40.800	48.937	49.952	0.000	0.000	Automatic
41P	23	40.800	Shear	40.800	Shear	106	7.00	50.000	40.800	61.172	61.697	0.000	0.000	Automatic
41X	23	40.800	Shear	40.800	Shear	106	7.00	50.000	40.800	61.172	61.697	0.000	0.000	Automatic
41Y	23	40.800	Shear	40.800	Shear	106	7.00	50.000	40.800	61.172	61.697	0.000	0.000	Automatic
42P	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
42X	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
42Y	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
43P	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
43X	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
43Y	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
44P	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
44X	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
44Y	42	0.072	L/F	6.265	Net Sect	1912	8.60	0.072	27.200	24.469	6.265	0.000	0.000	Automatic
45P	41	29.912	L/F	40.800	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	Automatic
45X	41	29.912	L/F	40.800	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	Automatic
45Y	41	29.912	L/F	40.800	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	Automatic
46P	41	29.912	L/F	40.800	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	Automatic
46X	41	29.912	L/F	40.800	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	Automatic
46Y	41	29.912	L/F	40.800	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	Automatic
47P	40	41.379	L/F	47.613	Net Sect	102	6.73	41.379	47.613	65.250	47.613	0.000	0.000	Automatic
47X	40	41.379	L/F	47.613	Net Sect	102	6.73	41.379	47.613	65.250	47.613	0.000	0.000	Automatic
47Y	40	41.379	L/F	47.613	Net Sect	102	6.73	41.379	47.613	65.250	47.613	0.000	0.000	Automatic
48P	40	41.379	L/F	47.613	Net Sect	102	6.73	41.379	47.613	65.250	47.613	0.000	0.000	Automatic
48X	40	41.379	L/F	47.613	Net Sect	102	6.73	41.379	47.613	65.250	47.613	0.000	0.000	Automatic
48Y	40	41.379	L/F	47.613	Net Sect	102	6.73	41.379	47.613	65.250	47.613	0.000	0.000	Automatic
49P	39	59.125	L/F	68.000	Shear	108	7.07	59.125	68.000	122.344	68.570	0.000	0.000	Automatic
49X	39	59.125	L/F	68.000	Shear	108	7.07	59.125	68.000	122.344	68.570	0.000	0.000	Automatic
49Y	39	59.125	L/F	68.000	Shear	108	7.07	59.125	68.000	122.344	68.570	0.000	0.000	Automatic
50P	39	59.150	L/F	68.000	Shear	108	7.07	59.150	68.000	122.344	68.570	0.000	0.000	Automatic
50X	39	59.150	L/F	68.000	Shear	108	7.07	59.150	68.000	122.344	68.570	0.000	0.000	Automatic
50Y	39	59.150	L/F	68.000	Shear	108	7.07	59.150	68.000	122.344	68.570	0.000	0.000	Automatic
51P	43	48.988	L/F	54.400	Shear	145	19.91	48.988	54.400	65.250	72.542	0.000	0.000	Automatic
51X	43	48.988	L/F	54.400	Shear	145	19.91	48.988	54.400	65.250	72.542	0.000	0.000	Automatic
51Y	43	48.988	L/F	54.400	Shear	145	19.91	48.988	54.400	65.250	72.542	0.000	0.000	Automatic
52P	44	55.071	L/F	81.600	Shear	189	30.73	55.071	81.600	171.281	121.751	0.000	0.000	Automatic
52X	44	55.071	L/F	81.600	Shear	189	30.73	55.071	81.600	171.281	121.751	0.000	0.000	Automatic
52Y	44	55.071	L/F	81.600	Shear	189	30.73	55.071	81.600	171.281	121.751	0.000	0.000	Automatic
53P	45	12.168	L/F	27.500	Net Sect	173	17.14	12.168	40.800	36.703	27.500	0.000	0.000	Automatic
53X	45	12.168	L/F	27.500	Net Sect	173	17.14	12.168	40.800	36.703	27.500	0.000	0.000	Automatic
53Y	45	12.168	L/F	27.500	Net Sect	173	17.14	12.168	40.800	36.703	27.500	0.000	0.000	Automatic
54P	26	10.390	L/F	16.214	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	Automatic
54X	26	10.390	L/F	16.214	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	Automatic
54Y	26	10.390	L/F	16.214	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	Automatic
55P	33	15.275	L/F	24.469	Bearing	157	7.81	15.275	27.200	24.469	16.214	0.000	0.000	Automatic
55X	33	15.275	L/F	24.469	Bearing	157	7.81	15.275	27.200	24.469	16.214	0.000	0.000	Automatic
55Y	33	15.275	L/F	24.469	Bearing	157	7.81	15.275	27.200	24.469	16.214	0.000	0.000	Automatic
56P	26	10.390	L/F	16.214	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	Automatic
56X	26	10.390	L/F	16.214	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	Automatic
56Y	26	10.390	L/F	16.214	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	Automatic
57P	33	18.584	L/F	24.469	Bearing	135	6.73	18.584	27.200	24.469	16.214	0.000	0.000	Automatic
57X	33	18.584	L/F	24.469	Bearing	135	6.73	18.584	27.200	24.469	16.214	0.000	0.000	Automatic
57Y	33	18.584	L/F	24.469	Bearing	135	6.73	18.584	27.200	24.469	16.214	0.000	0.000	Automatic

57Y	33	18.584	Bearing	135	6.73	18.584	27.200	24.469	27.500	0.000	0.000	0.000	Automatic
58P	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
58X	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
58XY	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
58Y	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
59P	34	29.912	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	0.000	Automatic
59X	34	29.912	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	0.000	Automatic
59Y	34	29.912	Shear	137	6.73	29.912	40.800	61.172	44.745	0.000	0.000	0.000	Automatic
60P	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
60Y	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
61P	31	32.946	Shear	128	7.81	32.946	40.800	48.937	44.531	0.000	0.000	0.000	Automatic
61X	31	32.946	Shear	128	7.81	32.946	40.800	48.937	44.531	0.000	0.000	0.000	Automatic
61XY	31	32.946	Shear	128	7.81	32.946	40.800	48.937	44.531	0.000	0.000	0.000	Automatic
61Y	31	32.946	Shear	128	7.81	32.946	40.800	48.937	44.531	0.000	0.000	0.000	Automatic
62P	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
62X	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
62Y	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
63P	32	33.327	Shear	116	6.73	33.327	40.800	48.937	43.696	0.000	0.000	0.000	Automatic
63X	32	33.327	Shear	116	6.73	33.327	40.800	48.937	43.696	0.000	0.000	0.000	Automatic
63XY	32	33.327	Shear	116	6.73	33.327	40.800	48.937	43.696	0.000	0.000	0.000	Automatic
63Y	32	33.327	Shear	116	6.73	33.327	40.800	48.937	43.696	0.000	0.000	0.000	Automatic
64P	35	26.226	Shear	114	5.00	26.226	27.200	32.625	32.410	0.000	0.000	0.000	Automatic
64X	35	26.226	Shear	114	5.00	26.226	27.200	32.625	32.410	0.000	0.000	0.000	Automatic
64Y	35	26.226	Shear	114	5.00	26.226	27.200	32.625	32.410	0.000	0.000	0.000	Automatic
65P	36	41.379	Net Sect	102	6.73	41.379	54.400	65.250	47.613	0.000	0.000	0.000	Automatic
65X	36	41.379	Net Sect	102	6.73	41.379	54.400	65.250	47.613	0.000	0.000	0.000	Automatic
65XY	36	41.379	Net Sect	102	6.73	41.379	54.400	65.250	47.613	0.000	0.000	0.000	Automatic
65Y	36	41.379	Net Sect	102	6.73	41.379	54.400	65.250	47.613	0.000	0.000	0.000	Automatic
66P	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
66Y	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
67P	29	46.740	Shear	118	7.81	46.740	54.400	81.562	59.748	0.000	0.000	0.000	Automatic
67X	29	46.740	Shear	118	7.81	46.740	54.400	81.562	59.748	0.000	0.000	0.000	Automatic
67XY	29	46.740	Shear	118	7.81	46.740	54.400	81.562	59.748	0.000	0.000	0.000	Automatic
67Y	29	46.740	Shear	118	7.81	46.740	54.400	81.562	59.748	0.000	0.000	0.000	Automatic
68P	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
68X	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
68XY	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
68Y	26	10.390	Net Sect	152	5.00	10.390	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
69P	30	41.379	Net Sect	102	6.73	41.379	54.400	65.250	49.627	0.000	0.000	0.000	Automatic
69X	30	41.379	Net Sect	102	6.73	41.379	54.400	65.250	49.627	0.000	0.000	0.000	Automatic
69XY	30	41.379	Net Sect	102	6.73	41.379	54.400	65.250	49.627	0.000	0.000	0.000	Automatic
69Y	30	41.379	Net Sect	102	6.73	41.379	54.400	65.250	49.627	0.000	0.000	0.000	Automatic
70P	37	38.640	Shear	86	5.00	38.640	40.800	48.937	43.696	0.000	0.000	0.000	Automatic
70X	37	38.640	Shear	86	5.00	38.640	40.800	48.937	43.696	0.000	0.000	0.000	Automatic
70Y	37	38.640	Shear	86	5.00	38.640	40.800	48.937	43.696	0.000	0.000	0.000	Automatic
71P	38	60.729	Net Sect	102	6.73	60.729	68.000	122.344	66.816	0.000	0.000	0.000	Automatic
71X	38	60.729	Net Sect	102	6.73	60.729	68.000	122.344	66.816	0.000	0.000	0.000	Automatic
71XY	38	60.729	Net Sect	102	6.73	60.729	68.000	122.344	66.816	0.000	0.000	0.000	Automatic
71Y	38	60.729	Net Sect	102	6.73	60.729	68.000	122.344	66.816	0.000	0.000	0.000	Automatic
72P	26	10.141	Net Sect	155	5.09	10.141	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
72Y	26	10.141	Net Sect	155	5.09	10.141	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
73X	27	57.974	Shear	111	7.31	57.974	68.000	122.344	70.324	0.000	0.000	0.000	Automatic
73Y	27	57.974	Shear	111	7.31	57.974	68.000	122.344	70.324	0.000	0.000	0.000	Automatic
74P	26	10.141	Net Sect	155	5.09	10.141	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
74X	26	10.141	Net Sect	155	5.09	10.141	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
74Y	26	10.141	Net Sect	155	5.09	10.141	27.200	24.469	16.214	0.000	0.000	0.000	Automatic
75P	27	57.974	Shear	111	7.31	57.974	68.000	122.344	70.324	0.000	0.000	0.000	Automatic
75X	27	57.974	Shear	111	7.31	57.974	68.000	122.344	70.324	0.000	0.000	0.000	Automatic
75Y	27	57.974	Shear	111	7.31	57.974	68.000	122.344	70.324	0.000	0.000	0.000	Automatic
76P	28	54.400	Shear	77	5.09	56.998	54.400	81.562	63.159	0.000	0.000	0.000	Automatic
76X	28	54.400	Shear	77	5.09	56.998	54.400	81.562	63.159	0.000	0.000	0.000	Automatic
76Y	28	54.400	Shear	77	5.09	56.998	54.400	81.562	63.159	0.000	0.000	0.000	Automatic

138BP	70	5.168	L/R	12.234	Bearing 224	5.168	13.600	12.234	21.917	0.000	0.000	0.000	0.000	Automatic
KL/R value of 223.50 exceeds maximum of 200.00 for member "138BP" ??														
139P	71	4.471	L/R	12.234	Bearing 213	4.471	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 213.20 exceeds maximum of 200.00 for member "139P" ??														
139X	71	4.471	L/R	12.234	Bearing 213	4.471	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 213.20 exceeds maximum of 200.00 for member "139X" ??														
140AP	72	6.344	L/R	12.234	Bearing 202	6.344	13.600	12.234	21.917	0.000	0.000	0.000	0.000	Automatic
KL/R value of 201.74 exceeds maximum of 200.00 for member "140AP" ??														
140BP	72	6.344	L/R	12.234	Bearing 202	6.344	13.600	12.234	21.917	0.000	0.000	0.000	0.000	Automatic
KL/R value of 201.74 exceeds maximum of 200.00 for member "140BP" ??														
141P	73	4.471	L/R	12.234	Bearing 213	4.471	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 213.20 exceeds maximum of 200.00 for member "141P" ??														
141X	73	4.471	L/R	12.234	Bearing 213	4.471	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 213.20 exceeds maximum of 200.00 for member "141X" ??														
142AP	74	6.344	L/R	12.234	Bearing 202	6.344	13.600	12.234	21.917	0.000	0.000	0.000	0.000	Automatic
KL/R value of 201.74 exceeds maximum of 200.00 for member "142AP" ??														
142BP	74	6.344	L/R	12.234	Bearing 202	6.344	13.600	12.234	21.917	0.000	0.000	0.000	0.000	Automatic
KL/R value of 201.74 exceeds maximum of 200.00 for member "142BP" ??														
143P	75	18.774	L/R	27.200	Shear 186	18.774	27.200	32.625	43.696	0.000	0.000	0.000	0.000	Automatic
144P	76	4.933	L/R	16.214	Net Sect 229	4.933	27.200	24.469	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 202.97 exceeds maximum of 200.00 for member "144P" ??														
144X	76	4.933	L/R	16.214	Net Sect 229	4.933	27.200	24.469	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 202.97 exceeds maximum of 200.00 for member "144X" ??														
144XY	76	4.933	L/R	16.214	Net Sect 229	4.933	27.200	24.469	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 202.97 exceeds maximum of 200.00 for member "144XY" ??														
144Y	76	4.933	L/R	16.214	Net Sect 229	4.933	27.200	24.469	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 202.97 exceeds maximum of 200.00 for member "144Y" ??														
145P	77	9.420	L/R	16.214	Net Sect 164	9.420	27.200	24.469	16.214	0.000	0.000	0.000	0.000	Automatic
145X	77	9.420	L/R	16.214	Net Sect 164	9.420	27.200	24.469	16.214	0.000	0.000	0.000	0.000	Automatic
146AP	78	29.570	L/R	36.271	Net Sect 109	29.570	40.800	48.937	36.271	0.000	0.000	0.000	0.000	Automatic
146AX	78	29.570	L/R	36.271	Net Sect 109	29.570	40.800	48.937	36.271	0.000	0.000	0.000	0.000	Automatic
146BP	78	29.570	L/R	36.271	Net Sect 109	29.570	40.800	48.937	36.271	0.000	0.000	0.000	0.000	Automatic
146BX	78	29.570	L/R	36.271	Net Sect 109	29.570	40.800	48.937	36.271	0.000	0.000	0.000	0.000	Automatic
147P	79	11.348	L/R	21.421	Net Sect 165	11.348	40.800	48.937	21.421	0.000	0.000	0.000	0.000	Automatic
147X	79	11.348	L/R	21.421	Net Sect 165	11.348	40.800	48.937	21.421	0.000	0.000	0.000	0.000	Automatic
147Y	79	11.348	L/R	21.421	Net Sect 165	11.348	40.800	48.937	21.421	0.000	0.000	0.000	0.000	Automatic
148P	80	11.417	L/R	21.421	Net Sect 164	11.417	40.800	48.937	21.421	0.000	0.000	0.000	0.000	Automatic
148X	80	11.417	L/R	21.421	Net Sect 164	11.417	40.800	48.937	21.421	0.000	0.000	0.000	0.000	Automatic
148Y	80	11.417	L/R	21.421	Net Sect 164	11.417	40.800	48.937	21.421	0.000	0.000	0.000	0.000	Automatic
149P	81	12.534	L/R	21.421	Net Sect 163	12.534	27.200	32.625	21.421	0.000	0.000	0.000	0.000	Automatic
149X	81	12.534	L/R	21.421	Net Sect 163	12.534	27.200	32.625	21.421	0.000	0.000	0.000	0.000	Automatic
150P	82	7.568	L/R	24.469	Bearing 255	7.568	27.200	24.469	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 203.04 exceeds maximum of 200.00 for member "150P" ??														
151P	83	3.237	L/R	12.234	Bearing 251	3.237	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 250.54 exceeds maximum of 200.00 for member "151P" ??														
151X	83	3.237	L/R	12.234	Bearing 251	3.237	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 250.54 exceeds maximum of 200.00 for member "151X" ??														
151XY	83	3.237	L/R	12.234	Bearing 251	3.237	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 250.54 exceeds maximum of 200.00 for member "151XY" ??														
151Y	83	3.237	L/R	12.234	Bearing 251	3.237	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 250.54 exceeds maximum of 200.00 for member "151Y" ??														
152P	84	5.462	L/R	12.234	Bearing 193	5.462	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
152X	84	5.462	L/R	12.234	Bearing 193	5.462	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
153P	85	19.149	L/R	27.200	Shear 163	19.149	27.200	32.625	36.271	0.000	0.000	0.000	0.000	Automatic
153X	85	19.149	L/R	27.200	Shear 163	19.149	27.200	32.625	36.271	0.000	0.000	0.000	0.000	Automatic
154P	86	4.513	L/R	12.234	Bearing 212	4.513	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 212.19 exceeds maximum of 200.00 for member "154P" ??														
154X	86	4.513	L/R	12.234	Bearing 212	4.513	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 212.19 exceeds maximum of 200.00 for member "154X" ??														
154XY	86	4.513	L/R	12.234	Bearing 212	4.513	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 212.19 exceeds maximum of 200.00 for member "154XY" ??														
154Y	86	4.513	L/R	12.234	Bearing 212	4.513	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 212.19 exceeds maximum of 200.00 for member "154Y" ??														
155P	87	10.549	L/R	12.234	Bearing 172	10.549	13.600	12.234	27.500	0.000	0.000	0.000	0.000	Automatic
156P	88	1.496	L/R	12.234	Bearing 369	1.496	13.600	12.234	16.214	0.000	0.000	0.000	0.000	Automatic
KL/R value of 368.56 exceeds maximum of 200.00 for member "156P" ??														

156X 88 1.496 L/r 12.234 Bearing 369 24.20 1.496 13.600 12.234 16.214 0.000 0.000 0.000
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156X" ??
 156XY 88 1.496 L/r 12.234 Bearing 369 24.20 1.496 13.600 12.234 16.214 0.000 0.000 0.000
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156XY" ??
 156Y 88 1.496 L/r 12.234 Bearing 369 24.20 1.496 13.600 12.234 16.214 0.000 0.000 0.000
 KL/R value of 368.56 exceeds maximum of 200.00 for member "156Y" ??
 Sum of Unfactored Dead Load and Drag Areas From Equipment, Input and Calculated:

Joint Label	Dead Load (kips)	X-Drag Area (ft ²)	Y-Drag Area (ft ²)
1P	0.0613	3.898	4.024
2P	0.104	4.522	4.535
3P	0.164	5.708	5.592
4P	0.138	4.807	5.125
5P	0.148	5.713	5.709
6P	0.218	6.729	6.576
7P	0.229	6.826	7.151
8P	0.25	7.171	7.317
9P	0.28	7.361	7.605
14P	0.661	15.209	14.806
15P	0.0615	2.467	2.021
16P	0.0615	2.467	2.021
17P	0.0671	2.467	2.021
18P	0.0582	2.542	1.729
19P	0.0801	4.015	2.979
20P	0.0652	3.016	2.735
21P	0.0955	4.869	3.417
22P	0.0707	2.604	2.313
23P	0.119	4.814	4.888
24P	0.0684	3.042	1.729
25P	0.106	4.918	3.292
26P	0.0828	3.435	2.562
27P	0.125	6.020	3.833
28P	0.0796	3.042	2.312
29P	0.142	6.098	4.917
30P	0.078	3.042	1.729
31P	0.125	5.058	3.396
32P	0.0949	3.819	2.875
33P	0.15	6.020	3.833
34P	0.088	3.042	2.312
35P	0.178	6.389	5.140
36P	0.213	5.667	3.784
37P	0.23	6.333	3.017
38P	0.239	9.167	5.324
39P	0.244	7.208	5.815
40P	0.125	3.042	1.480
41P	0.29	8.265	6.887
48P	0.125	5.937	8.109
45P	0.059	1.550	2.472
1X	0.0613	3.898	4.024
2X	0.117	4.991	5.264
2XY	0.104	4.522	4.535
3X	0.164	5.708	5.592
3XY	0.164	5.708	5.592
4X	0.138	4.807	5.125
4XY	0.138	4.807	5.125
5X	0.161	6.182	5.125
5XY	0.148	5.713	5.709
6X	0.218	6.182	6.438
6XY	0.218	6.729	6.576
6Y	0.218	6.729	6.576
7X	0.229	6.826	7.151

7XY	0.229	6.826	7.151
7Y	0.229	6.826	7.151
8X	0.263	7.640	8.046
8XY	0.25	7.171	7.317
8Y	0.263	7.640	8.046
9X	0.28	7.361	7.605
9XY	0.28	7.361	7.605
9Y	0.28	7.361	7.605
14X	0.661	15.209	14.806
14XY	0.661	15.209	14.806
14Y	0.661	15.209	14.806
15X	0.661	2.467	2.021
15XY	0.661	2.467	2.021
15Y	0.661	2.467	2.021
16X	0.615	2.467	2.021
16XY	0.615	2.467	2.021
16Y	0.615	2.467	2.021
17X	0.0671	2.467	2.021
17XY	0.0671	2.467	2.021
17Y	0.0671	2.467	2.021
18Y	0.0582	2.542	1.729
19X	0.0815	4.171	2.979
19XY	0.0801	4.015	2.979
19Y	0.0815	4.171	2.979
20X	0.0652	3.016	2.735
20XY	0.0652	3.016	2.735
20Y	0.0652	3.016	2.735
21Y	0.0355	4.869	3.417
22X	0.0707	2.604	2.313
22XY	0.0707	2.604	2.313
22Y	0.0707	2.604	2.313
23X	0.119	4.814	4.188
23XY	0.119	4.814	4.188
23Y	0.119	4.814	4.188
24Y	0.0684	3.042	1.729
25X	0.107	5.074	3.292
25XY	0.106	4.918	3.292
25Y	0.107	5.074	3.292
26X	0.0828	3.435	2.562
26XY	0.0828	3.435	2.562
26Y	0.0828	3.435	2.562
27Y	0.125	6.020	3.833
28X	0.0796	3.042	2.312
28XY	0.0796	3.042	2.312
28Y	0.0796	3.042	2.312
29X	0.142	6.098	4.917
29XY	0.142	6.098	4.917
29Y	0.142	6.098	4.917
30Y	0.078	3.042	1.729
31X	0.126	5.215	3.396
31XY	0.125	5.058	3.396
31Y	0.126	5.215	3.396
32X	0.0949	3.819	2.875
32XY	0.0949	3.819	2.875
32Y	0.0949	3.819	2.875
33Y	0.115	6.020	3.833
34X	0.088	3.042	2.312
34XY	0.088	3.042	2.312
34Y	0.088	3.042	2.312
35X	0.178	6.389	5.140
35XY	0.178	6.389	5.140
35Y	0.178	6.389	5.140
36Y	0.213	5.667	3.784
37X	0.23	6.333	3.017
37XY	0.23	6.333	3.017
37Y	0.23	6.333	3.017
38X	0.299	9.167	5.324
38XY	0.299	9.167	5.324
38Y	0.299	9.167	5.324

39Y	0.244	7.208	5.815
40X	0.125	3.042	1.480
40XY	0.125	3.042	1.480
40Y	0.125	3.042	1.480
41X	0.29	8.265	6.887
41XY	0.29	8.265	6.887
41Y	0.29	8.265	6.887
44X	0.125	5.937	8.109
45X	0.059	1.550	2.472
10S	0.236	6.829	6.906
11S	0.29	7.798	6.243
12S	0.537	14.282	14.602
13S	0.63	17.204	19.043
42S	0.972	23.048	16.380
43S	0.117	4.058	6.398
10X	0.236	6.829	6.906
10XY	0.236	6.829	6.906
10Y	0.236	6.829	6.906
11X	0.29	7.798	6.243
11XY	0.29	7.798	6.243
11Y	0.29	7.798	6.243
12X	0.537	14.282	14.602
12XY	0.537	14.282	14.602
12Y	0.537	14.282	14.602
13X	0.63	17.204	19.043
13XY	0.63	17.204	19.043
13Y	0.63	17.204	19.043
42Y	0.972	23.048	16.380
43X	0.117	4.058	6.398
Total	29.815	936.018	822.886

Unadjusted Dead Load and Drag Areas by Section:

Section	Unfactored	X-Drag	Y-Drag	X-Drag	Y-Drag
Label	Dead Load Area (kips)	All Area (ft^2)	Face Area (ft^2)	Face Area (ft^2)	Face Area (ft^2)
TOWER	29.815	936.018	822.886	377.563	200.865
Total	29.815	936.018	822.886	377.563	200.865

Angle Member Weights and Surface Areas by Section:

Section	Unfactored	Factored
Label	Weight (kips)	Surface Area (ft^2)
TOWER	29.815	31.305
Total	29.815	31.305

Sections Information:

Section	Top	Bottom	Joint	Member	Tran.	Face	Tran.	Face	Tran.	Face	Long.	Face	Long.	Face
Label	(ft)	(ft)	Z	Count	Top	Width	Bot	Width	Bot	Width	Top	Width	Bot	Width
TOWER	94.000	0.000	154	517	0.00	26.15	1105.150	28.00	38.15	3119.650				

*** Insulator Data

Clamp Properties:

Label	Stock Holding
Number	Capacity
	(lbs)
C-EX1	5e+004

Clamp Insulator Connectivity:

Clamp Structure Property Min. Required
 Label And Tip Set Vertical Load
 Attach (lbs)

C1	1P	C-EX1	No Limit
C2	1X	C-EX1	No Limit
C3	15P	C-EX1	No Limit
C4	15X	C-EX1	No Limit
C5	15XY	C-EX1	No Limit
C6	15Y	C-EX1	No Limit
C7	16P	C-EX1	No Limit
C8	16X	C-EX1	No Limit
C9	16XY	C-EX1	No Limit
C10	16Y	C-EX1	No Limit
C11	17P	C-EX1	No Limit
C12	17X	C-EX1	No Limit
C13	17XY	C-EX1	No Limit
C14	17Y	C-EX1	No Limit
C15	22P	C-EX1	No Limit
C16	22X	C-EX1	No Limit
C17	22XY	C-EX1	No Limit
C18	22Y	C-EX1	No Limit
C19	28P	C-EX1	No Limit
C20	28X	C-EX1	No Limit
C21	28XY	C-EX1	No Limit
C22	28Y	C-EX1	No Limit
C23	34P	C-EX1	No Limit
C24	34X	C-EX1	No Limit
C25	34XY	C-EX1	No Limit
C26	34Y	C-EX1	No Limit
C27	3XY	C-EX1	No Limit
C28	5XY	C-EX1	No Limit
C29	7XY	C-EX1	No Limit
C30	9XY	C-EX1	No Limit
C31	11XY	C-EX1	No Limit
C32	13XY	C-EX1	No Limit
C33	14XY	C-EX1	No Limit
C34	3Y	C-EX1	No Limit
C35	5Y	C-EX1	No Limit
C36	7Y	C-EX1	No Limit
C37	9Y	C-EX1	No Limit
C38	11Y	C-EX1	No Limit
C39	13Y	C-EX1	No Limit
C40	14Y	C-EX1	No Limit
C41	3X	C-EX1	No Limit
C42	3P	C-EX1	No Limit
C43	7X	C-EX1	No Limit
C44	7P	C-EX1	No Limit

Section Label	Z of Top	Z of Bottom	Ave. Res. of Top	Tran. Wind	Tran. Drag	Tran. Wind	Long Wind	Long Drag	Long Wind	Long Drag	Ice Weight	Total Weight
(ft)	(ft)	(ft)	(psf)	(psf)	(psf)	(psf)	(psf)	(psf)	(psf)	(psf)	(lbs)	(lbs)
3Y	344	124	0	0	0	0	0	0	0	0	0	0
5Y	344	124	0	0	0	0	0	0	0	0	0	0
7Y	344	124	0	0	0	0	0	0	0	0	0	0
9Y	344	124	0	0	0	0	0	0	0	0	0	0
11Y	516	187	0	0	0	0	0	0	0	0	0	0
13Y	688	249	0	0	0	0	0	0	0	0	0	0
3X	3132	980	0	0	0	0	0	0	0	0	0	0
3XY	3132	980	0	0	0	0	0	0	0	0	0	0
7X	555.5	-360	0	0	0	0	0	0	0	0	0	0
7XY	555.5	-360	0	0	0	0	0	0	0	0	0	0
3P	3397	1121.5	0	0	0	0	0	0	0	0	0	0
3Y	3397	1121.5	0	0	0	0	0	0	0	0	0	0
7P	555.5	-419	0	0	0	0	0	0	0	0	0	0
7Y	555.5	-419	0	0	0	0	0	0	0	0	0	0

Section Load Case Information (Standard) for "NESC Heavy":

Section Label	Z of Top	Z of Bottom	Ave. Res. of Top	Tran. Wind	Tran. Drag	Tran. Wind	Long Wind	Long Drag	Long Wind	Long Drag	Ice Weight	Total Weight
(ft)	(ft)	(ft)	(psf)	(psf)	(psf)	(psf)	(psf)	(psf)	(psf)	(psf)	(lbs)	(lbs)
TOWER	94.00	0.00	47.00	10.00	10.00	1.600	17190.9	0.00	1.600	0.0	12161	59119

Point Loads for Load Case "NESC Extreme":

Joint Label	Vertical Load (lbs)	Transverse Load (lbs)	Longitudinal Load (lbs)	Comment
1X	339	2270	0	
1P	430	4939	0	0.438 Comp Shield Wire
15P	571.5	2743	0	OPGW-120 Shield Wire
15X	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
15XY	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
15Y	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
22P	571.5	2743	0	TERN 795 Conductor Wire (Back)
22X	571.5	2743	0	TERN 795 Conductor Wire (Back)
22XY	571.5	2743	0	TERN 795 Conductor Wire (Back)
22Y	571.5	2743	0	TERN 795 Conductor Wire (Back)
16P	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
16X	571.5	2743	0	TERN 795 Conductor Wire (Back)
16XY	571.5	2743	0	TERN 795 Conductor Wire (Back)
16Y	571.5	2743	0	TERN 795 Conductor Wire (Back)
28P	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
28X	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
28XY	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
28Y	571.5	2743	0	TERN 795 Conductor Wire (Ahead)
17P	571.5	2743	0	TERN 795 Conductor Wire (Back)
17X	571.5	2743	0	TERN 795 Conductor Wire (Back)
17XY	571.5	2743	0	TERN 795 Conductor Wire (Back)
17Y	571.5	2743	0	TERN 795 Conductor Wire (Back)
34P	571.5	2743	0	TERN 795 Conductor Wire (Back)
34X	571.5	2743	0	TERN 795 Conductor Wire (Back)
34XY	571.5	2743	0	TERN 795 Conductor Wire (Back)
34Y	571.5	2743	0	TERN 795 Conductor Wire (Back)
3XY	79	358	0	TERN 795 Conductor Wire (Back)
5XY	79	358	0	Coax Cable
7XY	79	358	0	Coax Cable
9XY	79	358	0	Coax Cable
11XY	119	538	0	Coax Cable
13XY	158	717	0	Coax Cable
3Y	87	358	0	Coax Cable
5Y	87	358	0	Coax Cable
7Y	87	358	0	Coax Cable
9Y	87	358	0	Coax Cable
11Y	130	538	0	Coax Cable
13Y	173	717	0	Coax Cable

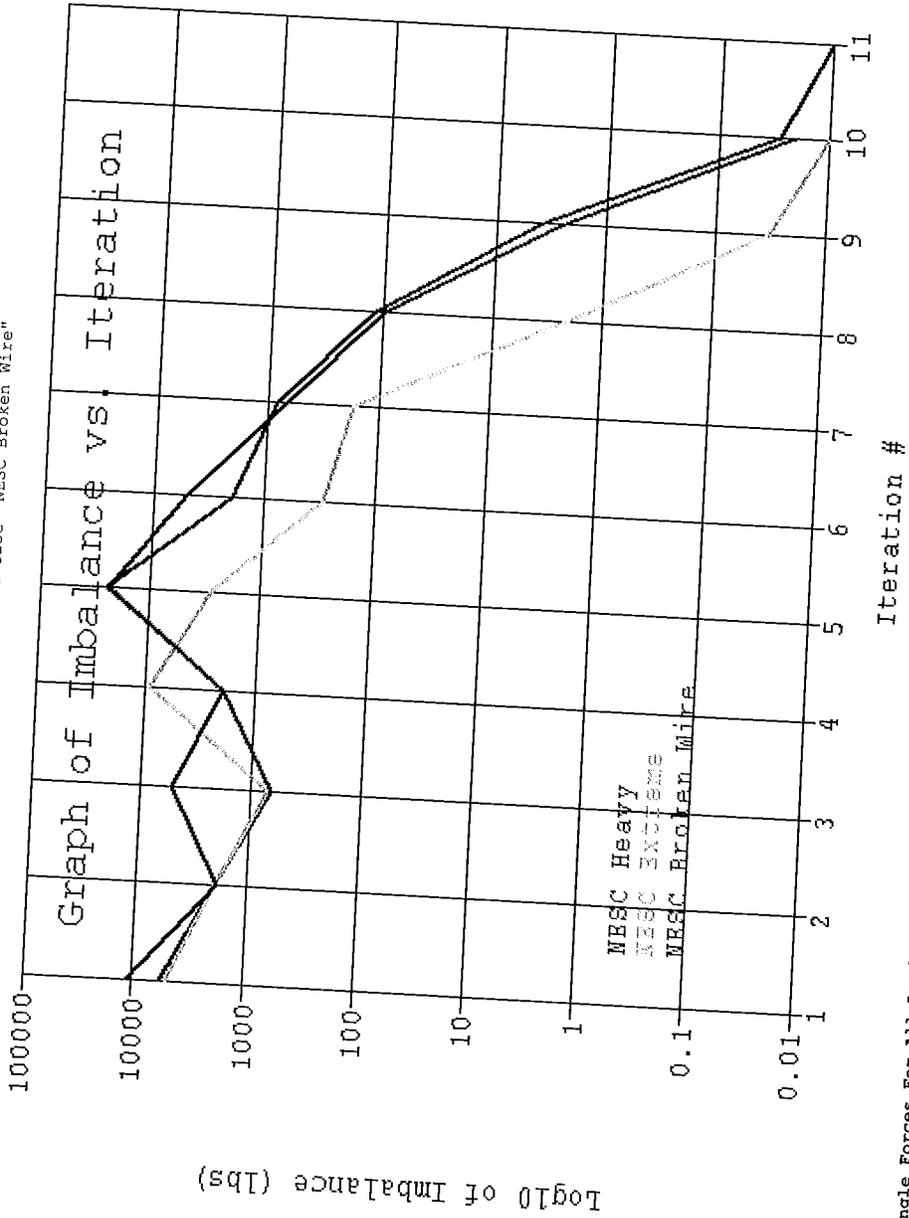
7P 555.5 -419 0 Proposed Mast Bottom Connection
 7Y 555.5 -419 0 Proposed Mast Bottom Connection

Section Load Case Information (Standard) for "NESC Broken Wire":

Section Label	Z of Top (ft)	Ave. of Bottom (ft)	Res. Above Ground (psf)	Tran. Wind Pres. (psf)	Tran. Wind Adj. Pres. (psf)	Drag Coef	Tran. Wind Load (lbs)	Long Wind Coef	Long Wind Load (lbs)	Ice Weight	Total Weight (lbs)
TOWER	94.00	0.00	47.00	10.00	10.00	1.600	17190.9	0.00	1.600	0.0	12161 59119

*** Analysis Results:

Maximum element usage is 92.14% for Angle "156XY" in load case "NESC Broken Wire"
 Maximum insulator usage is 23.70% for Clamp "C5" in load case "NESC Broken Wire"



Angle Forces For All Load Cases:
 Positive for tension - negative for compression

Group Label	Angle	Max. Usage For All LC (%)	Max. Tens. For All LC (kips)	Max. Comp. For All LC (kips)	LC 1 (kips)	LC 2 (kips)	LC 3 (kips)
1	1P	38.22	0.000	-6.745	-6.745	-5.566	-6.725
1	1X	17.56	3.849	0.000	3.756	2.849	3.849
1	1XY	16.07	3.523	0.000	3.523	2.362	3.430
2	1Y	40.35	0.000	-7.122	-7.102	-5.934	-7.122
2	2P	5.48	5.483	0.000	1.250	5.483	0.834
2	2X	9.24	0.000	-9.846	-9.846	-9.528	-8.576
2	2XY	9.36	0.000	-9.974	-9.974	-9.720	-7.362
2	2Y	5.44	5.446	0.000	1.178	5.446	0.928

3	3P	4.10	3.394	-3.374	-2.645	3.394	-3.374
3	3X	14.96	0.000	-15.940	-13.195	-10.996	-15.940
3	3XY	12.86	0.000	-13.695	-13.695	11.328	-7.349
4	4P	4.03	3.333	-3.230	-3.033	3.333	-3.230
4	4X	28.78	0.000	-30.659	-26.701	-23.727	-30.659
4	4XY	19.33	15.993	0.000	8.118	15.993	2.316
4	4Y	19.28	15.953	0.000	7.885	15.953	12.637
5	5P	25.33	0.000	-26.985	-26.985	-23.667	-21.652
5	5X	13.94	0.000	-14.848	-11.664	-5.176	-14.848
5	5XY	24.75	0.000	-26.358	-11.973	-4.766	-26.358
5	5Y	11.87	3.112	-12.641	-12.641	-4.899	3.112
6	6P	11.50	0.000	-12.246	-12.246	-5.272	-8.869
6	6X	6.51	0.000	-15.967	-12.848	-5.943	-15.967
6	6XY	14.46	0.000	-35.453	-12.621	-4.878	-35.453
6	6Y	5.45	10.500	-13.374	-13.374	-5.198	10.500
7	7P	5.44	0.000	-13.347	-13.347	-5.855	-10.376
7	7X	23.49	0.000	-57.613	-22.510	-48.272	-57.613
7	7XY	14.96	34.688	-7.197	22.510	34.688	-7.197
7	7Y	21.20	49.175	0.000	21.361	34.123	49.175
8	8P	15.09	0.000	-53.592	-53.592	-48.286	-44.832
8	8X	16.11	11.335	-37.010	-33.435	-26.689	-37.010
8	8XY	17.99	35.614	-39.514	-1.193	11.335	-39.514
8	8Y	13.93	0.000	-2.513	-2.513	10.369	35.614
9	9P	12.37	0.000	-34.173	-34.173	-26.269	-28.262
9	9X	14.14	11.982	-38.683	-36.103	-28.727	-38.683
9	9Y	10.93	38.870	-44.203	-1.600	11.982	-44.203
10	10P	11.82	0.000	-36.949	-3.255	11.982	38.870
10	10X	27.07	0.000	-84.643	-36.949	-28.093	-32.439
10	10XY	18.65	55.965	0.000	39.047	55.965	-84.643
10	10Y	24.02	72.048	0.000	37.709	54.662	72.048
11	11P	26.33	0.000	-82.339	-82.339	-74.497	-74.459
11	11X	25.31	0.000	-79.126	-76.118	-68.987	-79.126
11	11XY	16.20	48.614	-4.113	31.903	48.614	-4.113
11	11Y	21.05	63.140	0.000	30.159	47.357	63.140
12	12P	24.65	0.000	-77.085	-77.085	-68.393	-69.450
12	12X	30.88	0.000	-94.943	-90.293	-84.885	-94.943
12	12XY	21.82	65.467	0.000	46.380	65.467	15.195
12	12Y	24.16	72.472	0.000	45.101	64.337	72.472
13	13P	29.55	0.000	-90.849	-90.849	-84.207	-84.840
13	13X	31.58	0.000	-96.407	-94.614	-90.086	-96.407
13	13XY	20.28	60.848	0.000	42.512	60.848	12.666
13	13Y	22.29	66.855	0.000	40.789	59.352	66.855
14	14P	31.26	0.000	-95.434	-95.434	-89.209	-88.276
14	14X	28.07	6.153	0.000	6.153	5.618	6.109
14	14XY	29.19	0.000	-4.871	-4.753	-3.029	-4.871
14	14Y	27.00	0.000	-4.506	-4.506	-2.725	-4.387
15	15P	29.98	6.571	0.000	6.528	6.005	6.571
15	15X	10.76	0.724	-2.932	-0.350	0.724	-2.932
15	15XY	6.40	0.825	-1.745	-0.338	0.825	-1.745
15	15Y	3.38	1.007	-0.243	-0.189	1.007	-0.243
15	16P	3.16	0.942	0.000	0.210	0.942	0.872
15	16X	40.52	14.697	0.000	13.913	14.450	14.697
15	16XY	46.99	0.000	-15.152	-10.701	-11.266	-15.152
15	16Y	34.50	0.000	-11.125	-10.587	-11.125	-6.883
15	17P	40.54	14.705	0.000	14.124	14.705	11.721
15	17X	45.15	12.281	0.000	11.640	12.281	11.595
15	17XY	46.22	0.000	-12.573	-9.015	-10.087	-12.573
15	17Y	36.79	0.000	-10.007	-8.954	-10.007	-6.094
16	18P	46.05	12.527	0.000	11.840	12.527	10.273
16	18X	36.85	0.000	-10.046	-6.321	-6.834	-10.046
16	18XY	23.45	6.981	0.000	6.686	6.981	5.905
16	18Y	28.10	8.367	0.000	6.630	6.883	8.367
16	19P	25.20	0.000	-6.868	-6.385	-6.868	-1.234
16	19X	36.68	0.000	-11.826	-9.748	-9.804	-11.826
16	19XY	27.80	10.082	0.000	10.082	9.942	7.702
16	19Y	37.08	13.449	0.000	10.029	9.782	13.449
16	20P	30.45	0.000	-9.817	-9.817	-9.776	-6.279
16	20X	20.75	5.643	0.000	2.087	5.643	1.382

16	20X	40.98	0.000	-11.146	-5.941	-6.840	-11.146
16	20XY	26.32	4.073	-7.159	-6.060	-7.159	4.073
16	20Y	21.82	5.963	0.000	2.211	5.963	2.951
18	21P	4.83	0.000	-2.104	-0.491	-0.609	-2.104
18	21X	1.72	0.000	-0.750	-0.450	-0.555	-0.750
18	21XY	1.57	0.000	-0.686	-0.603	-0.686	-0.364
18	21Y	2.16	0.966	-0.739	-0.584	-0.739	0.966
18	22P	64.41	32.950	0.000	29.607	32.750	32.930
18	22X	67.40	0.000	-32.168	-26.349	-32.168	-31.255
18	22XY	68.27	0.000	-32.583	-26.580	-32.583	-17.970
18	22Y	64.36	32.903	0.000	29.590	32.903	23.092
18	23P	49.07	20.021	0.000	18.540	20.021	19.185
18	23X	47.66	0.000	-19.445	-16.372	-19.445	-17.709
18	23XY	48.25	0.000	-19.688	-16.372	-19.688	-13.495
18	23Y	49.62	20.245	0.000	18.655	20.245	15.815
19	24P	41.00	0.000	-17.861	-14.962	-17.861	-17.555
19	24X	39.43	17.597	0.000	15.150	17.597	17.518
19	24XY	39.63	17.684	0.000	15.171	17.684	10.517
19	24Y	40.39	0.000	-17.597	-14.968	-17.597	-10.679
19	25P	44.02	0.000	-21.009	-18.700	-21.009	-20.094
19	25X	41.18	21.053	0.000	18.892	21.053	19.750
19	25XY	41.05	20.985	0.000	18.923	20.985	15.700
19	25Y	43.78	0.000	-20.895	-18.718	-20.895	-15.865
19	26P	1.86	0.949	-0.233	0.397	0.949	-0.233
19	26X	8.38	0.000	-3.998	-3.998	-2.321	-2.852
19	26XY	11.30	0.000	-5.392	-3.964	-2.247	-5.392
19	26Y	2.21	1.132	0.000	0.444	0.936	1.132
21	27P	2.00	0.000	-1.075	-0.423	-0.134	-1.075
21	27X	0.72	0.000	-0.388	-0.388	-0.072	-0.041
21	27XY	3.23	0.000	-1.737	-0.400	-0.049	-1.737
21	27Y	1.31	0.000	-0.706	-0.366	-0.078	-0.706
21	28P	70.67	44.635	0.000	41.723	43.317	44.635
21	28X	70.66	0.000	-41.667	-38.165	-41.667	-41.121
21	28XY	71.18	0.000	-41.976	-38.249	-41.976	-32.768
21	28Y	69.19	43.697	0.000	41.846	43.697	34.937
21	29P	63.52	25.916	0.000	24.851	25.275	25.916
21	29X	59.21	0.000	-24.160	-22.089	-24.160	-23.052
21	29XY	59.52	0.000	-24.284	-22.129	-24.284	-20.158
21	29Y	62.55	25.519	0.000	24.994	25.519	21.584
22	30P	51.27	0.000	-27.578	-23.604	-24.203	-27.578
22	30X	41.29	22.461	0.000	20.019	22.461	19.943
22	30XY	41.39	22.519	0.000	19.905	22.519	18.038
22	30Y	45.18	0.000	-24.299	-23.713	-24.299	-18.136
22	31P	50.85	0.000	-29.987	-27.060	-27.259	-29.987
22	31X	40.37	25.497	0.000	23.400	25.497	22.288
22	31XY	40.23	25.407	0.000	23.290	25.407	22.434
22	31Y	46.15	0.000	-27.217	-27.177	-27.217	-22.616
22	32P	10.95	0.000	-5.954	-4.680	-3.553	-5.954
22	32X	5.06	1.140	-2.755	-1.122	1.140	-2.755
22	32XY	2.44	0.845	-1.330	-1.330	0.845	-0.069
22	32Y	8.58	0.000	-4.668	-4.668	-3.323	-2.940
24	33P	1.48	0.000	-3.080	-2.145	-1.370	-3.080
24	33X	0.76	0.000	-1.592	-1.592	-0.716	-1.066
24	33XY	0.91	0.000	-1.907	-1.636	-0.751	-1.907
24	33Y	1.04	0.000	-2.181	-2.181	-1.557	-0.971
24	34P	14.26	30.967	0.000	28.315	30.126	30.967
24	34X	15.23	0.000	-31.806	-28.742	-30.424	-31.806
24	34XY	14.77	0.000	-30.846	-28.923	-30.846	-23.759
24	34Y	14.05	30.525	0.000	28.415	30.525	24.187
24	35P	7.23	7.862	0.000	7.735	7.862	7.848
24	35X	6.46	0.000	-7.027	-5.683	-7.027	-3.304
24	35XY	7.03	0.000	-7.654	-5.735	-7.334	-7.654
24	35Y	7.53	8.196	0.000	7.893	8.196	7.333
25	36P	8.12	0.000	-12.068	-7.879	-12.068	-6.394
25	36X	16.95	26.751	0.000	21.477	19.369	26.751
25	36XY	13.79	21.762	0.000	21.762	19.586	15.420
25	36Y	8.19	0.000	-12.171	-7.707	-12.171	-8.437
25	37P	8.17	0.000	-12.144	-7.915	-12.144	-6.430
25	37X	16.98	26.786	0.000	21.512	19.445	26.786

25	37XY	13.82	21.798	0.000	21.798	19.662	15.455
25	37Y	8.24	0.000	-12.246	-7.743	-12.246	-8.473
25	38P	18.50	0.000	-22.645	-18.067	-22.645	-18.455
25	38X	30.95	37.889	0.000	29.013	28.249	37.889
25	38XY	24.07	29.460	0.000	29.460	28.748	18.996
25	39P	18.79	0.000	-23.002	-17.934	-23.002	-15.947
17	39P	6.98	1.900	0.000	1.131	1.900	1.110
17	39XY	18.91	0.000	-5.144	-5.054	-3.457	-5.144
17	39Y	18.57	0.770	-5.051	-5.051	-3.454	0.770
17	39Y	6.99	1.902	0.000	1.134	1.902	1.139
20	40X	12.27	1.743	0.000	0.996	1.743	0.970
20	40XY	12.34	0.000	-4.974	-4.974	-3.325	-4.954
20	40Y	4.28	1.747	-5.002	-4.870	-3.322	-5.002
23	41P	4.65	1.899	0.000	1.000	1.747	1.006
23	41X	12.11	1.899	0.000	1.218	1.899	1.213
23	41XY	12.19	0.000	-4.941	-4.941	-3.377	-4.912
23	41Y	4.66	1.900	-4.974	-4.938	-3.373	-4.974
42	42P	43.57	2.730	0.000	1.222	1.900	1.220
42	42X	42.39	2.656	0.000	2.730	1.118	2.730
42	42XY	42.39	2.656	0.000	2.656	1.025	0.160
42	42Y	43.58	2.656	0.000	2.656	1.025	2.649
42	43P	44.07	2.730	0.000	2.730	1.119	2.727
42	43X	41.38	2.761	0.000	2.761	1.158	2.759
42	43XY	41.197	2.593	0.000	2.593	0.966	2.568
42	43Y	44.06	2.760	0.000	2.592	0.966	2.629
42	44P	43.40	2.719	0.000	2.760	1.157	2.756
42	44X	42.42	2.658	0.000	2.719	1.102	2.718
42	44XY	42.96	2.692	0.000	2.658	1.038	2.626
42	44Y	43.42	2.720	0.000	2.657	1.037	2.692
41	45P	65.19	0.000	-19.498	-16.832	-18.895	-19.498
41	45X	46.62	19.022	0.000	15.143	19.022	18.683
41	45XY	47.26	19.282	0.000	15.343	19.282	8.953
41	45Y	63.03	0.000	-18.854	-16.767	-18.854	-12.882
41	46P	46.42	18.939	0.000	16.364	18.759	18.939
41	46X	63.18	0.000	-18.898	-15.066	-18.759	-18.898
41	46XY	64.03	0.000	-19.153	-15.258	-19.153	-18.716
41	46Y	45.96	18.752	0.000	16.317	18.752	12.317
40	47P	74.06	0.000	-30.644	-28.300	-30.644	-30.438
40	47X	60.81	28.951	0.000	25.574	28.951	26.348
40	47XY	60.44	28.779	0.000	25.485	28.779	22.566
40	47Y	74.02	0.000	-30.627	-28.339	-30.627	-23.654
40	48P	56.03	26.678	0.000	24.971	26.609	26.678
40	48X	62.89	0.000	-26.024	-23.980	-26.024	-25.833
40	48XY	53.61	0.000	-26.323	-24.111	-26.323	-19.967
40	48Y	56.69	26.994	0.000	25.158	26.994	21.042
39	49P	61.78	0.000	-36.528	-34.229	-34.552	-36.528
39	49X	47.89	32.563	0.000	30.081	32.563	31.477
39	49XY	48.00	32.638	0.000	30.079	32.638	26.455
39	49Y	58.48	0.000	-34.577	-34.232	-34.577	-30.099
39	50P	48.49	32.975	0.000	30.909	32.975	32.975
39	50X	54.75	0.000	-32.382	-29.380	-31.229	-32.382
39	50XY	53.04	0.000	-31.372	-29.442	-31.372	-24.307
39	50Y	47.32	32.180	0.000	30.931	32.180	27.097
43	51P	47.97	26.095	0.000	20.734	26.095	21.343
43	51X	79.38	0.000	-38.885	-30.683	-31.308	-38.885
43	51XY	65.03	0.000	-31.858	-31.129	-31.858	-21.335
43	51Y	48.74	26.514	0.000	20.643	26.514	18.480
44	52P	84.52	0.000	-46.546	-39.876	-43.201	-46.546
44	52X	46.56	37.990	0.000	30.081	37.990	31.141
44	52XY	47.59	39.158	0.000	30.304	39.158	27.185
44	52Y	80.74	0.000	-44.465	-40.496	-44.465	-31.734
45	53P	3.80	0.000	-0.098	0.371	1.045	-0.098
45	53X	5.29	1.045	-0.643	-0.192	-0.643	0.440
45	53XY	9.75	0.000	-1.187	-0.423	-1.187	-1.077
45	53Y	5.64	1.552	0.000	0.490	1.552	1.185
26	54P	1.31	0.000	-0.137	-0.137	-0.137	-0.127
26	54Y	1.44	0.000	-0.150	-0.138	-0.138	-0.150
33	55P	51.92	12.703	0.000	9.599	9.946	12.703

33	55X	79.53	-12.148	-9.015	-9.659	-12.148
33	55XY	63.25	-9.661	9.015	9.661	-5.549
33	55Y	40.67	0.000	0.000	9.951	6.166
26	56P	9.62	0.000	1.557	0.591	1.560
26	56X	10.09	0.000	1.620	0.665	1.637
26	56XY	9.99	0.000	1.620	0.665	1.593
26	56Y	9.60	0.000	1.556	0.590	1.553
33	57P	70.87	-13.170	-10.487	-9.359	-13.170
33	57X	32.33	0.000	0.000	7.239	7.911
33	57XY	29.61	0.000	5.263	7.246	2.359
33	57Y	56.43	-10.487	-10.487	-9.359	-7.524
26	58P	30.96	0.000	5.020	4.615	4.974
26	58X	40.77	0.000	-4.236	-2.579	-4.236
26	58XY	38.00	-3.948	-3.948	-2.315	-3.301
26	58Y	33.29	0.000	5.340	4.315	5.398
34	59P	51.70	-15.465	-12.644	-15.465	-12.575
34	59X	40.82	0.000	15.694	15.266	16.655
34	59XY	38.23	0.000	15.599	15.165	11.510
34	59Y	53.04	-15.866	-13.008	-15.866	-11.957
26	60P	1.51	-0.157	-0.157	-0.071	-0.150
26	60Y	1.61	0.000	-0.156	-0.070	-0.167
31	61P	63.53	0.000	21.500	24.734	25.918
31	61X	76.47	-25.193	-20.758	-24.376	-25.193
31	61XY	74.60	-24.577	-20.769	-24.577	-13.744
31	61Y	61.11	0.000	21.508	24.934	14.939
26	62P	9.18	0.000	1.489	0.517	1.482
26	62X	10.44	0.000	1.673	0.733	1.693
26	62XY	10.33	0.000	1.674	0.735	1.644
26	62Y	9.29	0.000	1.490	0.517	1.506
32	63P	72.86	-24.283	-20.517	-21.807	-24.283
32	63X	47.90	0.000	15.057	19.545	18.283
32	63XY	48.32	0.000	15.066	19.715	9.146
32	63Y	65.95	-21.980	-20.529	-21.980	-14.576
35	64P	48.71	0.000	11.400	13.178	13.249
35	64X	52.16	-13.679	-10.958	-13.679	-13.615
35	64XY	52.88	-13.867	-11.098	-13.867	-5.923
35	64Y	48.42	0.000	11.365	13.171	8.515
36	65P	63.17	-26.138	-22.468	-26.138	-23.315
36	65X	57.90	0.000	25.333	27.570	25.868
36	65XY	57.71	0.000	25.421	27.476	21.583
36	65Y	62.68	-25.936	-22.502	-25.936	-19.909
26	66P	1.59	-0.165	-0.165	-0.081	-0.155
26	66Y	1.65	-0.171	-0.171	-0.081	-0.171
29	67P	62.04	0.000	30.538	32.323	33.749
29	67X	70.50	-32.949	-29.709	-31.898	-32.949
29	67XY	68.70	-32.109	-29.702	-32.109	-24.013
29	67Y	59.81	0.000	30.530	32.534	24.854
26	68P	10.19	0.000	1.443	0.473	1.439
26	68X	12.47	0.000	1.733	0.784	1.766
26	68XY	12.24	0.000	1.735	0.786	1.695
26	68Y	10.33	0.000	1.443	0.472	1.463
30	69P	74.73	-30.931	-28.187	-28.226	-30.931
30	69X	52.13	0.000	22.554	25.869	25.258
30	69XY	52.48	0.000	22.548	26.045	17.767
30	69Y	68.64	-28.401	-28.182	-28.401	-23.378
37	70P	46.25	0.000	17.607	18.871	18.825
37	70X	49.02	-18.940	-17.534	-18.940	-18.841
37	70XY	49.58	-19.158	-17.628	-19.158	-14.646
37	70Y	46.93	0.000	17.742	19.147	14.806
38	71P	48.34	-29.356	-27.143	-29.356	-28.227
38	71X	45.17	0.000	29.558	30.178	29.859
38	71XY	45.44	0.000	29.685	30.358	27.143
38	71Y	48.70	-29.572	-27.333	-29.572	-24.283
26	72P	5.20	-0.527	-0.452	-0.234	-0.527
26	72Y	4.51	-0.457	-0.457	-0.235	-0.382
27	73P	35.77	0.000	21.703	22.723	24.321
27	73X	39.22	-22.736	-20.249	-21.955	-22.736
27	73XY	38.34	-22.229	-20.342	-22.229	-16.511
27	73Y	33.82	0.000	21.805	23.000	17.848

26	74P	0.85	0.138	0.000	0.138	0.043	0.114
26	74X	1.72	0.279	0.000	0.254	0.165	0.279
26	74XY	1.58	0.256	0.000	0.256	0.169	0.226
26	74Y	0.95	0.153	0.000	0.138	0.040	0.153
27	75P	40.02	20.169	-23.199	-20.818	-21.366	-23.199
27	75X	29.166	19.901	0.000	17.658	19.638	20.169
27	75XY	29.27	19.901	0.000	17.755	19.901	14.016
27	75Y	37.31	0.000	-21.627	-20.907	-21.627	-17.289
28	76P	40.12	21.826	0.000	20.437	20.894	21.826
28	76X	35.93	0.000	-19.548	-17.573	-19.548	-17.710
28	76XY	36.02	0.000	-19.596	-17.540	-19.596	-16.150
28	76Y	38.54	20.963	0.000	20.503	20.963	17.867
46	77P	6.21	0.000	-7.965	-7.452	-7.965	-7.076
46	77X	8.34	8.602	0.000	8.123	8.602	5.657
46	77XY	9.58	9.878	0.000	7.966	8.391	9.878
46	77Y	6.08	0.000	-7.792	-7.499	-7.792	-7.338
46	78P	0.92	0.000	-1.168	-1.038	-1.168	-1.168
46	78X	5.21	0.000	-6.519	-3.862	-2.085	-6.619
46	78XY	2.98	0.000	-3.782	-3.782	-2.153	-0.573
46	78Y	0.89	0.000	-1.128	-1.128	-0.175	-0.843
47	79P	6.37	1.033	0.000	0.368	0.401	1.033
47	79X	9.98	0.000	-1.226	-0.419	-0.324	-1.226
47	79XY	3.21	0.272	-0.395	-0.395	-0.297	0.272
47	79Y	5.02	0.374	-0.617	0.343	0.374	-0.617
48	80P	3.28	0.892	0.000	0.731	0.892	0.314
48	80X	25.10	6.826	-0.978	-0.762	-0.978	6.826
48	80XY	30.65	0.000	-7.926	-0.738	-0.896	-7.926
48	80Y	4.66	1.267	0.000	0.711	0.815	1.267
48	81X	29.54	8.034	-1.386	-0.604	-0.899	-1.386
48	81XY	26.76	1.034	0.000	0.767	0.943	8.034
48	81Y	3.74	1.017	-6.921	0.786	1.017	-6.921
48	82P	2.77	0.000	-0.968	-0.818	-0.968	-0.417
48	82X	20.56	0.000	-0.717	-0.717	-0.272	-0.523
48	82XY	28.23	5.593	-0.727	-0.727	-0.350	5.593
48	82Y	5.45	0.000	-7.301	-0.654	-0.257	-7.301
49	83P	2.16	0.882	-1.411	-0.789	-0.362	-1.411
49	83X	17.74	7.238	0.000	0.763	0.882	0.052
49	83XY	19.84	0.000	-0.798	-0.599	-0.798	7.238
49	83Y	3.76	1.533	-8.097	-0.527	-0.571	-8.097
49	84P	3.76	0.000	0.000	0.651	0.657	-1.533
49	84X	20.33	8.296	-1.535	-0.695	-0.699	-1.535
49	84XY	17.63	0.908	0.000	0.695	0.685	8.296
49	84Y	2.24	0.000	-7.194	0.768	0.908	-7.194
49	85P	5.75	0.000	-0.915	-0.753	-0.915	-0.109
49	85X	14.74	6.016	-2.346	-1.864	-1.860	-2.346
49	85XY	17.36	0.603	-0.395	-0.395	0.349	6.016
49	85Y	5.19	0.000	-7.081	-0.288	0.603	-7.081
50	86P	5.40	0.768	-2.118	-2.118	1.652	-2.044
50	86X	8.24	0.000	-1.139	0.706	0.768	-1.539
50	86XY	5.00	0.000	-1.056	-0.863	-0.868	-1.738
50	86Y	10.08	2.742	-1.056	-1.056	-0.838	-0.088
51	87P	13.43	0.000	0.000	0.404	0.526	2.742
51	87X	11.63	0.000	-2.502	-2.502	-2.275	-0.673
51	87XY	7.02	2.846	0.000	1.202	1.816	2.846
51	87Y	23.74	0.000	-0.314	1.441	1.719	-0.314
51	88P	28.57	0.000	-4.424	-2.173	-2.035	-4.424
51	88X	8.03	1.964	-4.146	-2.880	-2.589	-4.146
51	88XY	12.22	0.990	-0.422	1.485	1.964	-0.422
51	88Y	22.37	0.000	0.000	1.214	2.064	2.990
52	89P	84.39	0.538	-3.247	-3.247	-2.846	-2.497
52	89X	11.57	2.220	0.000	3.118	3.165	0.538
52	89XY	21.57	1.001	-0.809	0.653	1.119	2.220
52	89Y	77.86	0.000	-2.920	-2.920	-2.807	-0.809
53	90P	15.56	4.488	-2.920	-2.920	-2.042	4.488
53	90X	27.56	7.949	0.000	2.042	2.042	7.949
53	90XY	28.35	8.177	0.000	4.386	4.177	5.431
53	90Y	14.21	4.099	0.000	1.617	4.099	2.640
54	91P	9.69	2.665	0.000	0.818	2.665	2.252

54	91X	21.13	5.810	0.000	3.294	5.810	3.966
54	91Y	19.98	5.494	0.000	3.600	5.494	2.809
54	91Z	11.66	3.205	-0.054	1.408	3.205	-0.054
55	92P	9.54	2.090	0.000	2.090	1.640	1.551
55	92X	13.16	0.000	-1.498	-0.926	-0.587	-1.498
55	93P	13.59	0.000	-1.547	-1.035	-1.547	-0.977
55	93X	8.63	1.891	0.000	1.891	1.849	1.701
56	94P	10.14	1.240	0.000	1.240	0.982	0.769
56	94X	11.97	0.000	-0.535	-0.065	-0.535	-0.506
55	95P	5.75	0.000	-0.655	-0.251	-0.655	-0.166
55	95X	7.54	1.653	0.000	1.640	1.217	1.653
56	96P	14.66	1.794	0.000	1.794	1.547	1.482
56	96X	21.13	0.000	-0.945	-0.416	-0.945	-0.651
57	97P	8.07	0.000	-3.216	-3.216	-2.643	-3.165
57	97X	3.63	1.483	0.000	0.522	1.483	0.565
58	98P	3.69	1.469	0.000	1.459	1.340	1.469
58	98X	1.56	0.000	-0.516	-0.132	-0.516	-0.036
58	98Y	1.56	0.000	-0.515	-0.186	-0.515	-0.267
58	98Z	3.49	1.391	0.000	1.391	1.304	1.213
59	99P	14.74	4.010	0.000	4.009	4.010	1.667
59	99X	9.88	0.000	-2.472	-1.936	-2.472	-1.856
60	100P	13.24	0.000	-2.167	-0.015	-2.167	-2.089
60	100X	46.39	0.000	-7.594	-5.085	-7.594	-4.994
61	101P	3.12	0.000	-0.139	-0.024	-0.007	-0.139
62	102P	23.11	0.000	-2.383	-1.038	-1.087	-2.383
62	102X	20.93	2.561	0.000	1.069	1.095	2.561
62	102Y	9.39	1.149	-0.309	1.065	1.149	-0.309
62	102Z	11.07	0.494	-1.141	-1.033	-1.141	0.494
63	103P	6.81	1.854	0.000	1.734	1.854	1.600
63	103X	12.66	0.000	-1.881	-1.840	-1.881	-1.880
64	104P	17.17	0.000	-2.336	-1.127	-1.172	-2.336
64	104X	18.58	2.527	0.000	1.222	1.200	2.527
64	104Y	9.17	1.248	-0.092	1.222	1.248	-0.092
64	104Z	8.98	0.239	-1.222	-1.124	-1.222	0.239
65	105P	3.18	0.697	0.000	0.697	0.417	0.631
65	105X	6.56	0.000	-0.747	-0.493	-0.362	-0.747
66	106P	7.43	0.713	-1.010	0.282	0.713	-1.010
66	106X	7.16	0.974	-0.817	-0.632	-0.817	0.974
66	106Y	11.92	0.000	-1.621	-0.628	-0.758	-1.621
66	106Z	11.63	1.581	0.000	0.290	0.669	1.581
67	107P	0.36	0.049	-0.003	0.002	0.049	-0.003
67	107X	75.78	0.000	-8.835	-0.657	-0.321	-8.835
67	107Y	51.69	7.029	-0.654	-0.654	-0.316	7.029
67	107Z	0.39	0.054	0.000	0.007	0.054	0.036
68	108P	0.26	0.000	-0.036	-0.002	-0.036	-0.010
68	108X	36.70	0.464	-4.991	0.464	0.226	-4.991
61	109P	0.32	0.016	-0.014	-0.014	-0.006	0.016
62	110P	29.76	0.000	-3.068	-1.864	-2.126	-3.068
62	110X	24.79	3.033	0.000	1.880	2.131	3.033
62	110Y	18.55	2.270	0.000	1.872	2.270	0.443
62	110Z	21.94	0.000	-2.262	-1.852	-2.262	-0.458
63	111P	11.37	3.082	0.000	2.705	3.092	2.590
63	111X	20.84	0.000	-3.096	-2.732	-3.096	-2.549
64	112P	19.44	0.000	-2.643	-1.537	-1.626	-2.643
64	112X	19.32	2.627	0.000	1.555	1.632	2.627
64	112Y	12.80	1.754	0.000	1.546	1.754	0.287
64	112Z	12.89	0.000	-1.753	-1.530	-1.753	-0.323
65	113P	5.13	1.124	0.000	0.979	1.124	0.924
65	113X	10.01	0.000	-1.140	-0.992	-1.140	-0.926
66	114P	6.36	0.367	-0.865	0.320	0.367	-0.865
66	114X	6.39	0.869	-0.372	-0.333	-0.372	0.869
66	114Y	11.05	0.000	-1.503	-0.318	-0.218	-1.503
66	114Z	11.40	1.550	0.000	0.336	0.246	1.550
67	115P	1.65	0.225	0.000	0.000	0.157	0.152
67	115X	6.00	0.000	-0.700	-0.700	-0.441	-0.697
67	115Y	5.97	0.000	-0.695	-0.695	-0.435	-0.695
67	115Z	1.69	0.229	0.000	0.162	0.229	0.201
68	116P	1.13	0.000	-0.154	-0.154	-0.117	-0.154
68	116X	3.59	0.489	0.000	0.489	0.305	0.488

61	117P	1.75	0.214	0.000	0.205	0.095	0.214
62	118P	29.78	-3.070	-2.249	-2.269	-2.269	-3.070
63	118X	22.67	0.000	2.774	0.000	1.970	2.774
62	118XY	18.55	0.000	2.269	1.967	2.269	0.974
63	119P	23.26	-2.398	-2.241	-2.398	-2.398	-1.257
63	119X	14.48	0.000	3.837	3.838	3.715	3.715
63	119XY	25.13	-3.734	-3.443	-3.443	-3.734	-3.295
64	120P	23.10	0.000	-3.278	-2.527	-2.508	-3.278
64	120XY	22.48	0.000	2.337	2.337	2.408	3.057
64	120Y	18.56	-2.628	-2.523	-2.523	-2.628	1.431
65	121P	19.32	-1.488	-1.533	-1.533	-1.488	-1.631
65	121X	7.71	0.000	1.689	1.610	1.639	1.304
66	122P	20.75	-2.822	-1.540	-1.300	-2.822	-1.300
66	122X	13.02	0.000	0.553	0.862	1.771	1.771
66	122XY	7.53	1.024	0.706	0.577	1.024	-0.706
66	122Y	11.30	0.000	-1.537	-1.537	-1.426	-0.166
67	123P	0.93	-0.108	-0.108	-0.108	-0.108	-0.108
67	123X	7.04	-0.821	-0.821	-0.821	-0.450	-0.809
67	123XY	7.04	-0.821	-0.821	-0.817	-0.445	-0.821
67	123Y	0.88	-0.103	-0.103	-0.103	0.074	-0.821
68	124P	0.78	0.106	0.106	0.106	-0.018	0.102
68	124X	4.05	0.000	0.551	0.288	0.550	0.550
69	125P	30.01	-1.342	-0.017	-0.017	-0.020	-1.342
70	126AP	14.40	0.000	0.017	0.020	1.762	1.762
70	126BP	14.52	0.000	0.030	0.036	1.776	1.776
71	127P	30.36	-1.357	-0.032	-0.032	-0.033	-1.357
71	127X	30.04	-1.343	-0.014	-0.019	-1.343	-1.343
72	128AP	13.11	1.803	0.031	0.035	1.603	1.603
72	128BP	13.11	1.598	0.020	0.021	1.598	1.598
73	129P	13.06	-3.545	-2.829	-2.829	-2.056	-3.545
73	129X	13.01	0.000	1.592	1.007	0.305	0.305
74	130AP	14.30	0.000	0.186	0.194	1.750	1.750
74	130BP	11.53	-0.098	-0.078	-0.098	1.410	1.410
69	131P	34.97	-1.564	-0.034	-0.034	-1.564	-1.564
70	132AP	16.50	2.019	0.053	0.000	2.019	2.019
70	132BP	17.21	0.000	0.091	0.053	2.305	2.305
71	133P	33.28	-1.577	-0.051	-0.019	-1.577	-1.577
71	133X	35.45	-0.040	-0.040	-0.007	-1.585	-1.585
72	134AP	15.65	0.000	0.116	0.090	1.915	1.915
72	134BP	15.07	-0.034	0.009	-0.034	1.844	1.844
73	135P	34.95	-1.563	-0.077	-0.052	-1.563	-1.563
73	135X	34.96	-1.563	-0.023	-0.007	-1.563	-1.563
74	136AP	14.90	0.000	0.069	0.031	1.823	1.823
74	136BP	15.52	0.000	0.065	0.031	1.899	1.899
69	137P	26.90	-1.203	-0.040	-0.019	-1.203	-1.203
70	138AP	12.49	-0.041	-0.008	-0.041	1.528	1.528
70	138BP	13.46	0.000	0.115	0.091	1.646	1.646
71	139P	27.00	-1.207	-0.050	-0.028	-1.207	-1.207
71	139X	27.67	-1.237	-0.062	-0.040	-1.237	-1.237
72	140AP	12.31	0.000	0.148	0.132	1.506	1.506
72	140BP	11.52	-0.012	0.013	-0.012	1.409	1.409
73	141P	28.48	-1.273	-0.170	-0.158	-1.273	-1.273
73	141X	25.29	-1.131	0.032	0.052	-1.131	-1.131
74	142AP	11.56	0.000	0.121	0.093	1.414	1.414
74	142BP	11.82	0.000	0.067	0.040	1.446	1.446
75	143P	7.15	0.000	1.944	1.230	1.932	1.932
76	144P	17.61	-0.868	-0.868	-0.425	0.189	0.189
76	144X	52.13	-2.571	-1.537	-1.084	-2.571	-2.571
76	144XY	31.06	-1.532	-1.532	-1.050	-0.467	-0.467
76	144Y	39.11	-1.829	-0.875	-0.461	-1.929	-1.929
77	145P	7.22	-0.860	-0.860	-0.433	-0.680	-0.680
77	145X	7.92	-0.746	-0.746	-0.462	-0.745	-0.745
78	146AP	7.41	0.000	2.336	1.409	2.688	2.688
78	146AX	7.44	0.000	2.598	1.787	2.272	2.272
78	146BP	6.46	0.000	2.341	1.399	2.007	2.007
78	146BX	8.60	0.000	2.708	1.807	3.118	3.118
79	147P	11.89	-1.350	-1.350	-0.997	-0.871	-0.871
79	147X	15.10	-1.714	-1.125	-0.572	-1.714	-1.714

79	147XY	9.79	0.000	-1.110	-1.110	-0.544	-0.529
79	147Y	16.06	0.000	-1.825	-1.342	-1.011	-1.825
80	148F	10.67	0.000	-1.218	-1.218	-0.678	-0.561
80	148P	16.20	0.000	-1.850	-1.275	-0.904	-1.850
80	148XY	11.17	0.000	-1.276	-1.276	-0.886	-0.706
80	148Y	16.50	0.000	-1.884	-1.220	-0.688	-1.884
81	149P	8.57	1.836	0.000	1.833	1.281	1.836
81	149X	7.59	1.627	0.000	1.622	0.909	1.627
82	150P	5.48	0.000	-0.414	-0.391	-0.202	-0.414
83	151P	19.31	0.000	-0.625	-0.492	-0.625	-0.383
83	151X	7.38	0.902	0.000	0.902	0.838	0.815
83	151XY	7.77	0.951	0.000	0.923	0.896	0.951
83	151Y	21.14	0.000	-0.684	-0.512	-0.684	-0.519
84	152P	1.21	0.000	-0.066	-0.066	-0.040	-0.035
84	152X	0.93	0.000	-0.051	-0.051	-0.024	-0.051
85	153P	1.20	0.024	-0.230	-0.230	-0.030	0.024
85	153X	3.57	0.000	-0.685	-0.685	-0.516	-0.671
86	154P	2.81	0.344	-0.001	0.344	0.302	-0.001
86	154X	0.76	0.092	-0.006	0.092	-0.006	0.090
86	154XY	0.96	0.117	0.000	0.112	0.046	0.117
87	155P	2.69	0.329	-0.075	0.329	0.253	-0.075
87	155Y	2.87	0.351	-0.010	-0.010	0.351	0.088
88	156P	53.96	0.373	-0.807	0.179	0.373	-0.807
88	156X	77.08	0.153	-1.153	-0.675	-1.153	0.153
88	156XY	92.14	0.000	-1.378	-0.594	-0.921	-1.378
88	156Y	6.16	0.754	0.000	0.096	0.137	0.754

*** Analysis Results for Load Case No. 1 "NESC Heavy" - Number of iterations in SAPS 11

Equilibrium Joint Positions and Rotations for Load Case "NESC Heavy":

Joint Label	X-Displ (ft)	Y-Displ (ft)	Z-Displ (ft)	X-Rot (deg)	Y-Rot (deg)	Z-Rot (deg)	X-Pos (ft)	Y-Pos (ft)	Z-Pos (ft)
1P	-0.001829	0.1834	-0.01886	0.0000	0.0000	0.0000	-0.001829	14.18 93.98	
2P	-0.0009175	0.1521	-0.01924	-0.0817	0.0055	-0.0131	3.499	15.15 84.98	
3P	-0.001112	0.1448	-0.01929	-0.1089	-0.0052	-0.0069	3.499	15.14 79.98	
4P	-0.0002981	0.1314	-0.01915	-0.2026	-0.0062	-0.0108	3.5	15.13 74.98	
5P	-0.0003351	0.1137	-0.01784	-0.1482	-0.0039	-0.0148	3.5	15.11 69.98	
6P	-0.0003946	0.1048	-0.01696	-0.2309	-0.0054	-0.0235	3.5	15.09 59.98	
7P	0.0002041	0.08773	-0.01575	-0.1674	-0.0054	-0.0313	3.5	15.07 54.98	
8P	0.0002825	0.06824	-0.01575	-0.1356	-0.0071	-0.0435	3.5	15.06 49.98	
9P	-6.725e-005	0.05788	0	0.0000	0.0000	0.0000	13.07	19.07 79.97	0
14P	0	0	0	0.0000	0.0000	0.0000	3.499	22.14 79.97	
15P	-0.000785	0.1449	-0.03292	-0.1128	0.0052	-0.0006	3.5	22.11 64.97	
16P	-0.0002249	0.1049	-0.03386	-0.1221	-0.0063	0.0058	3.5	22.06 49.97	
17P	0.0002031	0.05798	-0.03378	-0.1627	-0.0069	0.0184	3.5	22.06 49.97	
18P	-0.002783	0.1494	-0.009437	-0.0060	-0.0021	-0.0028	3.497	0.1494 84.99	
19P	-0.002629	0.1493	-0.009028	-0.0271	0.0009	0.0003	3.497	6.149 84.99	
20P	-0.002361	0.1508	-0.009068	-0.0837	0.0032	-0.0137	3.498	10.65 84.99	
21P	-0.001369	0.1465	-0.009403	0.0024	-0.0043	-0.0038	3.499	0.1465 79.99	
22P	-0.001029	0.1456	-0.009404	0.0096	-0.0047	-0.0025	3.499	6.146 79.99	
23P	-0.0009974	0.1446	-0.01028	-0.0696	-0.0049	0.0031	3.499	10.64 79.99	
24P	-0.003302	0.1099	-0.008082	0.0147	-0.0014	0.0001	3.497	0.1099 69.99	
25P	-0.003275	0.1099	-0.005423	0.0473	0.0007	-0.0105	3.497	6.11 69.99	
26P	-0.001756	0.1122	-0.004701	-0.0932	0.0023	-0.0217	3.498	10.61 70	
27P	-0.0006722	0.1079	-0.008043	0.0261	-0.0026	-0.0045	3.499	0.1079 64.99	
28P	-0.0002716	0.1063	-0.005782	0.0250	-0.0041	-0.0025	3.5	6.106 64.99	
29P	-0.0003239	0.1048	-0.006196	-0.0752	-0.0052	0.0057	3.5	0.06198 49.99	
30P	-0.003056	0.064	-0.006611	0.0159	0.0005	0.0008	3.5	10.6 64.99	
31P	-0.003041	0.06396	-0.003086	0.0536	0.0025	-0.0125	3.497	0.064 54.99	
32P	-0.001371	0.06666	-0.001943	-0.0923	0.0040	-0.0208	3.497	6.064 55	
33P	-2.03e-005	0.06198	-0.006069	0.0280	-0.0039	-0.0067	3.499	10.57 55	
34P	0.0004092	0.05995	-0.003434	0.0307	-0.0051	0.0001	3.5	0.06198 49.99	
35P	-0.0001081	0.0582	-0.003732	-0.0841	-0.0060	0.0153	3.5	6.06 50	
36P	0.0003503	0.02912	-0.005951	-0.0177	0.016	-0.0020	5.375	0.02917 38.99	
37P	9.264e-006	0.02912	-0.006993	0.0022	0.0024	0.0152	5.375	5.279 39.99	
38P	-0.001463	0.02978	-0.007354	0.0396	0.0033	-0.0003	5.374	10.53 39.99	
39P	9.033e-005	0.02548	-0.005886	-0.109	-0.0011	-0.0006	6.333	0.02548 34.99	
40P	0.0001968	0.02523	-0.008927	-0.0115	-0.0035	-0.0006	6.333	5.275 34.99	
41P	0.0002324	0.02498	-0.008549	-0.0305	0.0000	0.0000	6.333	10.52 34.99	
42P	0.0003482	0.03381	0.02527	0.0000	0.0000	0.0000	0.0003482	17.97 17.78	
43P	0.0002406	0.03254	-0.1541	0.0000	0.0000	0.0000	0.0002406	10.53 39.85	
1X	-0.002736	0.1783	0.0008852	0.0000	0.0000	0.0000	-0.002736	-13.82 94	
2X	-0.002222	0.1516	0.002594	-0.0682	0.0000	0.0000	3.498	-14.85 85	
2XY	-0.001974	0.1517	0.002177	-0.0668	0.0030	0.0057	3.501	15.15 84.98	
2Y	-0.001477	0.1523	-0.01956	-0.0823	-0.0109	0.0000	3.501	15.15 84.98	
3X	-0.001544	0.1451	0.003068	-0.1084	-0.0035	-0.0008	3.498	-14.85 80	
3XY	-0.00205	0.1454	0.002658	-0.1076	-0.0033	0.0015	3.501	15.14 79.98	
3Y	-0.0008348	0.145	-0.01962	-0.1099	0.0001	-0.0017	3.501	15.13 74.98	
4X	-0.001533	0.1302	0.003721	-0.2126	-0.0001	0.0003	3.499	-14.89 70	
4XY	-0.001485	0.1305	0.003334	-0.2132	-0.0065	0.0044	3.501	15.11 69.98	
4Y	-0.001211	0.1315	-0.01945	-0.2031	0.0014	-0.0023	3.501	14.87 75	
5X	-0.001245	0.1134	0.003361	-0.1303	-0.0068	0.0015	3.501	15.13 74.98	
5XY	-0.001223	0.1136	0.002986	-0.1309	0.0006	0.0071	3.499	-14.89 70	
5Y	-0.0007568	0.1138	-0.01813	-0.1478	-0.0086	-0.0029	3.501	15.11 69.98	
6X	-0.0007474	0.1051	0.00394	-0.1845	0.0010	-0.0070	3.499	-14.89 65	
6XY	-0.001166	0.1052	0.003597	-0.1854	-0.0068	0.0098	3.501	14.69 65	
6Y	-0.0003274	0.105	-0.01754	-0.1623	0.0023	0.0073	3.5	15.1 64.98	
7X	-0.0008487	0.08612	0.004257	-0.2362	-0.0007	-0.0126	3.499	-14.91 60	
7XY	-0.0005924	0.08618	0.00393	-0.2366	-0.0048	0.0167	3.501	14.91 60	
7Y	-0.000577	0.08792	-0.01721	-0.2314	0.0015	-0.0138	3.501	15.09 59.98	
8X	-0.0005598	0.06795	0.003789	-0.1442	-0.0045	-0.0183	3.499	-14.93 55	
8XY	-0.0004186	0.06802	0.003488	-0.1436	-0.0008	0.0237	3.5	-14.93 55	

8Y	-0.0003272	0.06833	-0.01598	-0.1682	-0.0091	0.0203
9X	-0.0002437	0.05883	0.003824	-0.1380	-0.0011	-0.0338
9Y	-0.000304	0.06895	0.003552	-0.1380	0.0027	0.0358
14X	0.0003042	0.05796	-0.01521	-0.1358	0.0047	0.0378
14XY	0	0	0	0.0000	0.0000	0.0000
14Y	0	0	0	0.0000	0.0000	0.0000
15X	-0.001974	0.1458	0.007077	0.0048	0.0000	0.0000
15XY	-0.002051	0.146	0.006526	0.0061	-0.0035	-0.0049
15Y	-0.0007847	0.1451	-0.00333	-0.0033	-0.0008	0.0008
16X	-0.001059	0.1057	-0.01059	-0.1131	0.0001	0.0002
16XY	-0.001141	0.1059	-0.01059	-0.1103	0.0010	0.0002
16Y	-0.0002072	0.1051	-0.0341	-0.1025	-0.0107	-0.0068
17X	-0.0003471	0.05934	0.01224	-0.1223	0.0022	-0.0043
17XY	-0.0004395	0.05946	0.01187	-0.0345	-0.0011	0.0155
17Y	-0.001854	0.05805	-0.03402	-0.1630	0.0028	-0.0194
18X	-0.002777	0.1495	-0.00964	-0.0059	-0.0045	-0.0174
18XY	-0.002859	0.1494	-0.009428	0.0087	-0.0052	0.0059
18Y	-0.002854	0.1496	-0.009692	0.0088	-0.0012	-0.0016
20X	-0.002679	0.1495	-0.009225	0.0282	-0.0068	-0.0101
20XY	-0.002194	0.1505	-0.007514	-0.0598	-0.0075	0.0050
20Y	-0.001603	0.1507	-0.007787	-0.0987	0.0009	0.0074
21Y	-0.001361	0.1456	-0.009199	-0.0850	-0.0088	-0.0089
22X	-0.001719	0.1456	-0.009606	0.0027	-0.0016	0.0007
22XY	-0.001346	0.1458	-0.01008	-0.0067	-0.0023	-0.0021
22Y	-0.001381	0.1458	-0.01008	-0.0067	-0.0023	-0.0021
23X	-0.001728	0.1445	-0.009602	0.0098	-0.0009	-0.0009
23XY	-0.001596	0.1447	-0.006824	-0.0930	-0.0037	-0.0024
23Y	-0.001184	0.1448	-0.01049	-0.0705	-0.0028	-0.0069
24Y	-0.003329	0.11	-0.00847	0.0149	-0.0040	-0.0046
25X	-0.003329	0.11	-0.00847	0.0149	-0.0040	-0.0046
25XY	-0.003258	0.1101	-0.01078	0.0366	-0.0035	0.0091
25Y	-0.002016	0.1121	-0.005974	0.0477	-0.0059	-0.0111
26XY	-0.002008	0.1122	-0.00991	0.0137	-0.0011	-0.0021
26Y	-0.00173	0.1123	-0.005013	-0.1074	-0.0051	-0.0170
27Y	-0.0006674	0.1063	-0.01078	-0.0929	-0.0073	-0.0203
28X	-0.001069	0.1064	-0.008431	0.0263	-0.0023	0.0156
28XY	-0.0005148	0.1064	-0.006124	0.0255	-0.0042	-0.0004
28Y	-0.0008203	0.1049	-0.008462	-0.0978	-0.0000	0.0003
29X	-0.001015	0.1048	-0.008462	-0.0978	-0.0000	0.0003
29XY	-0.0007493	0.1049	-0.008462	-0.0978	-0.0000	0.0003
29Y	-0.0005858	0.1049	-0.008462	-0.0978	-0.0000	0.0003
30Y	-0.003043	0.06406	-0.006503	0.0748	0.0008	-0.0089
31X	-0.003016	0.06403	-0.006331	0.0160	-0.0008	-0.0064
31XY	-0.002995	0.0641	-0.009072	0.0476	-0.0014	0.0099
31Y	-0.003024	0.06403	-0.003283	0.0481	-0.0034	0.0127
32X	-0.001446	0.0665	-0.003283	0.0539	-0.0069	-0.0107
32XY	-0.001457	0.06657	-0.009489	-0.0961	-0.0029	0.0254
32Y	-0.001313	0.06673	-0.002124	-0.0959	-0.0021	0.0254
33Y	-8.992e-005	0.06207	-0.00629	0.0225	-0.0081	-0.0280
34X	-0.0004866	0.06026	-0.009242	0.0282	-0.0007	0.0052
34XY	-0.0002117	0.06036	-0.009242	0.0238	-0.0027	0.0012
34Y	-0.000369	0.06003	-0.009491	0.0243	-0.0008	-0.0025
35X	2.125e-005	0.0308	-0.003631	0.0308	0.0022	0.0025
35XY	-0.0004307	0.05875	-0.007694	-0.0960	-0.0018	-0.0018
35Y	0.0002486	0.05885	-0.007979	0.0960	-0.0018	-0.0104
36Y	-7.612e-005	0.02928	-0.003926	-0.0842	-0.0033	-0.0153
37X	-0.0001075	0.02921	-0.00625	-0.0175	0.0032	-0.0009
37XY	-0.0002819	0.02932	-0.004618	-0.0662	0.0007	-0.0109
37Y	0.0003641	0.02923	-0.007209	0.0025	-0.0025	0.0098
38X	-0.001049	0.02988	-0.003306	-0.0539	-0.0039	-0.0163
38XY	0.001119	0.02999	-0.003352	-0.0540	-0.0017	-0.0016
38Y	0.001937	0.02989	-0.007601	-0.0384	-0.0017	-0.0016
39Y	0.0002469	0.0256	-0.006196	-0.0108	0.0004	-0.0008
40X	0.0001073	0.0248	-0.004639	-0.0198	0.0004	-0.0004
40XY	0.0001387	0.02492	-0.004966	-0.0196	0.0012	0.0001
40Y	0.0002374	0.02536	-0.007218	-0.0113	0.0028	-0.0005

41X	-2.222e-005	0.02413	-0.001537	-0.0527	0.0035	-0.0036	6.333	-10.48	35
41Y	0.0001854	0.02423	-0.001864	-0.0530	-0.0045	0.0028	-6.333	-10.48	35
41Z	0.0003023	0.02512	-0.000813	-0.0302	0.0053	0.0007	-6.333	10.53	34.99
45X	3.913e-005	0.1584	-0.01061	0.0000	0.0000	0.0000	0.0001809	-17.47	17.74
10S	0.001257	0.02420	-0.01518	-0.0200	0.0000	0.0000	3.913e-005	10.47	39.87
11S	0.0004637	0.02995	-0.0114	-0.0889	0.0034	-0.0282	4.459	15.45	44.98
12S	0.0008895	0.02435	-0.013	-0.0518	-0.0085	0.0132	5.415	15.84	39.99
43S	0.0002536	0.01061	-0.009468	-0.0592	0.0007	-0.0132	6.373	16.25	34.99
42S	0.0003433	0.01061	-0.001127	-0.0051	0.0007	-0.0132	8.541	17.16	23.66
43S	0.0002892	0.03107	-0.01457	-0.0890	0.0019	-0.0000	8.541	0.01041	23.67
10XY	-0.0004858	0.04183	0.005229	-0.1808	-0.0027	-0.0029	0.0002892	15.85	39.99
10Y	0.0002131	0.04191	0.004947	-0.1808	-0.0001	0.0035	4.457	-15.37	45.01
11Y	-3.568e-005	0.04213	-0.01154	-0.1696	0.0012	0.0032	-4.457	15.45	44.98
11XY	2.541e-006	0.03014	0.005084	-0.1015	-0.0019	-0.0118	5.415	15.78	40.01
12X	-0.0001228	0.03006	-0.01464	-0.0890	0.0046	0.0265	-5.414	15.84	39.99
12XY	0.0003158	0.02323	0.005173	-0.0704	-0.0064	0.0042	6.372	-16.2	35.01
13X	-0.0007507	0.0245	0.004892	-0.0706	-0.0075	-0.0050	-6.372	16.2	35
13XY	0.001022	0.0107	-0.01323	-0.0516	0.0082	0.0119	8.54	-17.13	23.67
13Y	0.0003485	0.0108	0.003669	-0.0521	0.0031	0.0013	-8.54	17.13	23.67
42Y	0.0002592	0.01053	-0.009676	-0.0594	-0.0001	0.0114	-8.541	17.16	23.66
43X	-1.981e-005	0.02935	0.001273	-0.0050	-0.0016	-0.0006	-8.541	0.01053	23.67
			0.005935	-0.1014	-0.0019	-0.0007	-1.981e-005	-15.79	40.01

Joint Support Reactions for Load Case "NESC Heavy":

Joint Label	X Force (kips)	X Usage %	Y Force (kips)	Y Usage %	Z Force (kips)	Z Usage %	Uplift Force (kips)	Uplift Usage %	Result. Force (kips)	Result. Usage %	X-Moment (ft-k)	X-Moment Usage %	Y-Moment (ft-k)	Y-Moment Usage %	Z-Moment (ft-k)	Z-Moment Usage %	Max. Usage %
14P	-23.13	0.0	-32.46	0.0	123.91	0.0	0.0	130.16	0.0	0.0	0.13	0.0	0.2	0.0	0.04	0.0	0.0
14X	14.36	0.0	-22.60	0.0	-66.21	0.0	0.0	71.42	0.0	0.0	0.31	0.0	0.0	0.0	-0.01	0.0	0.0
14XY	-14.25	0.0	-22.63	0.0	-64.94	0.0	0.0	70.23	0.0	0.0	0.34	0.0	-0.1	0.0	0.01	0.0	0.0
14Y	23.02	0.0	-32.89	0.0	124.72	0.0	0.0	131.02	0.0	0.0	0.15	0.0	-0.2	0.0	-0.05	0.0	0.0

Joint Displacements, Loads and Member Forces on Joints for Load Case "NESC Heavy":

Joint Label	X External Load (kips)	Y External Load (kips)	Z External Load (kips)	X Member Force (kips)	Y Member Force (kips)	Z Member Force (kips)	X Disp. (ft)	Y Disp. (ft)	Z Disp. (ft)
1P	0.0000	5.7421	-1.7446	0.0000	-5.7421	1.7446	-0.0018	0.1834	-0.0189
2P	0.0000	0.0994	-0.2208	0.0000	-0.0994	0.2208	-0.0009	0.1521	-0.0192
3P	0.0000	1.2431	-3.7360	0.0000	-1.2431	3.7360	-0.0011	0.1448	-0.0193
4P	0.0000	0.1068	-0.2751	0.0000	-0.1068	0.2751	-0.0003	0.1314	-0.0192
5P	0.0000	0.1208	-0.3039	0.0000	-0.1208	0.3039	-0.0003	0.1137	-0.0178
6P	0.0000	0.1373	-0.4363	0.0000	-0.1373	0.4363	-0.0004	0.1048	-0.0173
7P	0.0000	-0.2798	-0.5943	0.0000	0.2798	0.5943	0.0002	0.0877	-0.0170
8P	0.0000	0.1465	-0.4796	0.0000	-0.1465	0.4796	0.0003	0.0682	-0.0158
9P	0.0000	0.1544	-0.5437	0.0000	-0.1544	0.5437	-0.0001	0.0579	-0.0150
14P	0.0000	0.2837	-1.2171	23.1254	32.1809	-122.6948	0.0000	0.0000	0.0000
15P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	-0.0008	0.1449	-0.0329
16P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	-0.0002	0.1049	-0.0339
17P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.6031	0.0002	0.0580	-0.0338
18P	0.0000	0.0403	-0.1290	0.0000	-0.0403	0.1290	-0.0028	0.1494	-0.0094
19P	0.0000	0.0670	-0.1797	0.0000	-0.0670	0.1797	-0.0027	0.1494	-0.0094
20P	0.0000	0.0629	-0.1467	0.0000	-0.0629	0.1467	-0.0024	0.1508	-0.0091
21P	0.0000	0.0787	-0.2152	0.0000	-0.0787	0.2152	-0.0014	0.1465	-0.0094
22P	0.0000	3.3633	-1.6160	0.0000	-3.3633	1.6160	-0.0010	0.1456	-0.0094
23P	0.0000	0.0943	-0.2539	0.0000	-0.0943	0.2539	-0.0010	0.1456	-0.0094
24P	0.0000	0.0403	-0.1498	0.0000	-0.0403	0.1498	-0.0033	0.1446	-0.0103
25P	0.0000	0.0720	-0.2278	0.0000	-0.0720	0.2278	-0.0033	0.1099	-0.0081
26P	0.0000	0.0570	-0.1766	0.0000	-0.0570	0.1766	-0.0018	0.1122	-0.0047
27P	0.0000	0.0853	-0.2711	0.0000	-0.0853	0.2711	-0.0007	0.1079	-0.0047
28P	0.0000	3.3633	-1.6342	0.0000	-3.3633	1.6342	-0.0003	0.1063	-0.0058
29P	0.0000	0.1060	-0.3019	0.0000	-0.1060	0.3019	-0.0003	0.1048	-0.0062

30P	0.0000	0.0403	-0.1649	0.0000	-0.0403	0.1649	-0.0031	0.0640	-0.0061
31P	0.0000	0.0737	-0.2597	0.0000	-0.0737	0.2597	-0.0030	0.0640	-0.0031
32P	0.0000	0.0620	-0.1998	-0.0000	-0.0620	0.1998	-0.0014	0.0667	-0.0019
33P	0.0000	0.0853	-0.3124	0.0000	-0.0853	0.3124	0.0000	0.0620	-0.0061
34P	0.0000	3.3633	-1.6474	0.0000	-3.3633	1.6474	0.0004	0.0599	-0.0034
35P	0.0000	0.1096	-0.3625	0.0000	-0.1096	0.3625	-0.0001	0.0582	-0.0037
36P	0.0000	0.0854	-0.4182	0.0000	-0.0854	0.4182	0.0004	0.0292	-0.0060
37P	0.0000	0.0656	-0.4356	-0.0000	-0.0656	0.4356	0.0000	0.0291	-0.0069
38P	0.0000	0.1097	-0.5719	0.0000	-0.1097	0.5719	-0.0015	0.0298	-0.0074
39P	0.0000	0.1286	-0.4881	0.0000	-0.1286	0.4881	0.0001	0.0255	-0.0059
40P	0.0000	0.0355	-0.2388	0.0000	-0.0355	0.2388	0.0002	0.0252	-0.0069
41P	0.0000	0.1458	-0.5677	-0.0000	-0.1458	0.5677	0.0002	0.0252	-0.0069
42P	0.0000	0.0539	-0.2780	0.0000	-0.0539	0.2780	0.0003	0.0250	-0.0085
43P	0.0000	3.9001	-0.1462	0.0000	-3.9001	0.1462	0.0002	0.0250	-0.0085
44P	0.0000	0.1157	-0.3756	0.0000	-0.1157	0.3756	-0.0027	0.1783	0.0009
45P	0.0000	0.0994	-0.2208	0.0000	-0.0994	0.2208	-0.0022	0.1516	0.0026
1X	0.0000	1.1016	-0.2503	0.0000	-1.1016	0.2503	-0.0015	0.1523	0.0022
2X	0.0000	1.2256	-3.4710	0.0000	-1.2256	3.4710	-0.0015	0.1451	0.0031
3X	0.0000	1.3671	-4.0800	0.0000	-1.3671	4.0800	-0.0020	0.1454	0.0027
4X	0.0000	0.1068	-0.2751	0.0000	-0.1068	0.2751	-0.0018	0.1302	0.0037
5X	0.0000	0.1371	-0.2751	0.0000	-0.1371	0.2751	-0.0015	0.1305	0.0033
6X	0.0000	0.2448	-0.3334	0.0000	-0.2448	0.3334	-0.0012	0.1315	-0.0195
7X	0.0000	0.2611	-0.6479	0.0000	-0.2611	0.6479	-0.0012	0.1134	0.0034
8X	0.0000	0.1373	-0.4363	0.0000	-0.1373	0.4363	-0.0007	0.1138	0.0030
9X	0.0000	0.1373	-0.4363	0.0000	-0.1373	0.4363	-0.0007	0.1138	0.0030
10X	0.0000	-0.2208	-0.9943	0.0000	0.2208	0.9943	-0.0003	0.1050	-0.0175
11X	0.0000	-0.0968	-1.3383	0.0000	0.0968	1.3383	-0.0006	0.0862	0.0043
12X	0.0000	0.1629	-0.5091	0.0000	-0.1629	0.5091	-0.0006	0.0862	0.0043
13X	0.0000	0.1629	-0.5091	0.0000	-0.1629	0.5091	-0.0006	0.0862	0.0043
14X	0.0000	0.2784	-0.8877	0.0000	-0.2784	0.8877	-0.0003	0.0590	0.0036
15X	0.0000	0.2837	-1.2171	0.0000	-0.2837	1.2171	-0.0003	0.0580	-0.0172
16X	0.0000	0.2837	-1.2171	0.0000	-0.2837	1.2171	-0.0003	0.0580	-0.0172
17X	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	-0.0020	0.1458	0.0071
18X	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	-0.0020	0.1458	0.0071
19X	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	-0.0011	0.1059	0.0102
20X	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	-0.0002	0.1051	-0.0341
21X	0.0000	3.3540	-1.6031	0.0000	-3.3540	1.6031	-0.0004	0.0593	0.0122
22X	0.0000	3.3540	-1.6031	0.0000	-3.3540	1.6031	-0.0004	0.0593	0.0122
23X	0.0000	0.0670	-0.1290	0.0000	-0.0670	0.1290	-0.0028	0.0581	-0.0340
24X	0.0000	0.0670	-0.1290	0.0000	-0.0670	0.1290	-0.0028	0.0581	-0.0340
25X	0.0000	0.0629	-0.1829	0.0000	-0.0629	0.1829	-0.0029	0.1494	-0.0094
26X	0.0000	0.0629	-0.1829	0.0000	-0.0629	0.1829	-0.0029	0.1494	-0.0094
27X	0.0000	0.0629	-0.1467	0.0000	-0.0629	0.1467	-0.0027	0.1496	-0.0097
28X	0.0000	0.0629	-0.1467	0.0000	-0.0629	0.1467	-0.0027	0.1496	-0.0097
29X	0.0000	0.0787	-0.1467	0.0000	-0.0787	0.1467	-0.0027	0.1506	-0.0075
30X	0.0000	3.3633	-1.6160	0.0000	-3.3633	1.6160	-0.0017	0.1456	-0.0096
31X	0.0000	3.3633	-1.6160	0.0000	-3.3633	1.6160	-0.0017	0.1456	-0.0096
32X	0.0000	0.0943	-0.2539	0.0000	-0.0943	0.2539	-0.0017	0.1458	-0.0101
33X	0.0000	0.0943	-0.2539	0.0000	-0.0943	0.2539	-0.0017	0.1458	-0.0101
34X	0.0000	0.0403	-0.1498	0.0000	-0.0403	0.1498	-0.0012	0.1448	-0.0065
35X	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	-0.0033	0.1100	-0.0085
36X	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	-0.0033	0.1100	-0.0085
37X	0.0000	0.0720	-0.2278	0.0000	-0.0720	0.2278	-0.0033	0.1101	-0.0108
38X	0.0000	0.0720	-0.2278	0.0000	-0.0720	0.2278	-0.0033	0.1101	-0.0108
39X	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	-0.0033	0.1100	-0.0058
40X	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	-0.0033	0.1100	-0.0058

Label	Angle	Torsion	Origin X Moment (ft-lbs)	Origin Y Moment (ft-lbs)	End X Moment (ft-lbs)	End Y Moment (ft-lbs)	X Shear (lbs)	Y Shear (lbs)
26X	0.0000	0.0570	-0.1766	-0.0000	-0.0570	0.1766	-0.0020	0.1121
26XY	0.0000	0.0570	-0.1766	0.0000	0.0570	0.1766	0.0020	0.1122
26Y	0.0000	0.0570	-0.1766	0.0000	-0.0570	0.1766	-0.0017	0.1123
27X	0.0000	0.0853	-0.2711	0.0000	0.0853	0.2711	-0.0007	0.1080
27XY	0.0000	0.0853	-0.2711	0.0000	-0.0853	0.2711	0.0007	0.1080
27Y	0.0000	0.0853	-0.2711	0.0000	0.0853	0.2711	-0.0007	0.1080
28X	0.0000	0.0000	1.6342	0.0000	0.0000	1.6342	-0.0011	0.1063
28XY	0.0000	0.0000	1.6342	0.0000	0.0000	1.6342	0.0011	0.1063
28Y	0.0000	0.0000	1.6342	0.0000	0.0000	1.6342	-0.0011	0.1063
29X	0.0000	0.1060	-0.3019	0.0000	0.1060	0.3019	-0.0010	0.1064
29XY	0.0000	0.1060	-0.3019	0.0000	-0.1060	0.3019	0.0010	0.1064
29Y	0.0000	0.1060	-0.3019	0.0000	0.1060	0.3019	-0.0010	0.1064
30X	0.0000	0.0403	-0.1649	0.0000	0.0403	0.1649	-0.0030	0.1049
30XY	0.0000	0.0403	-0.1649	0.0000	-0.0403	0.1649	0.0030	0.1049
30Y	0.0000	0.0403	-0.1649	0.0000	0.0403	0.1649	-0.0030	0.1049
31X	0.0000	0.0737	-0.2629	0.0000	0.0737	0.2629	-0.0030	0.0641
31XY	0.0000	0.0737	-0.2629	0.0000	-0.0737	0.2629	0.0030	0.0641
31Y	0.0000	0.0737	-0.2629	0.0000	0.0737	0.2629	-0.0030	0.0641
32X	0.0000	0.0620	-0.1998	0.0000	0.0620	0.1998	-0.0014	0.0665
32XY	0.0000	0.0620	-0.1998	0.0000	-0.0620	0.1998	0.0014	0.0665
32Y	0.0000	0.0620	-0.1998	0.0000	0.0620	0.1998	-0.0014	0.0665
33X	0.0000	0.0853	-0.3124	0.0000	0.0853	0.3124	-0.0013	0.0667
33XY	0.0000	0.0853	-0.3124	0.0000	-0.0853	0.3124	0.0013	0.0667
33Y	0.0000	0.0853	-0.3124	0.0000	0.0853	0.3124	-0.0013	0.0667
34X	0.0000	0.3633	-1.6474	0.0000	0.3633	1.6474	-0.0005	0.0603
34XY	0.0000	0.3633	-1.6474	0.0000	-0.3633	1.6474	0.0005	0.0603
34Y	0.0000	0.3633	-1.6474	0.0000	0.3633	1.6474	-0.0005	0.0603
35X	0.0000	0.1096	-0.3625	0.0000	0.1096	0.3625	-0.0004	0.0589
35XY	0.0000	0.1096	-0.3625	0.0000	-0.1096	0.3625	0.0004	0.0589
35Y	0.0000	0.1096	-0.3625	0.0000	0.1096	0.3625	-0.0004	0.0589
36X	0.0000	0.0854	-0.4182	0.0000	0.0854	0.4182	-0.0001	0.0583
36Y	0.0000	0.0854	-0.4182	0.0000	0.0854	0.4182	0.0001	0.0583
36XY	0.0000	0.0854	-0.4182	0.0000	-0.0854	0.4182	0.0001	0.0583
37X	0.0000	0.0656	-0.4356	0.0000	0.0656	0.4356	-0.0001	0.0293
37Y	0.0000	0.0656	-0.4356	0.0000	0.0656	0.4356	0.0001	0.0293
37XY	0.0000	0.0656	-0.4356	0.0000	-0.0656	0.4356	0.0001	0.0293
38X	0.0000	0.1097	-0.5719	0.0000	0.1097	0.5719	-0.0010	0.0299
38XY	0.0000	0.1097	-0.5719	0.0000	-0.1097	0.5719	0.0010	0.0299
38Y	0.0000	0.1097	-0.5719	0.0000	0.1097	0.5719	-0.0010	0.0299
39X	0.0000	0.1286	-0.4881	0.0000	0.1286	0.4881	-0.0002	0.0256
39Y	0.0000	0.1286	-0.4881	0.0000	0.1286	0.4881	0.0002	0.0256
39XY	0.0000	0.1286	-0.4881	0.0000	-0.1286	0.4881	0.0002	0.0256
40X	0.0000	0.0355	-0.2388	0.0000	0.0355	0.2388	-0.0001	0.0248
40XY	0.0000	0.0355	-0.2388	0.0000	-0.0355	0.2388	0.0001	0.0248
40Y	0.0000	0.0355	-0.2388	0.0000	0.0355	0.2388	-0.0001	0.0248
41X	0.0000	0.1458	-0.5677	0.0000	0.1458	0.5677	-0.0002	0.0241
41XY	0.0000	0.1458	-0.5677	0.0000	-0.1458	0.5677	0.0002	0.0241
41Y	0.0000	0.1458	-0.5677	0.0000	0.1458	0.5677	-0.0002	0.0241
42X	0.0000	0.1730	-0.2780	0.0000	0.1730	0.2780	-0.0002	0.0154
42Y	0.0000	0.1730	-0.2780	0.0000	0.1730	0.2780	0.0002	0.0154
42XY	0.0000	0.1730	-0.2780	0.0000	-0.1730	0.2780	0.0002	0.0154
43X	0.0000	0.1365	-0.2574	0.0000	0.1365	0.2574	-0.0003	0.0104
43Y	0.0000	0.1365	-0.2574	0.0000	0.1365	0.2574	0.0003	0.0104
43XY	0.0000	0.1365	-0.2574	0.0000	-0.1365	0.2574	0.0003	0.0104
44X	0.0000	0.1348	-0.4484	0.0000	0.1348	0.4484	-0.0005	0.0311
44Y	0.0000	0.1348	-0.4484	0.0000	0.1348	0.4484	0.0005	0.0311
44XY	0.0000	0.1348	-0.4484	0.0000	-0.1348	0.4484	0.0005	0.0311
45X	0.0000	0.1173	-0.5387	0.0000	0.1173	0.5387	-0.0002	0.0418
45Y	0.0000	0.1173	-0.5387	0.0000	0.1173	0.5387	0.0002	0.0418
45XY	0.0000	0.1173	-0.5387	0.0000	-0.1173	0.5387	0.0002	0.0418
46X	0.0000	0.3043	-1.0547	0.0000	0.3043	1.0547	-0.0001	0.0301
46Y	0.0000	0.3043	-1.0547	0.0000	0.3043	1.0547	0.0001	0.0301
46XY	0.0000	0.3043	-1.0547	0.0000	-0.3043	1.0547	0.0001	0.0301
47X	0.0000	0.2907	-1.0330	0.0000	0.2907	1.0330	-0.0002	0.0231
47Y	0.0000	0.2907	-1.0330	0.0000	0.2907	1.0330	0.0002	0.0231
47XY	0.0000	0.2907	-1.0330	0.0000	-0.2907	1.0330	0.0002	0.0231
48X	0.0000	0.3706	-1.2107	0.0000	0.3706	1.2107	-0.0002	0.0245
48Y	0.0000	0.3706	-1.2107	0.0000	0.3706	1.2107	0.0002	0.0245
48XY	0.0000	0.3706	-1.2107	0.0000	-0.3706	1.2107	0.0002	0.0245
49X	0.0000	0.6196	-1.8987	0.0000	0.6196	1.8987	-0.0010	0.0108
49Y	0.0000	0.6196	-1.8987	0.0000	0.6196	1.8987	0.0010	0.0108
49XY	0.0000	0.6196	-1.8987	0.0000	-0.6196	1.8987	0.0010	0.0108
50X	0.0000	0.3438	-1.8597	0.0000	0.3438	1.8597	-0.0003	0.0108
50Y	0.0000	0.3438	-1.8597	0.0000	0.3438	1.8597	0.0003	0.0108
50XY	0.0000	0.3438	-1.8597	0.0000	-0.3438	1.8597	0.0003	0.0108
51X	0.0000	0.1365	-0.2574	0.0000	0.1365	0.2574	-0.0000	0.0293
51Y	0.0000	0.1365	-0.2574	0.0000	0.1365	0.2574	0.0000	0.0293
51XY	0.0000	0.1365	-0.2574	0.0000	-0.1365	0.2574	0.0000	0.0293

Moments for Angles Modeled as Beams:

Label	Angle	Torsion	Origin X Moment (ft-lbs)	Origin Y Moment (ft-lbs)	End X Moment (ft-lbs)	End Y Moment (ft-lbs)	X Shear (lbs)	Y Shear (lbs)
2P	-29.47	272.46	1.72	608.82	134.17	176.25	27.19	
2X	-4.77	289.48	-1.72	786.02	-80.13	215.12	-16.37	

2XY	19.84	286.27	1.57	789.65	79.56	215.20	16.22
2Y	7.92	281.67	-1.57	822.48	-137.06	180.83	-27.73
3P	18.74	-488.13	-134.36	668.40	-121.60	36.05	-51.20
3X	-5.27	-1025.17	80.30	262.61	37.84	-152.53	23.63
3XY	-13.37	-1031.47	-79.95	273.22	-40.33	-151.67	-24.06
3Y	3.10	-501.38	137.44	648.95	120.83	29.51	51.65
4P	18.75	-668.39	121.62	-1340.11	-3.66	-401.80	23.62
4X	-5.27	-262.61	-37.84	-1279.82	45.11	-308.46	1.45
4XY	-13.37	-273.22	40.33	-1290.21	-47.06	-312.66	-1.36
4Y	3.10	-668.95	-120.83	-1331.90	2.76	-396.27	-23.62
5P	4.51	1861.01	6.48	2045.29	133.77	781.35	28.05
5X	40.02	1926.79	-47.96	2596.19	-144.19	904.70	-38.51
5Y	-12.38	1940.48	49.68	2614.14	140.83	911.03	38.13
6P	48.50	1853.77	-5.31	2032.69	-139.46	777.39	-28.88
6X	203.61	-2071.66	-135.67	2545.20	-189.93	94.71	-67.19
6Y	148.28	-3159.75	146.36	362.66	282.32	-559.44	81.73
7P	203.78	-2054.20	-143.45	310.08	-281.55	-574.00	-85.00
7X	148.21	-3545.18	200.03	2853.82	190.84	119.93	66.59
7XY	-182.95	-362.67	262.35	-6629.15	0.05	-1883.52	-67.30
7Y	-170.52	-310.09	-281.58	-6645.98	9.50	-1391.08	-52.32
8P	319.64	7435.37	50.10	5271.12	535.45	-1922.98	68.76
8X	405.59	7323.53	-3.66	6904.43	-236.21	2541.74	385.70
8Y	-457.96	7524.19	-537.82	5322.00	129.02	2862.17	-48.35
9P	-70.60	578.45	5003.37	-556.75	3063.96	4.22	-402.22
9X	-474.15	-2484.48	6486.82	-1272.99	4103.58	-736.00	1579.88
9Y	507.44	-2605.97	-6492.98	-1324.71	-4156.77	-769.94	-2085.23
10P	-70.29	556.81	-5085.49	-576.92	3082.46	-11.31	2085.23
10X	-474.19	1273.46	-3063.95	2267.82	2155.60	553.26	-177.91
10XY	507.42	1325.23	4103.43	-947.40	1083.39	63.77	-595.22
10Y	19.49	576.93	4156.61	-852.54	-1042.70	92.47	609.58
11P	-221.36	-2493.19	3082.46	2330.58	-2133.49	569.47	185.88
11X	306.21	1304.35	-1744.95	90.61	-140.34	273.10	-369.10
11XY	-307.16	1211.21	1722.58	62.06	106.48	249.28	358.10
11Y	212.49	-2564.30	2751.44	-808.09	629.50	-660.54	662.26
12P	-19.45	767.58	701.55	433.06	615.98	103.79	113.90
12X	73.39	19.82	-71.90	-102.69	431.87	-7.16	31.10
12XY	-75.08	51.01	120.16	-55.75	-408.25	-0.41	-24.89
12Y	15.68	776.98	-699.64	469.22	-584.80	107.73	-111.03
13P	-4.40	-424.40	-599.26	-89.42	182.66	-21.26	-17.24
13X	61.16	97.49	-409.76	-149.24	284.68	-2.14	-6.00
13XY	-65.28	47.29	387.11	-133.98	-282.22	-6.06	4.34
13Y	-0.10	-465.61	565.65	-139.65	-221.76	-25.04	14.23
15P	1.72	4.62	-3.69	52.98	0.84	9.60	-0.47
15X	-1.57	4.62	3.69	-16.90	16.36	-2.05	3.34
15XY	1.57	6.47	-5.72	-14.97	0.89	-1.42	1.10
16P	1.72	-52.98	-0.84	-268.55	-22.95	10.44	-4.78
16X	1.73	16.90	-16.36	227.98	-28.23	-71.43	-6.46
16XY	-1.57	14.97	-0.89	224.19	16.60	54.43	-7.65
16Y	-1.56	-56.16	-0.89	-276.44	25.32	-73.89	10.72
17P	1.72	288.55	28.22	272.45	29.49	120.19	12.82
17X	1.73	-227.98	18.03	-283.48	4.76	-115.02	5.07
17XY	-1.57	-224.19	-16.61	-286.27	-19.83	-113.46	-8.10
17Y	-1.56	276.44	-25.32	281.67	-7.94	123.99	-7.39
18P	-0.19	21.03	-0.48	31.56	1.37	8.77	0.15
18X	-0.19	21.03	0.48	35.36	2.92	9.40	0.57
18XY	0.38	21.78	0.13	35.51	-2.05	9.55	-0.32
18Y	0.38	21.78	0.13	32.08	-2.38	8.98	-0.42
19P	-0.19	-31.56	-1.57	-185.66	9.60	-48.28	1.83
19X	-0.19	-35.36	-2.92	133.22	5.86	21.74	0.65
19XY	0.38	-35.51	2.05	132.41	-9.74	21.53	-1.71
19Y	0.38	-32.08	2.38	-188.27	-4.84	-48.98	-0.55
20P	-0.20	185.66	9.60	109.07	-29.03	65.49	-8.58
20X	-0.18	-133.22	-5.86	-105.32	-12.02	-53.02	-3.97
20XY	0.37	-132.41	9.74	-104.14	26.13	-52.57	7.97

20Y	0.38	188.27	4.84	111.61	10.50	66.64	3.41
21P	2.84	-33.27	116.52	-171.20	19.54	-17.41	-17.41
21X	2.84	0.73	33.27	-75.66	65.27	-12.49	16.42
21XY	-2.158	-0.67	34.39	-77.62	67.57	-13.05	16.99
21Y	-2.158	-0.67	-34.39	115.97	-74.29	19.22	-18.11
22P	2.90	-116.52	71.20	-781.45	18.36	-199.44	19.90
22X	2.89	75.66	-65.27	755.42	-28.12	184.77	-20.77
22XY	-2.153	77.62	-67.57	760.31	-38.88	186.30	-23.66
22Y	-2.153	-115.97	74.29	-781.80	30.71	-139.40	23.32
23P	2.86	781.45	-18.37	520.90	14.27	289.32	-0.91
23X	2.90	-755.42	28.13	-646.97	-45.34	-311.73	-3.82
23XY	-2.156	-760.31	38.87	-650.27	-0.94	-313.55	8.43
23Y	-2.152	781.80	-30.70	521.87	51.55	289.61	4.63
24P	-2.02	43.57	0.03	39.81	6.80	13.90	1.13
24X	-2.02	43.57	0.03	87.65	7.35	21.86	1.23
24XY	2.49	42.45	1.25	86.68	-4.76	21.52	-0.59
24Y	2.49	42.45	-1.25	39.42	-9.71	13.65	-1.83
25P	-2.02	-39.81	-6.80	-514.55	32.26	-123.23	5.66
25X	-2.02	-87.65	-7.35	440.02	29.52	78.28	4.93
25XY	2.49	-86.68	4.76	444.01	-39.39	79.38	-7.70
25Y	2.49	-39.42	9.71	-514.29	-19.51	-123.09	-2.18
26P	-2.10	514.55	-32.25	98.45	-133.70	136.22	-36.88
26X	-1.97	-440.02	-29.52	-29.39	-88.04	-104.32	-26.13
26XY	2.42	-444.01	39.40	-31.02	127.80	-105.57	37.16
26Y	2.54	514.29	19.51	100.10	84.30	136.53	23.07
27P	3.17	-6.30	-44.49	156.66	-102.17	23.06	-24.44
27X	3.17	-6.30	44.49	-143.23	83.91	-24.92	21.40
27XY	-2.92	-6.51	45.79	-143.37	101.70	-25.31	24.58
27Y	-2.92	-6.51	45.79	157.30	-91.01	25.13	-22.80
28P	3.25	-156.66	102.17	-997.84	54.52	-256.40	34.81
28X	3.24	143.23	-83.91	971.51	5.43	247.86	-17.45
28XY	-2.84	145.37	-101.70	975.81	-85.14	249.29	-41.54
28Y	-2.84	-157.31	91.01	-1001.51	-8.39	-257.36	18.35
29P	3.08	997.84	-54.53	565.22	-115.46	347.22	-37.76
29X	3.41	971.51	-5.42	-694.37	-257.36	-370.32	-58.41
29XY	-3.00	-971.51	5.42	-694.37	132.32	-372.71	48.34
29Y	-3.00	1001.51	8.40	565.44	286.97	348.08	65.62
30P	-1.96	47.58	-4.48	59.14	25.02	17.79	3.42
30X	-1.96	47.58	4.48	65.82	38.53	18.89	7.17
30XY	2.45	47.18	-2.96	64.12	-36.53	18.54	-6.58
30Y	2.45	47.18	2.96	-720.70	-27.37	17.63	-4.07
31P	-1.99	-59.14	-25.02	-720.70	62.45	-173.36	8.32
31X	-1.94	-65.82	-38.53	624.87	14.56	124.19	-5.32
31XY	2.43	-64.12	36.54	629.00	-24.33	125.49	2.71
31Y	2.47	-58.59	27.37	-721.73	-50.54	-173.47	-5.15
32P	-2.23	720.69	-62.45	423.65	-401.33	254.32	-103.07
32X	-1.80	-624.87	-14.56	-382.77	-268.94	-223.92	-63.00
32XY	2.27	-629.00	24.34	-386.77	306.01	-225.73	73.41
32Y	2.69	721.73	50.54	424.01	356.55	254.63	90.47
33P	21.69	-103.94	-20.10	1189.56	1093.37	206.79	204.43
33X	21.70	-103.94	20.10	-849.75	-561.94	-181.66	-103.21
33XY	-18.13	-101.44	-19.70	-838.33	560.97	-179.01	103.10
33Y	-18.11	-101.44	19.70	1201.39	-1095.10	209.52	-204.84
34P	21.54	-1189.57	-1093.37	-3836.41	-2095.81	-957.21	-607.37
34X	21.60	849.75	561.94	3943.48	1299.52	913.12	354.56
34XY	-18.02	838.33	-560.98	-3842.66	-1305.36	910.79	-355.53
34Y	-17.97	-1201.40	1095.10	3854.89	2100.45	-962.98	608.59
35P	-6.90	3836.47	2095.80	611.46	307.51	836.88	452.18
35X	-7.58	-3943.54	-1299.31	-900.06	-624.41	-911.37	-361.97
35XY	11.13	-3942.68	1305.35	-905.67	657.23	-312.27	369.28
35Y	10.60	3854.92	-2100.44	612.33	-348.62	840.51	-460.79
36P	-23.77	18.52	43.46	3.61	44.89	4.22	16.83
36X	-23.77	18.52	-43.46	253.48	-23.52	51.80	-12.75
36XY	24.94	18.79	42.60	254.35	24.43	52.02	12.76
36Y	24.94	18.79	-42.59	5.33	-45.50	4.59	-16.78
37P	-23.77	-3.61	-44.89	-509.75	-77.07	-77.15	-23.24
37X	-23.77	-233.48	23.51	623.31	-77.15	70.44	-10.21
37XY	24.94	-234.35	-24.42	635.52	80.11	72.60	10.60
37Y	24.95	-5.33	45.50	-508.77	77.22	-97.93	23.38

Clamp Label	Input Holding Capacity (kips)	Factored Holding Capacity (kips)	Usage %
38P	-27.26	509.57	77.08
38X	-28.04	-623.13	77.14
38XY	28.30	-635.34	-80.09
38Y	28.43	508.58	-77.24
39P	0.00	11.62	-19.14
39X	-0.00	344.47	12.51
39XY	0.00	345.96	7.10
39Y	0.00	9.49	-5.73
40P	0.00	-124.82	-65.45
40X	-0.00	592.95	-20.22
40XY	0.00	596.82	42.86
40Y	0.00	-121.60	37.60
41P	0.00	100.50	-229.36
41X	-0.00	383.75	-182.68
41XY	0.00	387.65	204.59
41Y	-0.00	100.57	204.36
53P	-0.19	5.61	-4.44
53X	-0.19	5.61	4.44
53XY	0.27	5.84	-4.34
53Y	0.27	5.84	4.34
98P	0.02	-13.94	11.16
98X	0.01	13.63	-20.29
98XY	0.01	13.63	20.29
98Y	0.02	-13.94	-11.16
99P	-0.08	-6.14	-9.00
99X	0.08	9.59	3.34
100P	0.08	2.95	-9.02
100X	-0.11	4.55	2.49

Summary of Clamp Capacities and Usages for Load Case "NESC Heavy":

Clamp Label	Input Holding Capacity (kips)	Factored Holding Capacity (kips)	Usage %
C1	6.001	50.00	12.00
C2	4.136	50.00	8.27
C3	3.714	50.00	7.43
C4	3.714	50.00	7.43
C5	3.714	50.00	7.43
C6	3.714	50.00	7.43
C7	3.714	50.00	7.43
C8	3.714	50.00	7.43
C9	3.714	50.00	7.43
C10	3.714	50.00	7.43
C11	3.717	50.00	7.43
C12	3.717	50.00	7.43
C13	3.717	50.00	7.43
C14	3.717	50.00	7.43
C15	3.731	50.00	7.46
C16	3.731	50.00	7.46
C17	3.731	50.00	7.46
C18	3.731	50.00	7.46
C19	3.739	50.00	7.48
C20	3.739	50.00	7.48
C21	3.739	50.00	7.48
C22	3.739	50.00	7.48
C23	3.745	50.00	7.49
C24	3.745	50.00	7.49
C25	3.745	50.00	7.49
C26	3.745	50.00	7.49
C27	4.007	50.00	8.01
C28	0.693	50.00	1.39
C29	1.342	50.00	2.68
C30	0.930	50.00	1.86
C31	1.098	50.00	2.20

C32	1.997	50.00	50.00	3.99
C33	1.250	50.00	50.00	2.50
C34	4.303	50.00	50.00	8.61
C35	0.726	50.00	50.00	1.45
C36	1.347	50.00	50.00	2.69
C37	0.930	50.00	50.00	1.86
C38	1.098	50.00	50.00	2.20
C39	1.997	50.00	50.00	3.99
C40	1.250	50.00	50.00	2.50
C41	3.642	50.00	50.00	7.28
C42	3.937	50.00	50.00	7.87
C43	1.019	50.00	50.00	2.04
C44	1.033	50.00	50.00	2.07

*** Analysis Results for Load Case No. 2 "NESC Extreme" - Number of iterations in SAPS 10

Equilibrium Joint Positions and Rotations for Load Case "NESC Extreme":

Joint Label	X-Displ (ft)	Y-Displ (ft)	Z-Displ (ft)	X-Rot (deg)	Y-Rot (deg)	Z-Rot (deg)	X-Pos (ft)	Y-Pos (ft)	Z-Pos (ft)
1P	0.000449	0.1198	-0.01504	0.0000	0.0000	0.0000	0.000449	14.2 93.98	14.2 93.98
2P	0.0009214	0.1678	-0.01613	0.0818	0.0081	-0.0148	3.501	15.17 84.98	15.17 84.98
3P	0.0004815	0.1603	-0.01638	-0.1223	-0.0020	-0.0092	3.5	15.16 79.98	15.16 79.98
4P	0.001022	0.1443	-0.01652	-0.2360	-0.0038	-0.0129	3.501	15.14 74.98	15.14 74.98
5P	0.0008174	0.1245	-0.01535	-0.1619	-0.0060	-0.0167	3.501	15.12 69.98	15.12 69.98
6P	0.0005386	0.1146	-0.01509	-0.1921	-0.0040	-0.0175	3.501	15.11 64.98	15.11 64.98
7P	0.0009317	0.09486	-0.01492	-0.2545	-0.0029	-0.0255	3.501	15.09 59.99	15.09 59.99
8P	0.0008239	0.07429	-0.0138	-0.1725	-0.0065	-0.0334	3.501	15.07 54.99	15.07 54.99
9P	0.0003745	0.0635	-0.0132	-0.1453	-0.0042	-0.0462	3.5	15.06 49.99	15.06 49.99
14P	0	0	0	0.0000	0.0000	0.0000	13.07	19.07 70.0	19.07 70.0
15P	0.001198	0.1605	-0.02788	-0.0800	-0.0020	-0.0042	3.501	22.16 79.97	22.16 79.97
16P	0.00103	0.1148	-0.03044	-0.0926	-0.0040	-0.0027	3.501	22.11 64.97	22.11 64.97
17P	0.0008329	0.06367	-0.03013	-0.1353	-0.0041	-0.0174	3.501	22.06 49.97	22.06 49.97
18P	-0.001713	0.1649	-0.003975	-0.0067	0.0002	-0.0064	3.498	0.1649 85	0.1649 85
19P	-0.001241	0.1165	-0.004004	0.0192	0.0034	-0.0036	3.499	6.165 85	6.165 85
20P	-0.000632	0.1665	-0.004954	-0.0999	0.0058	-0.0161	3.499	10.167 85	10.167 85
21P	-0.0003111	0.1617	-0.003956	0.0005	-0.0012	-0.0063	3.5	0.1617 80	0.1617 80
22P	0.0002705	0.1607	-0.004145	0.0024	-0.0015	-0.0044	3.5	6.161 80	6.161 80
23P	0.0004349	0.1597	-0.00607	-0.0868	-0.0017	0.0014	3.5	10.66 79.99	10.66 79.99
24P	-0.002996	0.1204	-0.004182	0.0181	0.0001	-0.0026	3.497	0.1204 70	0.1204 70
25P	-0.0027	0.1203	-0.001039	0.0526	0.0024	-0.0145	3.497	6.12 70	6.12 70
26P	-0.0008081	0.1229	-0.0004469	-0.1090	-0.0042	-0.0257	3.499	10.62 70	10.62 70
27P	-0.0001728	0.1181	-0.004164	0.0316	0.0006	-0.0067	3.5	0.1181 65	0.1181 65
28P	0.0004527	0.1162	-0.002174	0.0265	-0.0039	-0.0046	3.5	6.116 65	6.116 65
29P	0.0005312	0.1146	-0.002174	0.0516	-0.0029	0.0047	3.501	10.61 65	10.61 65
30P	-0.00305	0.06989	-0.003045	-0.0151	0.0008	-0.0014	3.497	0.06989 55	0.06989 55
31P	-0.002813	0.06988	-0.000102	0.0534	0.0031	-0.0153	3.497	6.07 55	6.07 55
32P	-0.0009215	0.07268	0.0008366	-0.1008	0.0049	-0.0226	3.499	10.57 55	10.57 55
33P	-3.361e-006	0.06759	-0.0003024	0.0281	-0.0010	-0.0083	3.5	0.06759 50	0.06759 50
34P	0.0005924	0.06551	-0.0002139	0.0285	-0.0022	-0.0011	3.501	6.066 50	6.066 50
35P	0.0001587	0.06374	-0.00108	-0.0946	-0.0031	0.0138	3.5	10.56 50	10.56 50
36P	0.0001641	0.03272	-0.00315	-0.0196	0.0003	-0.0032	5.375	0.03272 40	0.03272 40
37P	0.018e-005	0.03268	-0.00437	-0.0011	0.0014	0.0099	5.375	5.283 40	5.283 40
38P	-0.0009257	0.03339	-0.005239	-0.0459	0.0025	-0.0032	5.374	10.53 39.99	10.53 39.99
39P	-4.622e-006	0.02869	-0.003122	-0.0124	0.0010	-0.0016	6.333	0.02869 35	0.02869 35
40P	0.0001621	0.02831	-0.004359	-0.0153	-0.0014	-0.0013	6.333	5.278 35	5.278 35
41P	0.0003055	0.02793	-0.006356	-0.0392	-0.0038	-0.0033	6.333	10.53 34.99	10.53 34.99
44P	0.0003191	0.3765	0.02921	0.0000	0.0000	0.0000	0.0003191	18 17.78	18 17.78
45P	0.0003209	0.03555	-0.1291	0.0000	0.0000	0.0000	0.0003209	10.54 39.87	10.54 39.87
IX	-0.001837	0.1909	0.006044	0.0000	0.0000	0.0000	-0.001837	-13.81 94.01	-13.81 94.01
2X	-0.001574	0.167	0.007768	-0.0682	-0.0077	-0.0021	3.498	-14.83 85.01	-14.83 85.01
2Y	0.0004825	0.1683	0.007572	-0.0670	0.0047	0.0030	-3.501	15.17 84.98	15.17 84.98
3X	-0.001005	0.1604	-0.01612	-0.0819	-0.0081	-0.0032	-3.5	14.84 80.01	14.84 80.01
3Y	0.000116	0.1609	0.008227	-0.1138	-0.0004	-0.0027	3.499	-14.84 80.01	-14.84 80.01
3Z	0.0008956	0.1608	0.008041	-0.1126	-0.0029	-0.0005	-3.502	15.16 79.98	15.16 79.98
4X	-0.001368	0.1445	-0.01637	-0.1324	0.0024	-0.0044	3.499	-14.86 75.01	-14.86 75.01
4Y	-0.00106	0.1451	-0.008778	-0.2389	-0.0021	-0.0015	-3.501	14.85 75.01	14.85 75.01
4Z	0.0003144	0.1447	0.008607	-0.2395	-0.0054	0.0035	-3.5	15.14 74.98	15.14 74.98
5X	-0.001174	0.1246	-0.01651	-0.2366	0.0044	-0.0051	3.499	-14.88 70.01	-14.88 70.01
5Y	0.0004802	0.1249	0.008054	-0.1595	-0.0059	-0.0002	-3.501	14.87 70.01	14.87 70.01
6X	-0.0007888	0.1148	-0.01534	-0.1608	0.0031	0.0074	3.499	-14.87 70.01	-14.87 70.01
6Y	0.0001115	0.1152	0.008291	-0.2030	-0.0026	-0.0057	-3.5	15.12 69.98	15.12 69.98
6Z	-0.0007138	0.115	-0.008129	-0.2032	-0.0057	0.0094	3.499	-14.89 65.01	-14.89 65.01
7X	-0.00104	0.09409	-0.01508	-0.1913	0.0047	0.0054	-3.501	14.88 65.01	14.88 65.01
7Y	-0.0005936	0.09447	0.008442	-0.2566	0.0012	-0.0149	3.499	15.22 64.98	15.22 64.98
7Z	0.000254	0.09551	0.008287	-0.2574	-0.0043	0.0169	3.499	-14.91 60.01	-14.91 60.01
8X	-0.0008495	0.07418	-0.01491	-0.2553	0.0037	0.0124	-3.5	15.1 59.99	15.1 59.99
8Y	-0.0005283	0.07448	0.007568	-0.1618	-0.0053	-0.0206	3.499	-14.93 55.01	-14.93 55.01
8Z	-0.0005283	0.07448	0.007568	-0.1618	-0.0053	-0.0206	-3.501	14.93 55.01	14.93 55.01

8Y	0.0002981	0.07461	-0.001379	-0.1734	-0.0059	0.0194	-3.5	15.07	54.99
9X	-0.0004841	0.06395	0.007468	-0.1462	0.0017	-0.0365	3.5	-14.94	50.01
9XY	-0.0006554	0.06427	0.007348	-0.1464	-0.0039	0.0365	-3.501	-14.94	50.01
9Y	0.0006797	0.0638	-0.001319	-0.1461	0.0051	0.0379	-3.499	15.06	49.99
14X	0	0	0	0.0000	0.0000	0.0000	13.07	-19.07	0
14XY	0	0	0	0.0000	0.0000	0.0000	-13.07	19.07	0
14Y	0	0	0	0.0000	0.0000	0.0000	-13.07	19.07	0
15X	-0.001877	0.1608	0.01509	-0.0275	-0.0004	-0.0081	3.498	-21.84	80.02
15XY	-0.001915	0.1614	-0.01468	-0.0254	-0.0029	-0.0036	-3.502	21.84	80.01
15Y	0.001204	0.161	-0.02789	-0.0797	0.0024	-0.0016	-3.499	22.16	79.97
16X	-0.001327	0.1152	0.01992	-0.0415	0.0026	-0.0020	3.499	-21.88	65.02
16XY	-0.001378	0.1156	-0.01984	-0.0425	-0.0038	-0.0079	-3.501	21.88	65.02
16Y	0.001056	0.1152	-0.03044	-0.0931	0.0048	-0.0069	3.499	-21.88	65.02
17X	-0.0008609	0.06643	0.02015	-0.0827	0.0018	0.0066	-3.501	21.94	50.02
17XY	-0.0009091	0.06462	-0.01998	-0.0820	-0.0040	-0.0213	3.501	-21.94	50.02
17Y	0.000836	0.06398	-0.03014	-0.1350	0.0050	-0.0208	-3.499	22.06	49.97
18X	-0.001706	0.1653	-0.003873	-0.0964	-0.0018	-0.0029	3.502	-0.1653	85
18XY	-0.001706	0.1653	-0.003873	-0.0964	-0.0018	-0.0029	3.498	-5.835	85
18Y	0.001638	0.1659	-0.004045	0.0096	0.0008	-0.0022	-3.502	-5.835	85
19X	-0.002161	0.1651	-0.00389	0.0206	-0.0044	-0.0129	3.501	6.15	85
19XY	-0.002161	0.1651	-0.00389	0.0206	-0.0044	-0.0129	3.498	-10.33	85
19Y	-0.00123	0.1854	-0.002191	-0.0964	0.0027	0.0059	-3.502	-10.33	85
20X	-0.001638	0.1659	-0.004045	0.0096	0.0008	-0.0022	3.5	10.67	85
20XY	-0.001638	0.1659	-0.004045	0.0096	0.0008	-0.0022	-3.5	10.67	85
20Y	6.712e-005	0.167	-0.002186	-0.0979	-0.0053	0.0055	3.499	-5.839	80
21X	-0.0003088	0.1622	-0.004754	-0.1013	-0.0062	-0.0123	-3.501	5.839	80
21XY	-0.0003088	0.1622	-0.004754	-0.1013	-0.0062	-0.0123	3.5	6.161	80
21Y	-0.0009012	0.1607	-0.004226	-0.0020	-0.0009	-0.0041	-3.501	-10.34	80
22X	-0.0005197	0.1612	-0.004205	-0.0010	-0.0013	-0.0033	3.499	-5.839	80
22XY	-0.0005197	0.1612	-0.004205	-0.0010	-0.0013	-0.0033	-3.501	5.839	80
22Y	-0.0001054	0.1612	-0.001424	-0.0885	-0.0006	-0.0035	3.499	-6.161	80
23X	-0.001073	0.1596	-0.001556	-0.0899	-0.0006	-0.0003	-3.501	10.34	80
23XY	-0.001073	0.1596	-0.001556	-0.0899	-0.0006	-0.0003	3.499	-10.34	80
23Y	0.0003233	0.1602	-0.00395	-0.0876	0.0016	-0.0076	-3.5	10.66	79.99
24X	-0.002997	0.1206	-0.00433	-0.0185	-0.0014	-0.0093	3.503	-5.88	69.99
24XY	-0.002997	0.1206	-0.00433	-0.0185	-0.0014	-0.0093	-3.503	5.88	69.99
24Y	0.003267	0.1204	-0.007056	0.0479	-0.0023	0.0088	3.497	-5.879	69.99
25X	-0.003265	0.1208	-0.007243	0.0486	-0.0004	0.0088	-3.503	6.121	70
25XY	-0.003265	0.1208	-0.007243	0.0486	-0.0004	0.0088	3.498	-10.38	69.99
25Y	0.002693	0.1207	-0.01114	0.0534	-0.0003	-0.0149	-3.502	10.38	69.99
26X	-0.001893	0.123	-0.007419	-0.1162	-0.0041	0.0178	3.501	-10.62	70
26XY	-0.001893	0.123	-0.007419	-0.1162	-0.0041	0.0178	-3.501	10.62	70
26Y	-0.0007906	0.1233	-0.004674	-0.1085	-0.0007	-0.0009	-3.5	0.1185	65
27X	-0.0001708	0.1185	-0.004311	0.0321	-0.0007	0.0014	3.499	-5.884	64.99
27XY	-0.0001708	0.1185	-0.004311	0.0321	-0.0007	0.0014	-3.5	5.884	64.99
27Y	-0.0007941	0.1162	-0.007232	0.0209	0.0007	-0.0019	3.5	-6.117	65
28X	-0.000166	0.1166	-0.007419	0.0214	-0.0027	-0.0044	-3.5	6.117	65
28XY	-0.000166	0.1166	-0.007419	0.0214	-0.0027	-0.0044	3.499	-10.39	64.99
28Y	-0.0001745	0.1166	-0.005587	-0.1030	-0.0043	-0.0110	-3.501	10.39	64.99
29X	-0.0008712	0.1146	-0.005377	-0.1027	0.0017	0.0033	3.499	-10.39	64.99
29XY	-0.0008712	0.1146	-0.005377	-0.1027	0.0017	0.0033	-3.5	10.61	65
29Y	0.0005662	0.115	-0.005587	-0.1030	-0.0043	-0.0110	3.503	0.7017	55
30X	-0.000304	0.1115	-0.002194	-0.0911	0.0030	-0.0093	-3.503	0.7017	55
30XY	-0.000304	0.1115	-0.002194	-0.0911	0.0030	-0.0093	3.497	-5.93	54.99
30Y	-0.00323	0.0699	-0.003087	0.0154	-0.0020	-0.0025	-3.503	5.93	54.99
31X	-0.003217	0.07017	-0.005851	0.0513	-0.0015	0.0090	3.497	-5.93	54.99
31XY	-0.003217	0.07017	-0.005851	0.0513	-0.0015	0.0090	-3.5	6.07	55
31Y	-0.002804	0.07016	-8.378e-005	0.0525	-0.0002	0.0114	3.503	-5.93	54.99
32X	-0.001664	0.07259	-0.006649	-0.1018	-0.0033	0.0255	3.498	-10.43	54.99
32XY	-0.001664	0.07259	-0.006649	-0.1018	-0.0033	0.0255	-3.502	10.43	54.99
32Y	-0.0008678	0.07298	-0.006833	-0.1017	0.0010	0.0167	3.501	-10.57	55
33X	-3.599e-005	0.06789	-0.009243	-0.1009	-0.0049	-0.0310	-3.5	0.06789	50
33XY	-3.599e-005	0.06789	-0.009243	-0.1009	-0.0049	-0.0310	3.499	-5.934	49.99
33Y	-0.0006115	0.06586	-0.003066	0.0286	0.0003	0.0042	-3.5	6.066	50
34X	-0.0001457	0.06595	-0.006039	0.0259	0.0002	-0.0002	3.499	-5.934	49.99
34XY	-0.0001457	0.06595	-0.006039	0.0259	0.0002	-0.0002	-3.5	5.934	49.99
34Y	-0.0002063	0.06588	-0.006149	0.0268	-0.0015	-0.0036	3.5	-10.44	50
35X	-0.000186	0.06401	-0.0001957	0.0293	0.0021	-0.0034	-3.5	6.066	50
35XY	-0.000186	0.06401	-0.0001957	0.0293	0.0021	-0.0034	3.499	-10.44	50
35Y	-0.0005567	0.06404	-0.004871	-0.0988	-0.0028	-0.0157	-3.501	10.44	50
36X	-0.0001057	0.03303	-0.001021	-0.0948	0.0035	-0.0170	3.499	-10.56	50
36XY	-0.0001057	0.03303	-0.001021	-0.0948	0.0035	-0.0170	-3.502	10.56	50
36Y	-0.0002339	0.03273	-0.003222	-0.1132	-0.0007	0.0001	5.375	-0.03303	40
37X	7.174e-006	0.03305	-0.001757	-0.0050	-0.0008	-0.0066	-3.5	5.217	40
37XY	7.174e-006	0.03305	-0.001757	-0.0050	-0.0008	-0.0066	3.501	-5.217	40
37Y	-0.0002862	0.033	-0.004401	-0.006	-0.0014	-0.0034	-3.501	10.44	50
38X	-0.0007728	0.03344	-0.0003258	-0.0542	-0.0019	-0.0009	5.375	-5.217	40
38XY	-0.0007728	0.03377	-0.0004628	-0.0542	-0.0019	-0.0009	-5.375	5.217	40
38Y	0.001569	0.03371	-0.0004628	-0.0542	-0.0019	-0.0009	5.375	-10.47	40
39Y	7.637e-005	0.02907	-0.005234	-0.0458	-0.0021	-0.0021	-5.375	10.47	40
40X	-0.0001089	0.02809	-0.003196	-0.0120	-0.0011	-0.0014	5.375	-0.02907	35
40XY	-0.0001089	0.02809	-0.003196	-0.0120	-0.0011	-0.0014	-6.333	0.02907	35
40Y	-9.408e-005	0.02845	-0.001773	-0.0198	0.0034	-0.0011	6.333	-5.222	35
40Y	0.000187	0.02886	-0.00189	-0.0193	-0.0038	-0.0019	-6.333	5.222	35
40Y	0.000187	0.02886	-0.00439	-0.0148	0.0016	-0.0017	-6.333	5.279	35

Label	X (kips)	Y (kips)	Z (kips)	Comp. Usage %	Uplift Usage %	Result. Force (kips)	Result. Usage %	X-M. Moment (ft-k)	X-M. Usage %	Y-M. Moment (ft-k)	Y-M. Usage %	Z-M. Moment (ft-k)	Z-M. Usage %
41X	-0.0003138	0.02747	0.001222	-0.0509	0.0058	-0.0043	6.333	-10.47	35				
41Y	-0.0001574	0.02783	0.001077	-0.0510	-0.0066	0.0015	-6.333	-10.47	35				
41Z	-0.0003146	0.0283	-0.006552	-0.0391	0.0043	0.0004	-6.333	-10.47	35				
44X	-0.0001869	0.214	-0.01381	0.0000	0.0000	0.0000	-0.0001869	-17.91	17.74				
44Y	-0.0002625	0.3273	-0.08953	0.0000	0.0000	0.0000	-0.0002625	-10.47	39.91				
10S	0.001405	0.04635	-0.0137	-0.1819	-0.0007	-0.0463	4.459	15.45	44.99				
11S	0.0006396	0.03356	-0.0132	-0.0981	-0.0027	-0.0234	5.415	15.85	39.99				
12S	-0.001019	0.02715	-0.01197	-0.0607	-0.0067	-0.0116	6.373	16.25	34.99				
13S	-1.5346	-0.05	0.01264	-0.008874	-0.0629	0.0023	-0.0108	8.541	17.16	23.66			
42S	0.0001527	0.01264	-0.0005972	-0.0050	0.0032	-0.0005	8.541	0.01208	23.67				
43S	0.0004754	0.03454	-0.01324	-0.0983	-0.0003	-0.0292	4.456	-15.36	45.01				
10X	-0.001118	0.04639	0.008531	-0.1883	-0.0008	-0.0292	-4.456	-15.36	45.01				
10Y	0.0001378	0.04667	0.008413	-0.1886	-0.0009	0.0278	4.458	15.45	44.99				
10Z	-0.0003395	0.04663	-0.0137	-0.1831	0.0017	0.0403	-5.415	-15.78	40.01				
11X	-0.0004834	0.03382	0.008409	-0.1066	-0.0021	0.0016	5.414	15.85	39.99				
11Y	-0.0003599	0.03389	0.008291	-0.1068	-0.0006	-0.0046	-5.415	-15.78	40.01				
12X	-0.0002233	0.03389	-0.01314	-0.0984	-0.0019	0.0195	-5.414	-15.85	39.99				
12Y	-2.5686	-0.05	0.02685	0.007712	-0.0709	-0.0087	-0.0005	-6.372	-16.2	35.01			
13X	-0.001583	0.01243	-0.01198	-0.0607	-0.0076	-0.0083	6.371	-16.2	35.01				
13Y	0.001064	0.01308	0.005367	-0.0599	0.0040	-0.0031	-8.54	-17.13	23.68				
42Y	0.0007399	0.01328	-0.005249	-0.0597	-0.0055	-0.0009	-8.54	-17.13	23.68				
42Z	-3.6886	-0.05	0.01244	-0.008865	-0.0629	-0.0007	-0.0085	-8.54	17.16	23.66			
43X	-0.0004216	0.03345	-0.0006311	-0.0047	-0.0031	-0.0015	-8.541	0.01244	23.67				
43Y	-0.0004216	0.03345	0.0008491	-0.1067	-0.0006	-0.0019	-8.541	0.01244	23.67				
43Z	-0.0004216	0.03345	-0.0008491	-0.1067	-0.0006	-0.0019	-8.541	0.01244	23.67				

Joint Support Reactions for Load Case "NESC Extreme":

Joint Label	X (kips)	Y (kips)	Z (kips)	Comp. Usage %	Uplift Usage %	Result. Force (kips)	Result. Usage %	X-M. Moment (ft-k)	X-M. Usage %	Y-M. Moment (ft-k)	Y-M. Usage %	Z-M. Moment (ft-k)	Z-M. Usage %
14P	-21.67	0.0	-34.55	0.0	120.03	0.0	0.0	126.77	0.0	0.29	0.0	0.2	0.0
14X	20.45	0.0	-29.66	0.0	-92.79	0.0	0.0	99.54	0.0	0.36	0.0	0.1	0.0
14Y	-20.16	0.0	-30.25	0.0	-91.97	0.0	0.0	98.89	0.0	0.44	0.0	-0.1	0.0
14Z	21.37	0.0	-35.25	0.0	119.71	0.0	0.0	126.61	0.0	0.36	0.0	-0.3	0.0

Joint Displacements, Loads and Member Forces on Joints for Load Case "NESC Extreme":

Joint Label	X External Load (kips)	Y External Load (kips)	Z External Load (kips)	X Member Force (kips)	Y Member Force (kips)	Z Member Force (kips)	X Disp. (ft)	Y Disp. (ft)	Z Disp. (ft)
1P	0.0000	5.1444	-0.4944	-0.0000	-5.1444	0.4944	0.0004	0.1998	-0.0150
2P	0.0000	0.2315	-0.1091	-0.0000	-0.2315	0.1091	0.0009	0.1678	-0.0161
3P	0.0000	4.3484	-1.8857	-0.0000	-4.3484	1.8857	0.0005	0.1603	-0.0164
4P	0.0000	0.2616	-0.1447	-0.0000	-0.2616	0.1447	0.0010	0.1443	-0.0165
5P	0.0000	0.2914	-0.1553	-0.0000	-0.2914	0.1553	0.0008	0.1245	-0.0153
6P	0.0000	0.3356	-0.2293	-0.0000	-0.3356	0.2293	0.0005	0.1146	-0.0151
7P	0.0000	-1.2325	-0.5678	-0.0000	1.2325	-0.5678	0.0009	0.0949	-0.0149
8P	0.0000	0.3735	-0.2624	-0.0000	-0.3735	0.2624	0.0008	0.0743	-0.0138
9P	0.0000	0.3882	-0.2944	-0.0000	-0.3882	0.2944	0.0004	0.0635	-0.0132
14P	0.0000	0.7557	-0.6944	21.6702	33.7980	-119.3383	0.0000	0.0000	0.0000
15P	0.0000	2.8461	-0.6361	-0.0000	-2.8461	0.6361	0.0012	0.1605	-0.0279
16P	0.0000	2.8461	-0.6420	-0.0000	-2.8461	0.6420	0.0008	0.1148	-0.0304
17P	0.0000	0.0883	-0.0611	-0.0000	-0.0883	0.0611	-0.0017	0.1637	-0.0301
18P	0.0000	0.1521	-0.0841	-0.0000	-0.1521	0.0841	-0.0012	0.1650	-0.0040
19P	0.0000	0.1396	-0.0685	-0.0000	-0.1396	0.0685	-0.0006	0.1665	-0.0050
20P	0.0000	0.1744	-0.1003	-0.0000	-0.1744	0.1003	-0.0003	0.1617	-0.0040
21P	0.0000	2.8610	-0.6457	0.0000	-2.8610	0.6457	0.0003	0.1607	-0.0041
22P	0.0000	0.2137	-0.1249	-0.0000	-0.2137	0.1249	0.0003	0.1597	-0.0061
23P	0.0000	0.1680	-0.0718	-0.0000	-0.1680	0.0718	-0.0030	0.1204	-0.0042
24P	0.0000	0.1111	-0.0000	-0.0000	-0.1111	0.0000	-0.0027	0.1203	-0.0010
25P	0.0000	0.1308	-0.0869	-0.0000	-0.1308	0.0869	-0.0008	0.1229	-0.0004
26P	0.0000	0.1957	-0.1314	-0.0000	-0.1957	0.1314	-0.0002	0.1181	-0.0042
27P	0.0000	2.8610	-0.6551	-0.0000	-2.8610	0.6551	0.0005	0.1162	-0.0012
28P	0.0000	0.2509	-0.1493	-0.0000	-0.2509	0.1493	0.0005	0.1146	-0.0022
29P	0.0000	0.2509	-0.1493	-0.0000	-0.2509	0.1493	0.0005	0.1146	-0.0022

30P	0.0000	0.0883	-0.0819	-0.0000	-0.0883	0.0819	-0.0031	0.0699	-0.0030
31P	0.0000	0.1733	-0.1309	-0.0000	-0.1733	0.1309	-0.0028	0.0699	-0.0030
32P	0.0000	0.1467	-0.0997	0.0000	-0.1467	0.0997	-0.0009	0.0727	-0.0008
33P	0.0000	0.1957	-0.1579	0.0000	-0.1957	0.1579	-0.0000	0.0676	-0.0030
34P	0.0000	2.8610	-0.8639	0.0000	-2.8610	0.8639	-0.0006	0.0655	-0.0002
35P	0.0000	0.2624	-0.1874	-0.0000	-0.2624	0.1874	-0.0002	0.0637	-0.0011
36P	0.0000	0.1931	-0.2233	0.0000	-0.1931	0.2233	-0.0001	0.0327	-0.0031
37P	0.0000	0.1540	-0.2411	0.0000	-0.1540	0.2411	-0.0001	0.0327	-0.0031
38P	0.0000	0.2717	-0.3140	-0.0000	-0.2717	0.3140	-0.0009	0.0334	-0.0044
39P	0.0000	0.2968	-0.2566	-0.0000	-0.2968	0.2566	-0.0000	0.0287	-0.0031
40P	0.0000	0.0755	-0.1308	-0.0000	-0.0755	0.1308	-0.0002	0.0283	-0.0044
41P	0.0000	0.3515	-0.3050	-0.0000	-0.3515	0.3050	-0.0003	0.0279	-0.0066
44P	0.0000	0.4139	-0.1308	0.0000	-0.4139	0.1308	-0.0003	0.0375	-0.0066
45P	0.0000	0.1262	-0.0620	0.0000	-0.1262	0.0620	-0.0003	0.0355	-0.0292
1X	0.0000	2.4754	-0.4034	-0.0000	-2.4754	0.4034	-0.0018	0.0355	-0.1291
2X	0.0000	0.2687	-0.1225	-0.0000	-0.2687	0.1225	-0.0016	0.1909	0.0060
2Y	0.0000	0.2315	-0.1091	-0.0000	-0.2315	0.1091	-0.0014	0.1674	0.0078
3X	0.0000	3.8479	-1.7797	-0.0000	-3.8479	1.7797	-0.0011	0.1683	-0.0161
3Y	0.0000	4.2059	-1.8587	-0.0000	-4.2059	1.8587	-0.0016	0.1604	0.0082
4X	0.0000	0.2616	-1.9727	-0.0000	-0.2616	1.9727	-0.0009	0.1608	-0.0080
4Y	0.0000	0.2616	-0.1447	-0.0000	-0.2616	0.1447	-0.0014	0.1445	0.0088
5X	0.0000	0.3286	-0.1687	-0.0000	-0.3286	0.1687	-0.0003	0.1447	-0.0365
5Y	0.0000	0.6494	-0.2343	-0.0000	-0.6494	0.2343	-0.0010	0.1246	0.0081
5Z	0.0000	0.6866	-0.2557	-0.0000	-0.6866	0.2557	-0.0005	0.1249	0.0079
6X	0.0000	0.3356	-0.2293	-0.0000	-0.3356	0.2293	-0.0008	0.1148	0.0083
6Y	0.0000	0.3356	-0.2293	-0.0000	-0.3356	0.2293	-0.0011	0.1152	0.0081
7X	0.0000	-1.0205	-0.5678	-0.0000	1.0205	0.5678	-0.0010	0.1150	-0.0151
7Y	0.0000	-0.6625	-0.6468	-0.0000	0.6625	0.6468	-0.0006	0.0941	0.0084
8X	0.0000	0.8745	-0.6548	-0.0000	-0.8745	0.6548	-0.0003	0.0953	0.0083
8Y	0.0000	0.4107	-0.2758	-0.0000	-0.4107	0.2758	-0.0008	0.0742	-0.0149
9X	0.0000	0.3735	-0.2758	-0.0000	-0.3735	0.2758	-0.0005	0.0742	0.0077
9Y	0.0000	0.7462	-0.2944	-0.0000	-0.7462	0.2944	-0.0003	0.0746	-0.0076
14X	0.0000	0.7557	-0.3814	-0.0000	-0.7557	0.3814	-0.0007	0.0640	-0.0138
14Y	0.0000	2.8461	-0.6944	-0.0000	-2.8461	0.6944	-0.0007	0.0638	0.0073
15X	0.0000	0.7557	-0.6944	-0.0000	-0.7557	0.6944	-0.0000	0.0000	-0.0132
15Y	0.0000	2.8461	-0.6361	-0.0000	-2.8461	0.6361	-0.0019	0.0000	0.0000
16X	0.0000	2.8461	-0.6361	-0.0000	-2.8461	0.6361	-0.0019	0.1608	0.0151
16Y	0.0000	2.8461	-0.6361	-0.0000	-2.8461	0.6361	-0.0012	0.1610	0.0147
17X	0.0000	2.8461	-0.6361	-0.0000	-2.8461	0.6361	-0.0013	0.1152	-0.0279
17Y	0.0000	2.8461	-0.6420	-0.0000	-2.8461	0.6420	-0.0014	0.1155	0.0199
17Z	0.0000	2.8461	-0.6420	-0.0000	-2.8461	0.6420	-0.0011	0.1152	0.0198
18X	0.0000	2.8461	-0.6420	-0.0000	-2.8461	0.6420	-0.0009	0.0643	0.0201
18Y	0.0000	0.0883	-0.0611	-0.0000	-0.0883	0.0611	-0.0009	0.0646	0.0200
19X	0.0000	0.1521	-0.0856	-0.0000	-0.1521	0.0856	-0.0017	0.0640	-0.0301
19Y	0.0000	0.1521	-0.0841	-0.0000	-0.1521	0.0841	-0.0022	0.1653	-0.0039
20X	0.0000	0.1396	-0.0856	-0.0000	-0.1396	0.0856	-0.0022	0.1651	-0.0041
20Y	0.0000	0.1396	-0.0685	-0.0000	-0.1396	0.0685	-0.0016	0.1659	-0.0039
20Z	0.0000	0.1396	-0.0685	-0.0000	-0.1396	0.0685	-0.0020	0.1659	-0.0022
21X	0.0000	0.1744	-0.1003	-0.0000	-0.1744	0.1003	-0.0001	0.1663	-0.0022
22X	0.0000	2.8610	-0.6457	-0.0000	-2.8610	0.6457	-0.0003	0.1670	-0.0048
22Y	0.0000	2.8610	-0.6457	-0.0000	-2.8610	0.6457	-0.0009	0.1622	-0.0039
23X	0.0000	2.8610	-0.6457	-0.0000	-2.8610	0.6457	-0.0005	0.1612	-0.0042
23Y	0.0000	0.2137	-0.1249	-0.0000	-0.2137	0.1249	-0.0001	0.1612	-0.0042
23Z	0.0000	0.2137	-0.1249	-0.0000	-0.2137	0.1249	-0.0011	0.1596	-0.0016
24X	0.0000	0.0883	-0.1249	-0.0000	-0.0883	0.1249	-0.0003	0.1602	-0.0016
24Y	0.0000	0.0883	-0.0718	-0.0000	-0.0883	0.0718	-0.0003	0.1602	-0.0060
25X	0.0000	0.1680	-0.1125	-0.0000	-0.1680	0.1125	-0.0033	0.1208	-0.0071
25Y	0.0000	0.1680	-0.1111	-0.0000	-0.1680	0.1111	-0.0033	0.1208	-0.0072
25Z	0.0000	0.1680	-0.1125	-0.0000	-0.1680	0.1125	-0.0027	0.1207	-0.0011

2XY	16.64	275.00	1.45	837.36	94.16	222.49	19.11
2X	5.54	325.86	-1.45	838.76	-131.00	232.91	-26.49
3P	17.89	-823.25	-127.67	581.47	-105.96	-48.35	-46.73
3X	-5.69	-984.05	92.36	560.99	61.68	-84.62	30.81
3XY	-18.93	-895.73	-94.76	572.85	-63.33	-84.58	-31.61
3Y	3.34	-849.43	131.59	548.45	106.65	-60.19	47.65
4P	17.89	-581.47	105.97	1496.77	-15.04	-43.74	18.21
4X	-5.69	-560.99	-61.68	1541.88	37.17	-420.51	-4.91
4XY	-18.93	-572.85	63.33	1546.11	-41.16	-423.73	4.41
4Y	3.33	-548.45	-106.65	1475.62	19.24	-404.91	-17.48
5P	3.94	2128.56	18.16	2501.05	142.44	925.97	32.11
5X	42.44	2225.24	-40.35	2762.44	-145.90	997.58	-37.54
5XY	-9.25	2223.37	43.73	2753.26	152.52	996.57	39.27
5Y	-52.91	2107.98	-21.74	2475.27	-151.38	916.70	-34.53
6P	207.06	-2725.68	-144.13	1525.30	-217.05	-240.09	-72.28
6X	149.48	-3195.10	147.86	455.79	245.94	-547.87	78.75
6XY	-196.57	-3177.99	-155.51	512.43	-257.23	-533.12	-82.54
6Y	-183.57	-2692.41	154.05	1667.55	220.50	-204.98	74.95
7P	207.18	-1525.28	217.08	7108.75	-430.09	-1727.19	-42.41
7X	149.41	-445.80	-245.96	-6932.68	192.42	-477.46	-10.57
7XY	-196.48	-512.45	237.26	-7018.91	-191.92	-1506.04	12.88
7Y	-183.69	-1667.93	-220.54	-7245.58	434.77	-1783.02	42.68
8P	336.62	7477.00	433.33	5892.35	1163.86	2728.25	319.21
8X	416.79	7632.27	-196.68	6593.12	-671.66	284.90	-174.02
8Y	-318.27	7724.80	195.33	6675.14	624.23	2879.83	164.19
9P	-167.63	1077.08	582.35	6029.60	-1187.41	2784.21	-324.55
9X	-378.90	-1890.43	-6261.76	-637.81	3851.44	495.21	1971.28
9XY	416.38	-1963.79	-6263.84	-678.02	-3928.32	-517.88	-1995.56
9Y	109.49	1109.04	-5745.09	-66.43	3574.88	204.12	-1825.06
10P	-167.36	93.09	-3482.26	2069.12	1946.34	423.47	-300.80
10X	-379.00	638.17	3851.37	-1413.48	1507.78	-151.85	-458.85
10Y	416.44	678.43	3228.25	-1359.20	-1459.33	-133.35	483.39
11P	-134.66	66.53	3574.48	2053.63	-1887.88	415.25	330.33
11X	203.21	1735.05	-2177.87	141.81	-440.01	-509.83	-537.02
11XY	-209.40	1695.06	2127.82	115.94	322.51	367.41	-491.45
11Y	115.83	-2330.28	2555.67	-763.74	383.39	-606.01	575.67
12P	5.43	731.35	438.63	461.35	486.39	103.10	79.96
12X	56.29	-54.18	193.56	-53.90	521.33	-9.33	61.76
12XY	-63.22	-16.56	-113.05	-29.14	-440.75	-3.94	-47.84
12Y	3.30	703.13	-370.45	454.83	-405.68	100.10	-67.09
13P	5.72	-451.10	-467.54	-73.77	349.26	-21.72	-4.89
13X	46.02	46.72	-498.08	-231.52	292.48	-7.64	-8.50
13XY	-58.13	23.89	415.67	-233.31	-373.99	-8.66	1.72
13Y	-18.66	-448.44	384.27	-92.77	-434.35	-22.39	-2.07
15P	1.77	9.72	-4.26	47.48	-0.13	9.53	-0.73
15X	1.45	11.86	7.55	-13.53	17.69	-0.63	3.66
15Y	-1.45	11.86	-7.55	-11.45	8.45	0.07	2.63
16P	1.78	-47.48	0.13	-279.31	-21.96	10.51	-4.88
16X	1.78	13.53	-17.69	222.06	-12.36	52.37	-6.68
16XY	-1.44	11.45	-8.45	217.75	9.10	50.95	0.15
16Y	-1.43	-51.20	21.96	-288.20	23.21	-75.40	10.03
17P	1.77	279.31	24.12	314.61	26.61	131.94	11.27
17X	1.78	-222.06	12.36	-277.93	-2.51	-111.13	2.59
17XY	-1.44	-217.75	-9.10	-275.00	-16.63	-109.53	-5.72
17Y	-1.43	288.20	-23.21	325.85	-5.56	136.42	-6.39
18P	-0.18	12.72	-0.42	15.53	2.31	4.71	0.31
18X	-0.18	12.72	0.42	16.34	-3.63	4.84	0.67
18XY	0.59	13.62	0.27	16.29	-2.76	4.98	-0.41
18Y	0.59	13.62	-0.27	16.35	-3.53	5.00	-0.63
19P	-0.18	-15.53	-2.31	-189.12	8.92	-45.49	1.47
19X	-0.18	-16.34	3.63	154.68	3.77	30.73	0.03
19XY	0.59	-16.29	2.76	153.92	-8.91	30.58	-1.37
19Y	0.59	-16.35	3.53	-192.04	-4.44	46.32	-0.20
20P	-0.19	189.12	-8.92	120.11	-29.39	68.71	-8.51
20X	-0.18	-154.68	-3.77	-108.12	-8.45	-58.41	-2.72
20XY	0.58	-153.92	8.91	-107.08	26.12	-58.01	7.79

20Y	0.59	192.04	4.44	122.35	10.65	69.85	3.35
21P	3.15	-5.43	-39.51	117.13	-81.70	18.62	-20.20
21X	3.15	-5.43	39.51	-117.13	80.10	-19.48	19.94
21XY	-2.53	-6.86	39.72	-113.73	80.16	-20.10	19.98
21Y	-2.53	-6.86	-39.72	116.98	-83.41	18.35	-20.52
22P	3.23	-117.13	81.70	-882.24	28.55	-221.95	24.49
22X	3.23	111.45	-80.16	886.47	-37.33	222.33	-26.12
22XY	-2.46	113.73	80.16	-894.13	38.53	-224.10	26.36
22Y	-2.46	-116.98	83.41	-883.46	35.28	-222.19	26.36
23P	3.18	882.24	-28.56	631.79	13.99	336.33	-3.24
23X	3.23	-888.47	37.34	-683.35	-48.17	-349.42	-2.40
23XY	-2.50	-894.13	38.52	-683.26	-9.63	-350.65	6.42
23Y	-2.45	883.46	-35.27	632.56	56.19	336.73	4.65
24P	-1.81	13.05	-0.48	-5.08	7.25	1.33	1.13
24X	-1.81	13.05	0.48	-5.08	7.25	1.33	1.13
24XY	2.86	12.02	0.89	51.09	9.69	10.69	1.70
24Y	2.86	12.02	0.89	50.07	9.69	10.69	1.70
25P	-1.82	5.08	-0.89	-4.90	-10.94	10.35	-1.06
25X	-1.81	-51.09	-7.25	554.03	36.41	-122.03	6.48
25XY	2.86	50.07	7.70	-533.97	25.77	107.27	3.57
25Y	2.87	4.90	10.93	-555.95	-23.98	108.54	-6.83
26P	-1.90	54.03	-36.41	-78.16	-14.51	140.49	-39.54
26X	-1.76	-533.97	-25.77	58.85	-85.17	-131.74	-24.65
26XY	2.77	-538.71	38.02	-84.25	134.60	-134.00	24.65
26Y	2.92	555.95	-23.97	81.70	93.44	141.70	38.36
27P	3.77	-3.99	-48.32	161.90	-108.34	141.70	26.09
27XY	-2.91	-3.62	48.32	-160.83	93.38	-26.32	-26.11
27Y	-2.91	-3.62	48.30	-163.70	108.55	-27.47	23.62
28P	3.86	-161.90	108.34	165.27	108.55	-27.89	26.14
28X	3.86	160.83	-93.38	-1043.70	66.45	-269.43	-23.79
28XY	-2.82	163.70	-108.35	1052.45	-77.91	270.42	-20.36
28Y	-2.82	163.70	-108.35	1052.45	-77.91	270.42	-20.36
29P	3.66	1051.27	-66.46	638.24	-129.07	375.31	19.16
29X	4.04	-1043.70	-1.85	-693.59	-267.54	-387.53	-43.44
29XY	-3.00	-1052.45	77.90	-705.89	121.91	-390.88	-59.88
29Y	-2.61	1061.41	8.21	643.86	299.10	378.81	44.41
30P	-1.95	18.01	-2.48	19.77	28.71	6.30	4.37
30X	-1.95	18.01	-2.48	19.77	28.71	6.30	4.37
30XY	3.00	18.16	1.21	26.01	-35.29	7.60	6.61
30Y	3.00	18.16	1.21	26.01	-35.29	7.60	6.61
31P	-1.98	-19.77	28.71	-729.81	56.82	-166.84	6.25
31X	-1.93	-27.59	-37.20	690.87	23.50	147.34	-3.04
31XY	2.98	-27.59	35.29	-698.17	-34.44	149.31	0.19
31Y	2.98	-27.59	35.29	-698.17	-34.44	149.31	0.19
32P	-2.22	729.81	-56.82	437.99	-46.75	-168.28	-3.34
32X	-1.76	-690.88	23.50	-417.05	-293.17	-246.20	-102.13
32XY	2.78	-698.17	34.45	-423.88	335.79	-249.34	82.28
32Y	2.78	-698.17	34.45	-423.88	335.79	-249.34	82.28
33P	26.97	736.01	46.74	440.22	362.79	261.40	91.01
33X	26.97	-55.86	-11.36	1147.04	833.30	207.85	156.56
33XY	-17.80	-54.96	13.62	-1003.62	-212.10	-201.81	-38.23
33Y	-17.79	-54.96	13.62	-1003.62	-212.10	-201.81	-38.23
34P	26.83	-1147.05	13.62	1131.23	-837.40	208.82	-156.91
34X	26.94	1003.63	-833.29	-4052.23	1550.80	-990.21	-454.04
34XY	-17.77	1001.58	212.10	4195.13	585.08	980.38	151.85
34Y	-17.77	1001.58	212.10	4195.13	585.08	980.38	151.85
35P	-17.65	-1151.23	837.40	-4681.60	-996.83	994.84	-152.73
35X	-3.27	4052.33	1550.79	705.49	131.25	895.18	454.88
35XY	13.52	-4195.22	-585.07	-838.60	-426.45	-947.17	316.47
35Y	13.52	-4195.22	-585.07	-838.60	-426.45	-947.17	316.47
36P	-24.50	4081.24	-1551.08	709.01	-170.13	901.28	-200.39
36X	-24.50	10.65	23.21	-65.11	31.27	-10.37	-323.84
36XY	27.86	10.65	-23.21	206.83	-8.32	41.42	-6.00
36Y	27.86	10.65	-23.21	206.83	-8.32	41.42	-6.00
37P	-24.50	10.72	22.62	205.99	8.66	41.27	5.95
37X	-24.50	65.11	-22.62	-63.65	-30.89	-10.08	-10.19
37XY	-24.49	-206.83	8.31	650.51	-83.61	-96.41	-21.89
37Y	-24.49	-206.83	8.31	650.51	-83.61	-96.41	-21.89
38P	27.85	-205.99	-8.65	638.47	82.39	82.37	-13.37
38X	27.85	-205.99	-8.65	638.47	82.39	82.37	-13.37
38XY	27.86	63.65	30.89	-585.32	88.23	-99.37	22.70

38P	-28.40	571.03	83.64	44.98	-118.96	107.67	-6.17
38X	-28.74	-620.33	78.54	-132.10	171.23	-131.86	43.64
38XY	32.22	-638.27	-82.38	-152.20	-174.54	-138.12	-44.89
38Y	31.85	585.12	-88.25	57.91	106.65	112.39	3.22
39P	0.00	-128.58	-15.04	-0.00	-0.00	-18.37	-2.15
39X	0.00	262.82	16.60	-0.00	0.00	37.55	2.37
39Y	0.00	265.45	9.50	-0.00	-0.00	37.92	1.36
40P	0.00	-133.02	-8.50	-0.00	-0.00	-19.00	-1.21
40X	-0.00	-302.79	-61.67	-0.00	-0.00	-43.25	-8.81
40XY	0.00	491.52	-21.85	0.00	0.00	70.22	-3.12
40Y	0.00	488.97	52.70	0.00	-0.00	69.86	7.53
41P	0.00	-298.83	37.26	0.00	0.00	-42.69	5.32
41X	-0.00	-36.82	-235.86	0.00	-0.00	-5.26	-33.69
41XY	0.00	235.61	-185.41	0.00	0.00	33.66	-26.49
41Y	0.00	238.56	214.26	0.00	-0.00	34.08	30.61
53P	-0.13	-41.00	217.31	0.00	0.00	-5.86	31.04
53X	-0.13	3.97	-5.27	-18.86	-9.34	-0.87	-0.85
53XY	0.37	3.97	5.27	25.60	4.22	1.72	0.55
53Y	0.37	4.01	-5.19	25.66	-4.23	1.73	-0.55
98P	0.12	-14.47	7.47	-18.90	9.14	-0.87	0.84
98X	0.08	14.28	-12.62	-21.95	-29.19	-6.73	-4.01
98XY	0.08	14.28	12.62	17.24	-6.68	5.97	-3.56
98Y	0.12	-14.47	-7.47	-18.68	28.35	-6.12	3.81
99P	0.00	-5.98	-7.16	9.12	7.23	0.25	3.86
99X	0.02	9.51	0.93	-10.15	-0.35	-0.05	0.01
100P	-0.01	3.23	-5.53	0.71	10.38	0.23	0.28
100X	-0.07	3.03	1.06	-4.86	4.39	-0.11	0.32

Summary of Clamp Capacities and Usages for Load Case "NESC Extreme":

Clamp Force Label	Input Factored Usage	
	Holding Capacity (kips)	Usage Capacity (kips) %
C1 S.168	50.00	50.00 10.34
C2 2.508	50.00	50.00 5.02
C3 2.916	50.00	50.00 5.83
C4 2.916	50.00	50.00 5.83
C5 2.916	50.00	50.00 5.83
C6 2.916	50.00	50.00 5.83
C7 2.916	50.00	50.00 5.83
C8 2.916	50.00	50.00 5.83
C9 2.916	50.00	50.00 5.83
C10 2.916	50.00	50.00 5.83
C11 2.918	50.00	50.00 5.84
C12 2.918	50.00	50.00 5.84
C13 2.918	50.00	50.00 5.84
C14 2.918	50.00	50.00 5.84
C15 2.933	50.00	50.00 5.87
C16 2.933	50.00	50.00 5.87
C17 2.933	50.00	50.00 5.87
C18 2.933	50.00	50.00 5.87
C19 2.935	50.00	50.00 5.87
C20 2.935	50.00	50.00 5.87
C21 2.935	50.00	50.00 5.87
C22 2.935	50.00	50.00 5.87
C23 2.937	50.00	50.00 5.87
C24 2.937	50.00	50.00 5.87
C25 2.937	50.00	50.00 5.87
C26 2.937	50.00	50.00 5.87
C27 4.598	50.00	50.00 5.87
C28 0.690	50.00	50.00 9.20
C29 0.926	50.00	50.00 1.38
C30 0.834	50.00	50.00 1.85
C31 0.956	50.00	50.00 1.67
		50.00 1.91

C32	1.877	50.00	3.75
C33	1.026	50.00	2.05
C34	5.103	50.00	10.21
C35	0.733	50.00	1.47
C36	1.093	50.00	2.19
C37	0.838	50.00	1.68
C38	0.960	50.00	1.92
C39	1.884	50.00	3.77
C40	1.026	50.00	2.05
C41	4.240	50.00	8.48
C42	4.740	50.00	9.48
C43	1.168	50.00	2.34
C44	1.357	50.00	2.71

Equilibrium Joint Positions and Rotations for Load Case "NESC Broken Wire":

Joint Label	X-Displ (ft)	Y-Displ (ft)	Z-Displ (ft)	X-Rot (deg)	Y-Rot (deg)	Z-Rot (deg)	X-Pos (ft)	Y-Pos (ft)	Z-Pos (ft)
1P	0.02006	0.1763	-0.01854	0.0000	0.0000	0.0000	0.02006	14.18 93.98	
2P	0.01373	0.1539	-0.02077	-0.0812	0.0428	0.1151	3.514	15.15 84.98	
3P	0.01047	0.1467	-0.02028	-0.1088	0.0275	0.1120	3.51	15.15 79.98	
4P	0.00876	0.1331	-0.02062	-0.2110	0.0224	0.0922	3.509	15.13 74.98	
5P	0.006243	0.1145	-0.01912	-0.1534	0.0336	0.0723	3.506	15.11 69.98	
6P	0.003884	0.1057	-0.01841	-0.1608	0.0173	0.0467	3.504	15.11 64.98	
7P	0.002539	0.08859	-0.01802	-0.2366	0.0163	0.0285	3.503	15.09 59.98	
8P	0.0007803	0.06835	-0.0167	-0.1734	0.0269	0.0102	3.501	15.07 54.98	
9P	-0.001223	0.0578	-0.01586	-0.1380	0.0071	-0.0142	3.499	15.06 49.98	
14P	0	0	0	0.0000	0.0000	0.0000	13.07	19.07	0
15P	-0.004524	0.1468	-0.03439	-0.1125	0.0275	0.1280	3.495	22.15 79.97	
16P	-0.005545	0.1058	-0.03494	-0.1227	0.0174	0.0923	3.494	22.11 64.97	
17P	-0.004518	0.0579	-0.03499	-0.1658	0.0072	0.0474	3.495	22.06 49.97	
18P	0.04937	0.1516	-0.01438	0.0124	0.0729	0.1419	3.549	0.1516 84.99	
19P	0.03443	0.1511	-0.01162	0.0459	0.0611	0.1431	3.534	6.151 84.99	
20P	0.02345	0.1527	-0.01073	-0.0786	0.0518	0.1331	3.523	6.151 84.99	
21P	0.04277	0.1479	-0.01454	0.0214	0.0801	0.1285	3.543	0.1493 79.99	
22P	0.02964	0.1493	-0.012	0.0284	0.0592	0.1228	3.53	6.148 79.99	
23P	0.02001	0.1466	-0.01193	-0.0642	0.0433	0.1244	3.52	10.65 79.99	
24P	0.02722	0.1106	-0.01027	0.0322	0.0845	0.0892	3.527	0.1106 69.99	
25P	0.01791	0.1103	-0.007894	0.0696	0.0643	0.0806	3.518	6.11 69.99	
26P	0.0121	0.1113	-0.005775	-0.0862	0.0489	0.0731	3.512	10.61 69.99	
27P	0.02345	0.1093	-0.01266	0.0455	0.0707	0.0748	3.523	0.1093 64.99	
28P	0.01568	0.1074	-0.008293	0.0443	0.0495	0.0734	3.516	6.107 64.99	
29P	0.009705	0.1058	-0.007513	-0.0679	0.0335	0.0825	3.51	10.61 64.99	
30P	0.009296	0.06391	-0.00878	-0.0278	0.0645	0.0431	3.509	0.06391 54.99	
31P	0.004807	0.06382	-0.004381	0.0665	0.0496	0.0325	3.505	6.064 55	
32P	0.006416	0.06252	-0.002543	-0.0907	0.0383	0.0277	3.503	10.57 55	
33P	0.003381	0.06014	-0.004729	-0.0421	0.0273	0.0316	3.506	0.06252 49.99	
35P	0.0006095	0.0582	-0.004455	-0.0822	0.0173	0.0395	3.503	6.06 50	
36P	0.002122	0.0295	-0.009109	-0.0101	0.0274	0.0178	3.501	10.56 50	
37P	5.436e-006	0.02942	-0.009342	0.0120	0.0244	0.0343	5.377	0.0295 39.99	
38P	-0.003134	0.03015	-0.008848	-0.0310	0.0215	0.0164	5.375	5.279 39.99	
39P	0.0007001	0.02647	-0.009247	-0.0024	0.0114	0.0153	5.372	10.53 39.99	
40P	-0.0006566	0.02637	-0.009496	-0.0024	0.0064	0.0152	6.334	0.02647 34.99	
41P	-0.002145	0.02607	-0.01028	-0.0227	0.0014	0.0173	6.332	5.276 34.99	
44P	-0.001562	0.03415	0.02547	0.0000	0.0000	0.0000	-0.001362	17.97 17.78	
45P	-0.001535	0.03163	-0.1534	0.0000	0.0000	0.0000	-0.001535	10.53 39.85	
1X	0.1061	0.1725	0.0007794	0.0000	0.0000	0.0000	0.1061	-13.83 94	
2X	0.08957	0.1549	-0.005209	-0.0587	0.0000	0.0000	3.59	-14.85 84.99	
2Y	0.09001	0.137	0.009708	-0.0912	0.1163	0.1639	-3.41	-14.86 85.01	
3X	0.01333	0.1379	-0.01725	-0.0724	0.0283	0.1311	-3.487	-15.14 84.98	
3Y	0.07977	0.1489	-0.004787	-0.1172	0.1321	0.1593	-3.487	-14.85 80.01	
3XY	0.07936	0.1291	0.01008	-0.1016	0.1341	0.1626	-3.421	-14.87 80.01	
3Y	0.01075	0.1316	-0.01729	-0.0959	0.0345	0.1187	-3.489	-14.87 75	
4X	0.06686	0.1323	-0.003981	-0.2309	0.1532	0.1308	-3.489	-14.87 75	
4XY	0.06689	0.1174	0.01046	-0.1622	0.1456	0.1334	-3.433	-14.88 75.01	
4Y	0.007802	0.1199	-0.01712	-0.1756	0.0280	0.1031	-3.492	-15.12 74.98	
5X	0.05438	0.1146	-0.004045	-0.1316	0.1347	0.1019	-3.554	-14.89 70	
5XY	0.05458	0.1039	0.009888	-0.1109	0.1115	0.1040	-3.445	-14.9 70.01	
5Y	0.005989	0.1045	-0.01606	-0.1310	0.0211	0.0875	-3.494	-15.1 69.98	
6X	0.04328	0.1061	-0.002766	-0.2042	0.1233	0.0582	-3.494	-14.89 65	
6XY	0.04285	0.08669	0.009758	-0.1452	0.1167	0.0729	-3.457	-14.9 65.01	
6Y	0.003935	0.08627	-0.01563	-0.1496	0.0267	0.0704	-3.496	-15.1 64.98	
7XY	0.03283	0.08552	-0.001924	-0.2419	0.1145	0.0416	-3.533	-14.91 60	
7Y	0.03306	0.08115	0.009558	-0.2095	0.0094	0.0683	-3.467	-14.92 60.01	
7Y	0.001756	0.08081	-0.01538	-0.2055	0.0221	0.0662	-3.498	-15.08 59.98	
8X	0.02335	0.06809	-0.001725	-0.1293	0.1015	0.0247	-3.523	-14.93 55	
8XY	0.02373	0.06364	0.008503	-0.1485	0.1050	0.0635	-3.476	-14.94 55.01	

8Y	0.0002785	0.06361	-0.01435	-0.1479	0.0122	0.0619	-3.5	15.06	54.99
9X	0.0156	0.05956	-0.008326	-0.1491	0.0733	-0.0039	3.516	-14.94	50
9Y	0.01554	0.05436	-0.007726	-0.1183	0.0726	0.0624	-3.484	-14.95	50.01
14X	-0.0008558	0.05432	-0.01371	-0.1223	0.0209	0.0653	-3.501	15.05	49.99
14Y	0	0	0	0.0000	0.0000	0.0000	13.07	-19.07	0
14Z	0	0	0	0.0000	0.0000	0.0000	-13.07	-19.07	0
15X	0.1034	0.1496	0.002014	-0.0257	0.1325	0.2097	-13.07	19.07	0
15Y	0.1042	0.1291	0.01724	-0.0380	0.1344	0.2239	3.603	-21.85	80
16X	-0.004504	0.1317	-0.02967	-0.1042	0.0345	0.1279	-3.396	-21.87	80.02
16Y	0.05251	0.1067	0.003508	0.0244	0.1169	0.0811	3.505	-22.13	79.97
16Z	0.05244	0.09732	0.01553	0.0013	0.1169	0.0811	3.553	-21.89	65
17X	-0.005518	0.09637	-0.03114	-0.1157	0.0268	0.0808	-3.448	-21.9	65.02
17Y	0.02061	0.06006	0.005962	-0.0092	0.0735	0.0632	3.506	22.1	64.97
17Z	0.02053	0.05507	0.01685	-0.0530	0.0726	0.0300	-3.521	-21.94	50.01
18X	-0.004533	0.05442	-0.03089	-0.1497	0.0208	0.0300	-3.479	-21.94	50.02
18Y	0.04985	0.1355	-0.005668	-0.0249	0.0208	0.0125	-3.505	22.05	49.97
18Z	0.06464	0.1518	-0.01605	0.0295	0.0724	0.1464	-3.445	0.1355	84.99
19X	0.06513	0.1386	-0.003728	-0.0198	0.0849	0.1549	3.565	-5.848	84.99
19Y	0.03491	0.1336	-0.007406	0.0121	0.0549	0.1480	-3.435	-5.864	85
20X	0.07721	0.1535	-0.0156	-0.0867	0.0935	0.1599	-3.465	6.136	84.99
20Y	0.07715	0.1363	6.695e-005	-0.0517	0.0935	0.1599	3.577	-10.35	84.99
20Z	0.02468	0.1369	-0.007828	-0.0791	0.0415	0.1402	-3.423	-10.36	85
21Y	0.04285	0.1321	-0.005626	-0.0170	0.0845	0.1326	-3.475	10.64	84.99
22X	0.05662	0.1485	-0.01644	-0.0314	0.1010	0.1365	-3.457	0.1321	79.99
22Y	0.05704	0.131	-0.004106	-0.0331	0.1043	0.1383	3.557	-5.852	79.98
22Z	0.02934	0.132	-0.007779	-0.0061	0.0646	0.1247	-3.443	-5.869	80
23X	0.06771	0.1477	-0.01455	-0.0856	0.1165	0.1469	3.471	6.132	79.99
23Y	0.06795	0.1295	0.001027	-0.1024	0.1191	0.1376	3.568	-10.35	79.99
23Z	0.01985	0.1313	-0.009133	-0.0656	0.0495	0.1166	-3.432	-10.37	80
24X	0.02776	0.1106	-0.003456	-0.0066	0.0815	0.0892	-3.48	10.63	79.99
25X	0.03672	0.1106	-0.003339	0.0582	0.048	0.1020	-3.472	0.1013	70
25Y	0.03728	0.1014	-0.003339	0.0055	0.1056	0.1031	3.537	-5.889	69.98
25Z	0.01845	0.1014	-0.003339	0.0183	0.0574	0.0794	-3.463	6.101	70
26X	0.04553	0.1132	-0.01784	-0.1047	0.1195	0.1175	3.546	-10.39	69.98
26Y	0.04609	0.1028	-0.00122	-0.1004	0.1235	0.1131	-3.454	-10.4	70
26Z	0.01264	0.1032	-0.004263	-0.0928	0.0392	0.0773	-3.487	10.6	70
27X	0.02346	0.09861	-0.003413	0.0615	0.0719	0.0810	-3.477	0.09861	65
28X	0.03124	0.1074	-0.01173	0.0318	0.0919	0.0739	3.531	-5.893	64.98
28Y	0.03178	0.09749	-0.003734	-0.0090	0.0899	0.0766	-3.468	-5.903	65
28Z	0.01516	0.09747	-0.003756	0.0013	0.0539	0.0756	3.485	6.097	65
29X	0.03723	0.09747	-0.003756	0.0013	0.0539	0.0756	3.537	-10.39	64.98
29Y	0.0375	0.1058	-0.01604	-0.0961	0.1076	0.0816	-3.462	-10.4	65
29Z	0.009465	0.09624	-0.0004283	-0.0806	0.1033	0.0681	-3.491	10.6	64.99
30Y	0.009708	0.09619	-0.005377	-0.0765	0.0403	0.0707	-3.49	0.06004	55
31X	0.01379	0.06004	-0.003836	0.0023	0.0586	0.0420	-3.49	-5.936	54.99
31Y	0.01422	0.06019	-0.004835	0.0248	0.0773	0.0561	3.514	-5.94	55
31Z	0.005219	0.05998	-0.002352	0.0368	0.0558	0.0372	-3.486	-5.94	55
32X	0.01884	0.06658	-0.01474	-0.0901	0.0400	0.0337	-3.495	6.06	55
32Y	0.01924	0.06231	-0.004113	-0.0966	0.0911	0.0607	3.519	-10.43	54.99
32Z	0.003222	0.06224	-0.001994	-0.0867	0.0260	0.0233	-3.481	-10.44	55
33Y	0.006347	0.05755	-0.003793	0.0126	0.0467	0.0397	-3.497	10.56	55
34X	0.009705	0.06008	-0.01327	0.0398	0.0538	0.0372	-3.494	0.05755	50
34Y	0.01038	0.05599	-0.005244	0.0348	0.0558	0.0372	3.51	-5.939	49.99
34Z	0.002629	0.05598	-0.002705	0.0348	0.0570	0.0336	-3.49	-5.944	49.99
35X	0.01306	0.05936	-0.01281	-0.0914	0.0363	0.0298	3.497	6.056	50
35Y	0.01263	0.05454	-0.002608	-0.0953	0.0647	0.0477	-3.513	-10.44	49.99
35Z	0.0009594	0.05452	-0.003498	-0.0789	0.0252	0.0252	3.487	-10.45	50
36Y	0.001701	0.02721	-0.003005	-0.0242	0.0285	0.0096	-3.499	10.55	50
37X	0.003478	0.02952	-0.008449	-0.0242	0.0199	0.0206	-3.499	10.55	50
37Y	0.003369	0.02726	-0.001074	-0.0001	0.0303	0.0084	5.378	0.02721	40
37Z	0.0003617	0.02719	-0.004659	-0.0075	0.0253	0.0293	-5.371	-5.222	39.99
38X	0.004201	0.03026	-0.007262	-0.0514	0.0145	0.0030	-5.375	-5.223	40
38Y	0.006392	0.03026	-0.0008309	-0.0536	0.0332	0.0152	5.379	-10.47	39.99
39Y	0.000231	0.02776	-0.0008309	-0.0536	0.0306	0.0152	-5.369	-10.47	39.99
40X	0.0008683	0.02309	-0.002747	-0.0433	0.0091	0.0161	-5.375	10.53	39.99
40Y	0.002137	0.02563	-0.002747	-0.0188	0.0102	0.0153	-6.332	0.02309	35
40Z	0.002171	0.0226	-0.0008032	-0.0267	0.0114	0.0138	6.335	-5.224	34.99
40Y	-0.0006338	0.02282	-0.004505	-0.0195	0.0089	0.0169	-6.331	-5.227	35
							-6.334	5.273	35

Joint Label	X Force Usage (kips)	X %	Y Force Usage (kips)	Y %	Z Force Usage (kips)	Z %	Comp. Usage %	Uplift Result. Force Usage (kips)	Force Usage % (kips)	X-M. Moment Usage (ft-k)	Y-M. Moment Usage (ft-k)	Z-M. Moment Usage (ft-k)	Max. Usage %
41X	0.003265		0.02479		-0.006119		-0.0532	0.0213	0.0083	6.336	-10.48	34.99	
41XY	0.003472		0.02212		0.002598		-0.0497	0.0126	0.0147	-6.33	-10.48	34.99	
41Y	-0.002151		0.02255		-0.006814		-0.0367	0.0077	0.0160	-6.335	10.52	34.99	
44X	-0.0006836		0.1606		-0.01087		0.0000	0.0000	0.0000	-0.0006836	-17.47	17.74	
45X	0.005258		0.0271		-0.1276		0.0000	0.0000	0.0000	0.005258	-10.47	39.87	
1S	-0.0008891		0.04204		-0.01616		-0.1717	0.0048	-0.0244	4.456	15.45	44.98	
1S	-0.002718		0.03032		-0.01549		0.0854	0.0176	-0.0105	5.412	15.84	34.99	
12S	-0.003511		0.02544		-0.0142		-0.0486	-0.0043	0.0051	6.368	16.25	34.99	
13S	-0.001529		0.0115		-0.009951		-0.0650	-0.0167	-0.0033	8.54	17.16	23.66	
42S	1.216e-005		0.01156		-0.001846		0.0031	-0.0014	0.0027	8.541	0.01156	23.66	
43S	-0.002894		0.03017		-0.01407		0.0863	0.0148	0.0113	-0.002894	15.84	39.99	
10X	0.01042		0.04124		0.0007303		-0.1904	0.0476	0.0000	4.468	-15.37	45	
10XY	0.01108		0.03991		0.008894		-0.1596	0.0497	0.0438	-4.446	-15.37	45.01	
10Y	-0.003123		0.03959		-0.0137		-0.1551	0.0093	0.0632	-4.46	15.45	44.99	
11X	0.006731		0.03037		0.000895		-0.0968	0.0371	0.0283	5.421	-15.79	40.01	
11XY	0.006777		0.028		0.003033		-0.0998	0.0354	0.0050	-5.408	-15.79	40.01	
11Y	-0.003038		0.0279		-0.01293		0.0871	0.0043	0.0424	-5.418	15.84	39.99	
12X	0.004181		0.0235		0.001067		-0.0757	0.0272	0.0164	6.376	-16.2	35	
12XY	0.004706		0.02146		-0.0085		-0.0613	0.0138	0.0071	-6.367	-16.2	35.01	
12Y	-0.003979		0.02199		-0.01162		-0.0522	0.0066	0.0240	8.541	-17.13	23.67	
13X	0.0002316		0.01132		0.0005114		-0.0524	0.0139	0.0101	-8.539	-17.13	23.67	
13XY	0.001973		0.00935		0.006205		-0.0482	0.0075	0.0065	-8.542	17.15	23.66	
13Y	-0.0008005		0.009405		-0.008782		-0.0504	-0.0145	0.0165	-8.541	0.008765	23.67	
42Y	-3.524e-005		0.008765		-0.0005395		-0.0129	-0.0035	0.0012	-8.541	0.008765	23.67	
43X	0.006737		0.02844		0.005161		-0.0983	0.0464	0.0106	0.006737	-15.79	40.01	

Joint Support Reactions for Load Case "NESC Broken Wire":

Joint Displacements, Loads and Member Forces on Joints for Load Case "NESC Broken Wire":

Joint Label	X External Load (kips)	Y External Load (kips)	Z External Load (kips)	X Member Force (kips)	Y Member Force (kips)	Z Member Force (kips)	X Disp. (ft)	Y Disp. (ft)	Z Disp. (ft)	X-M. Moment Usage (ft-k)	Y-M. Moment Usage (ft-k)	Z-M. Moment Usage (ft-k)	Max. Usage %
1P	0.0000	5.7421	-1.7446	-0.0000	-5.7421	1.7446	0.0201	0.1763	-0.0185	0.0	0.0	-0.01	0.0
2P	0.0000	0.0994	-0.2208	0.0000	-0.0994	0.2208	0.0137	0.1539	-0.0208	0.0	0.0	-0.04	0.0
3P	0.0000	1.2431	-3.7360	0.0000	-1.2431	3.7360	0.0103	0.1467	-0.0208	0.0	0.0	-0.03	0.0
4P	0.0000	0.1068	-0.2751	0.0000	-0.1068	0.2751	0.0088	0.1331	-0.0206	0.0	0.0	-0.03	0.0
5P	0.0000	0.1208	-0.3039	-0.0000	-0.1208	0.3039	0.0062	0.1145	-0.0191	0.0	0.0	-0.03	0.0
6P	0.0000	0.1373	-0.4363	-0.0000	-0.1373	0.4363	0.0039	0.1057	-0.0184	0.0	0.0	-0.03	0.0
7P	0.0000	-0.2798	-0.9943	0.0000	0.2798	-0.9943	0.0025	0.0886	-0.0180	0.0	0.0	-0.03	0.0
8P	0.0000	0.1465	-0.4796	-0.0000	-0.1465	0.4796	0.0008	0.0684	-0.0167	0.0	0.0	-0.03	0.0
9P	0.0000	0.1547	-0.5437	0.0000	-0.1547	0.5437	0.0012	0.0578	-0.0159	0.0	0.0	-0.03	0.0
14P	0.0000	0.2837	-1.2171	23.6178	36.3859	-128.4309	0.0000	0.0000	0.0000	0.0	0.0	-0.03	0.0
15P	0.0000	3.3540	-1.5943	-0.0000	-3.3540	1.5943	0.0045	0.1468	-0.0344	0.0	0.0	-0.03	0.0
16P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	0.0055	0.1058	-0.0349	0.0	0.0	-0.03	0.0
17P	0.0000	3.3540	-1.6031	0.0000	-3.3540	1.6031	0.0045	0.0579	-0.0350	0.0	0.0	-0.03	0.0
18P	0.0000	0.0403	-0.1290	-0.0000	-0.0403	0.1290	0.0494	0.1516	-0.0144	0.0	0.0	-0.03	0.0
19P	0.0000	0.0670	-0.1797	-0.0000	-0.0670	0.1797	0.0344	0.1511	-0.0116	0.0	0.0	-0.03	0.0
20P	0.0000	0.0629	-0.1467	-0.0000	-0.0629	0.1467	0.0235	0.1527	-0.0107	0.0	0.0	-0.03	0.0
21P	0.0000	0.0787	-0.2152	-0.0000	-0.0787	0.2152	0.0428	0.1493	-0.0143	0.0	0.0	-0.03	0.0
22P	0.0000	3.3633	-1.6160	-0.0000	-3.3633	1.6160	0.0206	0.1479	-0.0120	0.0	0.0	-0.03	0.0
23P	0.0000	0.0943	-0.2539	-0.0000	-0.0943	0.2539	0.0200	0.1466	-0.0119	0.0	0.0	-0.03	0.0
24P	0.0000	0.0403	-0.1498	-0.0000	-0.0403	0.1498	0.0272	0.1106	-0.0127	0.0	0.0	-0.03	0.0
25P	0.0000	0.0720	-0.2278	-0.0000	-0.0720	0.2278	0.0179	0.1103	-0.0079	0.0	0.0	-0.03	0.0
26P	0.0000	0.0570	-0.1766	-0.0000	-0.0570	0.1766	0.0121	0.1130	-0.0058	0.0	0.0	-0.03	0.0
27P	0.0000	0.0853	-0.2711	-0.0000	-0.0853	0.2711	0.0235	0.1093	-0.0127	0.0	0.0	-0.03	0.0
28P	0.0000	3.3633	-1.6342	-0.0000	-3.3633	1.6342	0.0157	0.1074	-0.0083	0.0	0.0	-0.03	0.0
29P	0.0000	0.1060	-0.3019	0.0000	-0.1060	0.3019	0.0097	0.1058	-0.0075	0.0	0.0	-0.03	0.0

30P	0.0000	0.0403	-0.1649	0.0000	-0.0403	0.1649	0.0093	0.0639	-0.0088
31P	0.0000	0.0737	-0.2597	0.0000	-0.0737	0.2597	0.0048	0.0638	-0.0044
32P	0.0000	0.0620	-0.1998	0.0000	-0.0620	0.1998	0.0028	0.0667	-0.0025
33P	0.0000	0.0853	-0.3124	0.0000	-0.0853	0.3124	0.0064	0.0625	-0.0087
34P	0.0000	3.3633	-1.6474	0.0000	-3.3633	1.6474	0.0034	0.0601	-0.0047
35P	0.0000	0.1096	-0.3625	0.0000	-0.1096	0.3625	0.0006	0.0582	-0.0045
36P	0.0000	0.0854	-0.4182	0.0000	-0.0854	0.4182	0.0021	0.0295	-0.0091
37P	0.0000	0.0656	-0.4356	0.0000	-0.0656	0.4356	0.0000	0.0294	-0.0091
38P	0.0000	0.1097	-0.5719	0.0000	-0.1097	0.5719	-0.0031	0.0301	-0.0088
39P	0.0000	0.1286	-0.4881	0.0000	-0.1286	0.4881	0.0007	0.0285	-0.0092
40P	0.0000	0.0355	-0.2388	0.0000	-0.0355	0.2388	-0.0007	0.0263	-0.0095
41P	0.0000	0.1458	-0.5677	0.0000	-0.1458	0.5677	-0.0021	0.0261	-0.0103
42P	0.0000	0.1730	-0.2780	0.0000	-0.1730	0.2780	0.0014	0.3415	-0.0103
43P	0.0000	0.0539	-0.1262	0.0000	-0.0539	0.1262	0.0015	0.0316	-0.0255
44P	0.0000	3.9001	-1.3756	0.0000	-3.9001	1.3756	0.1061	0.1725	-0.1534
45P	0.0000	0.1157	-0.2503	0.0000	-0.1157	0.2503	0.0896	0.1549	-0.0052
46P	0.0000	0.0994	-0.2208	0.0000	-0.0994	0.2208	0.0900	0.1370	-0.0097
47P	0.0000	0.1157	-0.2503	0.0000	-0.1157	0.2503	0.0133	0.1379	-0.0173
48P	0.0000	1.1016	-3.4710	0.0000	-1.1016	3.4710	0.0798	0.1489	-0.0048
49P	0.0000	1.2256	-4.8150	0.0000	-1.2256	4.8150	0.0794	0.1291	-0.0101
50P	0.0000	1.3671	-4.0800	0.0000	-1.3671	4.0800	0.0108	0.1316	-0.0173
51P	0.0000	0.1068	-0.2751	0.0000	-0.1068	0.2751	0.0669	0.1123	-0.0040
52P	0.0000	0.1068	-0.2751	0.0000	-0.1068	0.2751	0.0669	0.1123	-0.0040
53P	0.0000	0.1371	-0.3334	0.0000	-0.1371	0.3334	0.0078	0.1199	-0.0171
54P	0.0000	0.2448	-0.6479	0.0000	-0.2448	0.6479	0.0544	0.1146	-0.0040
55P	0.0000	0.2611	-0.6774	0.0000	-0.2611	0.6774	0.0546	0.1039	-0.0099
56P	0.0000	0.1373	-0.4363	0.0000	-0.1373	0.4363	0.0433	0.1045	-0.0161
57P	0.0000	0.1373	-0.4363	0.0000	-0.1373	0.4363	0.0429	0.0967	-0.0098
58P	0.0000	-0.2208	-0.9943	0.0000	0.2208	0.9943	0.0328	0.0855	-0.0156
59P	0.0000	-0.0968	-1.3383	0.0000	0.0968	1.3383	0.0331	0.0812	-0.0019
60P	0.0000	-0.1558	-0.5091	0.0000	0.1558	0.5091	0.0218	0.0808	-0.0154
61P	0.0000	0.1629	-0.4796	0.0000	-0.1629	0.4796	0.0235	0.0681	-0.0017
62P	0.0000	0.1465	-0.5091	0.0000	-0.1465	0.5091	0.0237	0.0636	-0.0085
63P	0.0000	0.1629	-0.5091	0.0000	-0.1629	0.5091	0.0003	0.0636	-0.0144
64P	0.0000	0.2784	-0.8877	0.0000	-0.2784	0.8877	0.0156	0.0596	-0.0008
65P	0.0000	0.2837	-0.8877	0.0000	-0.2837	0.8877	0.0155	0.0546	-0.0077
66P	0.0000	0.2837	-1.2171	0.0000	-0.2837	1.2171	-0.0009	0.0543	-0.0137
67P	0.0000	0.2837	-1.2171	0.0000	-0.2837	1.2171	0.0000	0.0543	-0.0137
68P	0.0000	0.2837	-1.2171	0.0000	-0.2837	1.2171	0.0000	0.0543	-0.0137
69P	0.0000	0.0450	-0.1323	0.0000	-0.0450	0.1323	0.0000	0.0000	0.0000
70P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	0.1034	0.1496	0.0020
71P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	0.1042	0.1291	0.0172
72P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	0.0045	0.1317	-0.0297
73P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	0.0525	0.1067	0.0035
74P	0.0000	3.3540	-1.5943	0.0000	-3.3540	1.5943	0.0524	0.0973	0.0155
75P	0.0000	3.3540	-1.6031	0.0000	-3.3540	1.6031	0.0055	0.0564	-0.0311
76P	0.0000	3.3540	-1.6031	0.0000	-3.3540	1.6031	0.0206	0.0601	0.0060
77P	0.0000	3.3540	-1.6031	0.0000	-3.3540	1.6031	0.0205	0.0551	0.0168
78P	0.0000	0.0403	-0.1290	0.0000	-0.0403	0.1290	0.0045	0.0544	-0.0309
79P	0.0000	0.0670	-0.1829	0.0000	-0.0670	0.1829	0.0499	0.1355	-0.0057
80P	0.0000	0.0670	-0.1797	0.0000	-0.0670	0.1797	0.0646	0.1518	-0.0160
81P	0.0000	0.0629	-0.1467	0.0000	-0.0629	0.1467	0.0651	0.1356	-0.0037
82P	0.0000	0.0629	-0.1467	0.0000	-0.0629	0.1467	0.0549	0.1356	-0.0074
83P	0.0000	0.0629	-0.1467	0.0000	-0.0629	0.1467	0.0772	0.1535	-0.0156
84P	0.0000	0.0629	-0.1467	0.0000	-0.0629	0.1467	0.0771	0.1363	0.0001
85P	0.0000	3.3633	-1.6152	0.0000	-3.3633	1.6152	0.0247	0.1369	-0.0078
86P	0.0000	3.3633	-1.6152	0.0000	-3.3633	1.6152	0.0428	0.1321	-0.0056
87P	0.0000	3.3633	-1.6160	0.0000	-3.3633	1.6160	0.0566	0.1485	-0.0164
88P	0.0000	3.3633	-1.6160	0.0000	-3.3633	1.6160	0.0570	0.1310	-0.0041
89P	0.0000	0.0943	-0.2539	0.0000	-0.0943	0.2539	0.0293	0.1320	-0.0078
90P	0.0000	0.0943	-0.2539	0.0000	-0.0943	0.2539	0.0677	0.1477	-0.0146
91P	0.0000	0.0943	-0.2539	0.0000	-0.0943	0.2539	0.0679	0.1295	0.0010
92P	0.0000	0.0403	-0.1498	0.0000	-0.0403	0.1498	0.0199	0.1313	-0.0091
93P	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	0.0278	0.1013	-0.0035
94P	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	0.0367	0.1106	-0.0169
95P	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	0.0373	0.1014	-0.0033
96P	0.0000	0.0720	-0.2310	0.0000	-0.0720	0.2310	0.0185	0.1014	-0.0034

Angle Label	Torsion (ft-lbs)	Origin X Moment (ft-lbs)	Origin Y Moment (ft-lbs)	End X Moment (ft-lbs)	End Y Moment (ft-lbs)	X Shear (lbs)	Y Shear (lbs)
26X	0.0000	0.0570	-0.1766	0.0000	-0.0570	0.1766	0.0455
26XY	0.0000	0.0570	-0.1766	0.0000	-0.0570	0.1766	0.0461
26Y	0.0000	0.0570	-0.1766	0.0000	-0.0570	0.1766	0.1028
27X	0.0000	0.0853	-0.2711	0.0000	-0.0853	0.2711	0.0235
28X	0.0000	3.3633	-1.6342	0.0000	-3.3633	1.6342	0.0312
28XY	0.0000	3.3633	-1.6342	0.0000	-3.3633	1.6342	0.0318
28Y	0.0000	3.3633	-1.6342	0.0000	-3.3633	1.6342	0.0975
29X	0.0000	0.1060	-0.3019	0.0000	-0.1060	0.3019	0.0152
29XY	0.0000	0.1060	-0.3019	0.0000	-0.1060	0.3019	0.0372
29Y	0.0000	0.1060	-0.3019	0.0000	-0.1060	0.3019	0.0375
30X	0.0000	0.1649	-0.4649	0.0000	-0.1649	0.4649	0.0095
30XY	0.0000	0.1649	-0.4649	0.0000	-0.1649	0.4649	0.0962
30Y	0.0000	0.1649	-0.4649	0.0000	-0.1649	0.4649	0.0600
31X	0.0000	0.0737	-0.2597	0.0000	-0.0737	0.2597	0.0138
31XY	0.0000	0.0737	-0.2597	0.0000	-0.0737	0.2597	0.0639
31Y	0.0000	0.0737	-0.2597	0.0000	-0.0737	0.2597	0.0602
32X	0.0000	0.0620	-0.1998	0.0000	-0.0620	0.1998	0.0552
32XY	0.0000	0.0620	-0.1998	0.0000	-0.0620	0.1998	0.0600
32Y	0.0000	0.0620	-0.1998	0.0000	-0.0620	0.1998	0.0666
33X	0.0000	0.0853	-0.3124	0.0000	-0.0853	0.3124	0.0192
33XY	0.0000	0.0853	-0.3124	0.0000	-0.0853	0.3124	0.0623
33Y	0.0000	0.0853	-0.3124	0.0000	-0.0853	0.3124	0.0622
34X	0.0000	3.3633	-1.6474	0.0000	-3.3633	1.6474	0.0063
34XY	0.0000	3.3633	-1.6474	0.0000	-3.3633	1.6474	0.0575
34Y	0.0000	3.3633	-1.6474	0.0000	-3.3633	1.6474	0.0575
35X	0.0000	0.1096	-0.3625	0.0000	-0.1096	0.3625	0.0010
35XY	0.0000	0.1096	-0.3625	0.0000	-0.1096	0.3625	0.0545
35Y	0.0000	0.1096	-0.3625	0.0000	-0.1096	0.3625	0.0545
36X	0.0000	0.0854	-0.4182	0.0000	-0.0854	0.4182	0.0010
36XY	0.0000	0.0854	-0.4182	0.0000	-0.0854	0.4182	0.0545
36Y	0.0000	0.0854	-0.4182	0.0000	-0.0854	0.4182	0.0545
37X	0.0000	0.0656	-0.4356	0.0000	-0.0656	0.4356	0.0035
37XY	0.0000	0.0656	-0.4356	0.0000	-0.0656	0.4356	0.0272
37Y	0.0000	0.0656	-0.4356	0.0000	-0.0656	0.4356	0.0295
38X	0.0000	0.1097	-0.5719	0.0000	-0.1097	0.5719	0.0039
38XY	0.0000	0.1097	-0.5719	0.0000	-0.1097	0.5719	0.0273
38Y	0.0000	0.1097	-0.5719	0.0000	-0.1097	0.5719	0.0272
39X	0.0000	0.1286	-0.4881	0.0000	-0.1286	0.4881	0.0064
39XY	0.0000	0.1286	-0.4881	0.0000	-0.1286	0.4881	0.0278
39Y	0.0000	0.1286	-0.4881	0.0000	-0.1286	0.4881	0.0278
40X	0.0000	0.0355	-0.2388	0.0000	-0.0355	0.2388	0.0009
40XY	0.0000	0.0355	-0.2388	0.0000	-0.0355	0.2388	0.0231
40Y	0.0000	0.0355	-0.2388	0.0000	-0.0355	0.2388	0.0231
41X	0.0000	0.1458	-0.5677	0.0000	-0.1458	0.5677	0.0021
41XY	0.0000	0.1458	-0.5677	0.0000	-0.1458	0.5677	0.0221
41Y	0.0000	0.1458	-0.5677	0.0000	-0.1458	0.5677	0.0221
42X	0.0000	0.1730	-0.2780	0.0000	-0.1730	0.2780	0.0007
42XY	0.0000	0.1730	-0.2780	0.0000	-0.1730	0.2780	0.1606
42Y	0.0000	0.1730	-0.2780	0.0000	-0.1730	0.2780	0.1606
43X	0.0000	0.1348	-0.4484	0.0000	-0.1348	0.4484	0.0053
43XY	0.0000	0.1348	-0.4484	0.0000	-0.1348	0.4484	0.0271
43Y	0.0000	0.1348	-0.4484	0.0000	-0.1348	0.4484	0.0271
10S	0.0000	0.1173	-0.5387	0.0000	-0.1173	0.5387	0.0009
11S	0.0000	0.3706	-1.2107	0.0000	-0.3706	1.2107	0.0030
12S	0.0000	0.3438	-1.8597	0.0000	-0.3438	1.8597	0.0015
13S	0.0000	0.1365	-0.2574	0.0000	-0.1365	0.2574	0.0035
10XY	0.0000	0.1348	-0.4484	0.0000	-0.1348	0.4484	0.0029
11XY	0.0000	0.1348	-0.4484	0.0000	-0.1348	0.4484	0.0302
11Y	0.0000	0.1348	-0.4484	0.0000	-0.1348	0.4484	0.0302
11X	0.0000	0.1173	-0.5387	0.0000	-0.1173	0.5387	0.0011
11XY	0.0000	0.3043	-1.0547	0.0000	-0.3043	1.0547	0.0396
11Y	0.0000	0.3043	-1.0547	0.0000	-0.3043	1.0547	0.0396
12X	0.0000	0.2907	-1.0330	0.0000	-0.2907	1.0330	0.0304
12XY	0.0000	0.2907	-1.0330	0.0000	-0.2907	1.0330	0.0279
12Y	0.0000	0.2907	-1.0330	0.0000	-0.2907	1.0330	0.0279
13X	0.0000	0.3706	-1.2107	0.0000	-0.3706	1.2107	0.0042
13XY	0.0000	0.3706	-1.2107	0.0000	-0.3706	1.2107	0.0215
13Y	0.0000	0.3706	-1.2107	0.0000	-0.3706	1.2107	0.0215
13X	0.0000	0.6196	-1.8987	0.0000	-0.6196	1.8987	0.0011
13Y	0.0000	0.6196	-1.8987	0.0000	-0.6196	1.8987	0.0113
42Y	0.0000	0.3438	-1.8597	0.0000	-0.3438	1.8597	0.0094
43X	0.0000	0.1365	-0.2574	0.0000	-0.1365	0.2574	0.0008
43Y	0.0000	0.1365	-0.2574	0.0000	-0.1365	0.2574	0.0088

Moments for Angles Modeled as Beams:

Angle Label	Torsion (ft-lbs)	Origin X Moment (ft-lbs)	Origin Y Moment (ft-lbs)	End X Moment (ft-lbs)	End Y Moment (ft-lbs)	X Shear (lbs)	Y Shear (lbs)
2P	15.11	275.51	-6.70	616.68	180.97	178.44	34.85
2X	-7.40	355.13	6.71	1077.05	-360.11	286.46	-70.68

2XY	6.24	166.75	9.88	295.45	-210.97	92.44	-40.22
2Y	59.05	262.96	-9.88	52.51	-87.88	163.09	-19.57
3P	94.32	-894.76	-132.62	768.04	-131.10	54.65	-64.80
3X	136.24	-1249.72	372.03	153.29	107.86	-219.31	95.98
3XY	139.19	-408.46	222.23	339.05	78.87	-13.87	60.19
3Y	74.26	-422.20	76.78	562.24	155.43	28.02	46.41
4P	94.32	-768.03	131.19	-1479.57	-6.81	-449.65	24.99
4X	136.25	-153.30	-107.83	-1379.62	123.32	-306.56	3.24
4XY	139.21	-339.06	-78.82	-972.90	-27.58	-262.36	-21.18
5P	121.54	-562.26	-155.37	-1113.13	-69.19	-335.15	-44.86
5X	208.56	2127.02	-21.09	2112.57	180.58	826.89	31.71
5XY	148.05	1455.00	-95.91	3024.62	44.30	1030.60	-10.79
5Y	81.36	1559.85	60.35	1878.85	366.06	666.99	85.08
6P	477.64	-2107.70	-209.12	3057.51	-148.28	669.85	0.41
6X	438.36	-3708.60	-14.68	-1140.86	581.82	-970.01	113.51
6XY	124.97	-2286.77	-341.24	2093.42	151.97	-38.66	-37.89
7P	477.80	-3057.47	9.11	1987.94	320.52	33.65	65.90
7X	438.25	-1140.76	148.58	-7364.11	-567.86	-2084.89	-83.41
7XY	124.83	-2093.43	-582.10	-6528.68	304.32	-1077.60	-55.18
7Y	111.28	-1987.95	-151.92	-6250.34	149.99	-1668.39	-0.28
8P	639.81	7944.44	-320.48	5909.06	356.42	-1579.71	7.28
8X	749.77	7372.60	541.84	5534.97	1891.32	2696.49	86.24
8XY	28.79	6752.46	-280.28	8722.52	1643.50	3219.75	271.82
8Y	-88.72	6413.15	-119.12	4702.01	2090.32	2290.54	394.16
9P	89.85	195.29	-387.44	4667.64	-980.04	2216.45	-273.47
9X	-240.03	-4959.30	5478.68	-544.25	3257.90	-68.30	1710.98
9XY	714.22	110.74	-4992.92	-2304.92	5856.32	-1422.85	2640.54
9Y	186.64	754.20	-214.36	-2181.49	-20.49	-1404.53	-1404.53
10P	90.22	544.17	-4283.80	-813.29	-2636.94	-11.64	-1355.30
10X	-238.72	2305.28	-5856.23	510.32	417.31	500.36	-159.98
10XY	714.71	214.70	2181.30	-2227.36	417.58	551.30	-1064.90
11P	186.47	813.42	2636.91	2273.92	-1567.71	-394.11	120.32
11X	419.70	-2362.86	3308.19	-58.28	-1240.82	-474.20	-851.87
11XY	-192.67	2389.50	-1317.83	61.95	39.15	12.85	-250.38
11Y	297.26	-2326.82	1999.59	60.15	266.62	479.51	443.62
12P	47.41	-4.80	1396.78	145.57	771.11	12.00	187.41
12X	131.23	65.80	-341.86	157.51	389.30	19.30	4.10
12XY	-15.54	1276.98	-139.28	-301.39	-418.71	-24.34	-48.20
12Y	61.61	-182.24	-43.75	725.72	-373.39	173.12	-36.07
13P	55.70	-184.72	-727.53	-40.61	196.58	-9.22	-21.97
13X	112.86	184.72	-369.31	-293.41	341.35	-19.77	-1.15
13XY	-11.30	315.50	396.65	-47.48	-193.76	11.08	8.39
13Y	42.30	-677.48	381.81	-211.20	-226.97	-36.77	6.41
15P	-6.71	-10.80	-1.86	38.08	-0.03	4.55	-0.31
15X	9.88	18.71	4.71	11.34	20.91	-7.76	3.79
15XY	-9.88	18.71	-4.71	11.34	7.12	5.01	1.97
16P	-6.70	-38.08	0.03	-280.46	-25.57	15.24	-5.04
16X	-6.69	35.73	-20.91	281.29	-19.81	-70.76	-4.40
16XY	-9.88	-11.34	-7.13	147.13	11.66	70.48	-7.23
16Y	-9.87	-72.71	25.57	-250.09	41.37	30.18	1.74
17P	-6.73	280.46	19.82	275.51	-15.09	123.51	1.06
17X	-6.70	-281.29	11.65	-355.12	7.34	-141.47	4.21
17XY	-9.89	-147.12	-14.92	-166.74	-6.25	-69.76	-4.72
17Y	-9.89	250.09	-41.36	262.96	-59.06	113.99	-22.30
18P	-11.74	6.91	5.01	17.21	-3.30	4.02	0.29
18X	-11.74	6.91	-5.01	17.21	3.30	4.02	0.29
18XY	-11.18	32.52	-4.32	56.08	6.56	4.72	0.26
18Y	-11.18	32.52	4.32	-56.08	3.86	14.76	-0.07
19P	-11.74	-17.21	3.30	-197.37	-7.21	13.49	-0.48
19X	-11.74	-17.21	-3.30	197.37	6.13	-47.70	2.09
19XY	-11.18	-56.07	-3.87	78.75	13.33	32.41	1.51
19Y	-11.17	-48.44	7.21	-164.10	-5.43	5.04	-2.06
20P	-11.75	197.37	-6.11	110.62	-8.62	-47.24	-0.32
20X	-11.75	-167.29	-13.35	-105.57	10.53	68.44	-8.08
20XY	-11.19	-78.75	5.42	-80.21	54.03	-35.32	13.21

20Y	-11.17	164.10	8.64	105.06	12.61	59.81	4.73
21P	-27.68	-11.01	-27.83	121.87	-58.49	18.48	-14.38
21X	-27.69	11.01	27.83	-103.14	73.35	-19.03	16.86
21XY	-32.94	12.96	31.22	-29.91	80.74	-2.83	18.66
21Y	-32.94	12.96	-31.22	101.43	-66.02	19.07	-16.20
22P	-27.63	-121.88	58.50	-859.87	22.68	-218.04	17.98
22X	-27.61	103.15	-73.36	874.58	-1.80	217.39	-16.66
22XY	-32.89	29.93	-80.76	531.40	-34.66	124.78	-25.62
22Y	-32.90	-101.44	66.03	-627.29	55.53	-161.88	26.96
23P	-27.70	856.87	-22.59	541.64	-27.13	311.34	-11.01
23X	-27.62	-874.58	1.71	-747.45	-72.02	-260.56	-15.67
23XY	-32.92	531.41	34.60	-482.12	-8.60	225.28	5.74
23Y	-32.92	627.29	-55.45	446.42	-7.12	238.54	-13.87
24X	-28.96	33.19	0.09	29.12	-5.03	10.39	-0.85
24XY	-24.58	33.19	0.09	81.72	-3.14	19.15	-0.50
24Y	-24.58	51.29	0.94	88.47	-14.67	23.29	-2.28
25P	-28.96	-29.12	-0.94	50.82	-20.25	17.02	-3.53
25XY	-24.58	-88.47	14.55	583.89	47.70	-131.11	11.69
25Y	-24.57	-50.82	20.25	-419.25	38.36	98.22	9.24
26P	-29.10	560.65	-47.62	120.83	-217.43	151.45	-56.89
26X	-28.87	-523.89	-38.44	-11.96	-150.19	-119.07	-41.92
26XY	-24.60	-297.81	26.31	-39.09	48.67	-74.88	16.66
26Y	-24.58	419.25	3.29	72.95	1.64	109.37	1.10
27P	-24.94	-16.92	-42.90	150.53	-88.49	22.27	-21.89
27X	-24.95	-16.92	42.90	-176.82	84.99	-32.29	21.21
27XY	-30.98	-4.24	46.70	-101.36	107.85	-17.61	25.75
27Y	-30.98	-4.24	46.70	145.00	-82.56	23.46	-21.54
28P	-24.87	-150.54	88.49	-1056.92	60.04	-268.15	32.94
28X	-24.86	176.83	-85.00	1069.71	30.64	277.17	-12.04
28XY	-30.91	101.37	-107.86	801.27	-82.31	200.69	-42.24
28Y	-30.92	-145.01	82.56	-857.11	22.51	-222.58	23.29
29P	-25.09	1056.92	-59.95	580.31	-161.26	363.70	-49.11
29X	-24.66	-1069.71	30.73	-844.12	-310.00	-425.42	-75.78
29XY	-31.03	-801.27	82.23	-502.12	97.35	-289.73	39.89
29Y	-30.80	857.12	-22.42	504.11	199.81	302.39	39.43
30P	-22.03	36.39	3.73	42.36	18.57	13.13	3.72
30X	-22.03	36.39	-3.72	40.35	35.28	12.78	5.26
30XY	-17.23	50.19	-11.15	85.75	-37.44	22.65	-8.09
30Y	-17.23	50.19	11.15	71.49	-31.61	20.29	-3.41
31P	-22.05	-42.36	-18.56	-78.75	26.67	-178.10	1.78
31X	-22.05	-40.35	-35.30	715.90	24.26	150.07	-2.43
31XY	-17.25	-85.75	37.43	488.91	-11.58	89.56	5.76
31Y	-17.20	-71.50	31.62	-627.22	-84.76	-155.32	-11.83
32P	-22.28	758.74	-26.62	436.97	-336.41	265.75	-80.66
32X	-21.81	-715.90	-24.31	-383.63	-321.68	-244.34	-76.91
32XY	-17.34	-688.90	11.55	-355.84	225.60	-187.73	52.69
32Y	-17.01	627.23	84.80	376.72	405.47	223.10	108.96
33P	-73.31	-66.28	8.44	1366.19	1075.92	277.60	206.56
33X	-73.29	-66.29	-8.45	-713.47	-618.54	-148.52	-119.44
33XY	-134.81	-135.67	46.69	-909.61	522.08	-199.15	90.54
33Y	-134.79	-135.69	46.68	950.43	-1088.63	155.21	-198.45
34P	-73.42	-1366.18	-1075.93	-4157.05	-2231.79	-1051.88	-630.00
34X	-73.44	713.46	618.54	4041.32	1183.40	905.79	343.31
34XY	-134.75	909.82	-522.08	3587.23	1441.87	856.79	-374.06
34Y	-134.65	-950.46	1088.62	-3272.26	1936.04	-804.28	576.00
35P	-104.22	4156.33	2231.91	673.42	503.05	908.71	514.59
35X	-103.36	-4040.63	-1189.52	-1135.33	-471.45	-973.90	-311.41
35XY	-108.24	-3588.19	1441.72	-623.08	789.46	-792.41	419.62
35Y	-110.41	3273.25	-1933.91	461.18	-252.55	702.64	-411.75
36P	-50.99	26.78	35.20	30.80	30.58	10.97	12.53
36X	-50.98	26.78	-35.20	276.88	-42.29	57.83	-14.75
36XY	-12.67	12.94	45.42	222.68	6.42	44.88	9.87
36Y	-12.67	12.94	-45.42	-4.92	-2.73	1.53	-9.17
37P	-50.99	-30.80	-573.74	26.43	-115.16	-0.80	-18.20
37X	-50.99	-276.88	42.26	824.73	-137.90	104.34	-18.20
37XY	-12.67	-222.68	-6.42	391.44	16.05	32.14	1.84
37Y	-12.67	4.92	2.73	-454.44	-21.29	-85.63	-3.54

Clamp Force Label	Input Capacity (kips)	Factored Holding Capacity (kips)	Usage
38P	-54.93	573.38	-26.40
38X	-56.65	-824.37	137.86
38XY	-9.99	-391.51	-16.05
38Y	-9.56	454.51	21.30
39P	0.00	11.31	-48.86
39X	-0.00	278.28	-154.22
39XY	0.00	193.25	-187.02
39Y	0.00	25.24	-27.87
40P	0.00	-115.93	-138.76
40X	-0.00	695.88	-79.97
40XY	0.00	445.95	-25.75
40Y	0.00	-103.25	-31.70
41P	0.00	102.86	-228.46
41X	-0.00	518.23	-249.32
41XY	-0.00	242.18	119.68
41Y	0.00	101.40	195.62
53P	-2.32	8.87	-5.25
53X	-2.32	8.87	5.25
53XY	-1.67	2.53	-4.41
53Y	-1.67	2.52	4.41
98P	0.69	-5.18	11.88
98X	1.21	13.18	-20.00
98XY	1.21	13.18	20.00
98Y	0.69	-5.18	-11.88
99P	1.23	-38.87	-8.85
99X	-4.93	-33.85	8.79
100P	-4.62	-49.27	-9.36
100X	-1.32	-18.17	5.66

Summary of Clamp Capacities and Usages for Load Case "NESC Broken Wire":

Clamp Force Label	Input Capacity (kips)	Factored Holding Capacity (kips)	Usage
C1	6.001	50.00	12.00
C2	4.236	50.00	50.00
C3	3.714	50.00	8.27
C4	0.140	50.00	7.43
C5	11.849	50.00	0.28
C6	3.714	50.00	23.70
C7	3.714	50.00	7.43
C8	3.714	50.00	7.43
C9	3.714	50.00	7.43
C10	3.714	50.00	7.43
C11	3.717	50.00	7.43
C12	3.717	50.00	7.43
C13	3.717	50.00	7.43
C14	3.717	50.00	7.43
C15	3.731	50.00	7.43
C16	3.731	50.00	7.46
C17	3.731	50.00	7.46
C18	3.731	50.00	7.46
C19	3.739	50.00	7.46
C20	3.739	50.00	7.48
C21	3.739	50.00	7.48
C22	3.739	50.00	7.48
C23	3.745	50.00	7.48
C24	3.745	50.00	7.49
C25	3.745	50.00	7.49
C26	3.745	50.00	7.49
C27	4.007	50.00	7.49
C28	0.693	50.00	8.01
C29	1.342	50.00	1.39
C30	0.930	50.00	2.68
C31	1.098	50.00	1.86
		50.00	2.20

C32	1.997	50.00	50.00	3.99
C33	1.250	50.00	50.00	2.50
C34	4.303	50.00	50.00	8.61
C35	0.726	50.00	50.00	1.45
C36	1.347	50.00	50.00	2.69
C37	0.930	50.00	50.00	1.86
C38	1.098	50.00	50.00	2.20
C39	1.997	50.00	50.00	3.99
C40	1.250	50.00	50.00	2.50
C41	3.642	50.00	50.00	7.28
C42	3.937	50.00	50.00	7.87
C43	1.019	50.00	50.00	2.04
C44	1.033	50.00	50.00	2.07

*** Overall summary for all load cases - Usage = Maximum Stress / Allowable Stress
 Printed capacities do not include the strength factor entered for each loadcase.

Group Summary (Compression Portion):

Group Label	Group Desc.	Angle Type	Angle Size	Strength (ksi)	Steel Usage (%)	Max In Comp. Member	Comp. Force (kips)	Comp. Control Load Case	I/R Capacity (kips)	Comp. Shear Capacity (kips)	Comp. Conn. Bearing Capacity (kips)	RLX	RLY	RLZ	L/R Length Member (ft)	Curve No.	No. Bolts	Comp.
1	L1	SAE	2.5X2.5X0.1875	33.0	40.35	40.35	1Y	-7.122NESC Broke	17.649	27.200	24.469	0.500	0.500	0.500	117.68	9.708	3	2
2	L2	SAE	5X5X0.375	33.0	9.36	9.36	2XX	-9.974NESC Heavy	106.517	0.000	0.000	1.000	1.000	1.000	60.81	5.000	1	0
3	L3	SAE	5X5X0.375	33.0	14.96	14.96	3X	-15.940NESC Broke	106.517	0.000	0.000	1.000	1.000	1.000	60.61	5.000	1	0
4	L4	SAE	5X5X0.375	33.0	28.78	28.78	4P	-30.659NESC Broke	106.517	0.000	0.000	1.000	1.000	1.000	60.61	5.000	1	0
5	L5	SAE	5X5X0.375	33.0	24.75	24.75	5X	-26.358NESC Broke	106.517	136.000	244.687	1.000	1.000	1.000	60.61	5.000	1	0
6	L6	SAE	8X8X0.5	33.0	14.46	14.46	6X	-35.453NESC Broke	245.252	0.000	0.000	1.000	1.000	1.000	37.74	5.000	1	0
7	L7	SAE	8X8X0.5	33.0	23.49	23.49	7P	-57.615NESC Broke	245.252	0.000	0.000	1.000	1.000	1.000	37.74	5.000	1	0
8	L8	SAE	8X8X0.5	33.0	17.99	16.11	8X	-39.514NESC Broke	245.252	272.000	326.249	1.000	1.000	1.000	37.74	5.000	1	0
9	L9	SAE	8X8X0.5	50.0	14.14	14.14	9X	-44.203NESC Broke	312.662	0.000	0.000	1.000	1.000	1.000	38.54	5.107	1	0
10	L10	SAE	8X8X0.5	50.0	27.07	27.07	10P	-64.643NESC Broke	312.662	380.800	944.999	1.000	1.000	1.000	38.54	5.107	1	0
11	L11	SAE	8X8X0.5	50.0	25.31	25.31	11P	-79.126NESC Broke	312.662	380.800	944.999	1.000	1.000	1.000	38.54	5.107	1	0
12	L12	SAE	8X8X0.5	50.0	30.88	30.88	12P	-94.943NESC Broke	307.458	380.800	944.999	0.500	0.500	0.500	43.67	11.573	1	0
13	L13	SAE	8X8X0.5	50.0	31.58	31.58	13P	-96.407NESC Broke	305.312	380.800	944.999	0.250	0.250	0.250	45.62	24.177	1	0
14	PEAK	SAE	2.5X2.5X0.1875	33.0	29.98	29.98	14X	-84.871NESC Broke	16.686	0.000	0.000	1.000	1.000	1.000	124.50	10.271	5	2
15	TIBC	SAE	3X3X0.25	33.0	46.99	46.99	16X	-45.152NESC Broke	32.243	27.200	32.625	1.000	1.000	1.000	91.22	4.500	3	2
16	TIBC	SAE	3X3X0.25	33.0	40.98	40.98	20X	-11.146NESC Broke	40.528	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	2
17	ARMTT	SAE	4X4X0.25	33.0	18.91	18.91	22XY	-32.583NESC Extre	47.728	0.000	0.000	1.000	1.000	1.000	67.92	4.500	3	0
18	ARMTT	SAE	4X4X0.25	33.0	68.27	68.27	25P	-21.009NESC Extre	40.528	40.800	48.937	1.000	1.000	1.000	105.66	7.000	3	0
19	MTBC	SAE	4X4X0.25	33.0	44.02	44.02	40XY	-5.002NESC Extre	58.971	0.000	0.000	1.000	1.000	1.000	105.66	7.000	3	0
20	ARMTT	SAE	4X4X0.25	33.0	71.18	71.18	28XY	-41.976NESC Extre	58.971	54.400	81.562	1.000	1.000	1.000	88.27	4.500	3	0
21	BIBC	SAE	4X4X0.3125	33.0	51.27	51.27	30P	-27.578NESC Extre	53.785	40.800	81.562	1.000	1.000	1.000	91.02	6.000	3	0
22	ARMTT	SAE	4X4X0.3125	33.0	12.19	12.19	41XY	-4.974NESC Extre	50.000	40.800	61.172	1.000	1.000	1.000	106.19	7.000	3	0
23	ARMTT	SAE	4X4X0.3125	33.0	15.23	15.23	34X	-31.806NESC Extre	146.334	122.400	293.625	1.000	1.000	1.000	39.62	5.250	3	0
24	BIBC	SAE	6X6X0.5	33.0	40.77	40.77	58X	-4.1236NESC Extre	10.390	27.200	24.469	1.000	1.000	1.000	58.19	5.722	3	0
25	BIBC	SAE	4X4X0.375	33.0	40.02	40.02	75P	-23.139NESC Extre	57.974	68.000	122.344	1.000	1.000	1.000	152.28	5.000	3	0
26	W1	SAE	4X4X0.3125	33.0	70.50	70.50	67X	-19.596NESC Extre	56.998	54.400	81.562	1.000	1.000	1.000	121.28	5.000	6	2
27	W2	SAE	4X4X0.3125	33.0	74.75	74.75	69P	-32.943NESC Extre	46.740	54.400	81.562	1.000	1.000	1.000	77.23	5.091	3	5
28	W3	SAE	4X4X0.25	33.0	76.47	76.47	61X	-25.123NESC Extre	41.379	54.400	81.562	1.000	1.000	1.000	118.49	7.810	3	4
29	W4	SAE	3.5X3.5X0.25	33.0	72.86	72.86	63P	-24.283NESC Extre	32.946	40.800	48.937	1.000	1.000	1.000	101.54	6.727	3	4
30	W5	SAE	3X3X0.1875	33.0	79.53	79.53	55X	-12.148NESC Extre	15.275	27.200	48.937	1.000	1.000	1.000	127.69	7.810	3	3
31	W6	SAE	3X3X0.1875	33.0	52.88	52.88	64XY	-13.866NESC Extre	29.912	27.200	61.172	1.000	1.000	1.000	116.31	6.727	3	3
32	W7	SAE	3X2.5X0.25	33.0	63.17	63.17	65P	-26.138NESC Extre	26.226	27.200	61.172	1.000	1.000	1.000	137.05	6.727	3	2
33	W8	SAE	3.5X3.5X0.25	33.0	49.58	49.58	70XY	-19.158NESC Extre	41.379	54.400	65.250	1.000	1.000	1.000	137.05	6.727	3	2
34	W9	SAE	4X4X0.375	33.0	48.70	48.70	71Y	-29.572NESC Extre	38.640	40.800	65.250	1.000	1.000	1.000	113.64	5.000	3	2
35	W10	SAU	4X4X0.375	33.0	61.78	61.78	49P	-36.528NESC Extre	60.729	68.000	122.344	1.000	1.000	1.000	86.46	5.000	3	4
36	W11	SAE	4X4X0.25	33.0	74.06	74.06	47P	-30.644NESC Extre	59.125	68.000	122.344	1.000	1.000	1.000	102.44	6.727	3	3
37	W12	SAE	3X3X0.3125	33.0	65.19	65.19	45P	-19.498NESC Extre	41.379	54.400	65.250	1.000	1.000	1.000	107.68	7.071	3	5
38	W13	SAE	2 x 0.1875	33.0	44.07	0.00	44Y	0.000	29.912	40.800	61.172	1.000	1.000	1.000	101.54	6.727	3	4
39	DB1	DAS	3.5X3X0.25	33.0	79.38	79.38	51X	-38.886NESC Extre	0.072	27.200	61.172	1.000	1.000	1.000	137.05	6.727	6	3
40	DB2	DAS	4X3X0.4375	33.0	84.52	84.52	52P	-46.546NESC Extre	48.988	27.200	24.469	0.540	0.540	0.540	191.63	6.727	6	2
41	DB3	SAE	3X3X0.1875	33.0	9.75	9.75	53XY	-1.187NESC Extre	55.071	81.600	171.281	0.250	0.250	0.250	189.13	30.734	6	2
42	X1	SAU	7X4X0.4375	33.0	9.58	6.21	77P	-7.962NESC Extre	128.184	40.800	36.703	0.500	0.500	0.500	172.60	17.145	5	3
43	X2	SAE	2X2X0.1875	33.0	9.98	9.98	78X	-1.226NESC Extre	12.292	149.600	314.015	0.500	0.500	0.500	59.10	7.354	5	3
44	X3	SAE	2.5X2.5X0.25	33.0	30.65	30.65	80XY	-7.926NESC Extre	25.861	27.200	24.469	0.750	0.750	0.750	131.00	8.602	5	2
45	X4	SAE	3X3X0.3125	33.0	20.33	19.84	83XY	-8.097NESC Extre	25.861	27.200	24.469	0.750	0.500	0.500	105.12	8.602	2	2
46	X5	SAE	2.5X2.5X0.25	33.0	10.08	8.24	86X	-1.738NESC Extre	43.226	40.800	61.172	0.750	0.500	0.500	87.63	8.602	2	2
47	D1	SAE	3X3X0.1875	33.0	28.57	28.57	88P	-4.146NESC Extre	21.099	27.200	32.625	0.780	0.560	0.560	128.74	9.407	5	2
48	X14	SAU	2.5X2X0.1875	33.0	84.39	84.39	89P	-3.165NESC Extre	3.750	27.200	24.469	1.000	1.000	1.000	163.28	8.110	5	2
49	DB3	SAU	3X2X0.25	33.0	28.35	0.00	90Y	0.000	3.750	27.200	24.469	1.000	1.000	1.000	163.28	8.110	6	2
50	DB4	SAE	3X3X0.1875	33.0	21.13	1.04	91Y	-0.054NESC Extre	6.868	40.800	48.937	0.530	0.770	0.530	288.77	18.752	5	2
51	H1	SAE	2.5X2.5X0.1875	33.0	13.59	13.59	93P	-1.547NESC Extre	11.388	40.800	36.703	1.000	0.333	0.333	282.33	22.092	6	3
52	H2	SAE	2X2X0.1875	33.0	21.13	21.13	96X	-0.945NESC Extre	4.471	13.600	24.469	1.000	1.000	1.000	169.70	7.000	6	2
53	H3	SAE	2X2X0.1875	33.0	21.13	21.13	96X	-0.945NESC Extre	4.471	13.600	24.469	1.000	1.000	1.000	213.20	7.000	6	2

Group Label	Group Desc.	Angle Type	Steel Strength (ksi)	Max Usage %	Max In Control Tens. %	Tension Force (kips)	Control Case Capacity (kips)	Net Section Capacity (kips)	Shear Capacity (kips)	Conn. Bearing Capacity (kips)	Conn. Tens. Capacity (kips)	Conn. Rupture Capacity (kips)	Length Tens. Member (ft)	No. of Bolts	Hole Diameter (in)
57	H3	SAE 3.5X3.5X0.3125	33.0	8.07	8.07	97P	-3.216NESC Heavy	39.830	40.800	61.172	1.000	1.000	1.000	121.74	7.000
58	H16	SAU 3.5X3X0.25	33.0	3.69	1.56	98X	-0.516NESC Extre	33.037	40.800	48.937	1.000	1.000	1.000	102.97	5.415
59	H17	SAU 3.5X3X0.25	33.0	14.74	9.88	99X	-2.72NESC Extre	25.022	27.200	32.625	1.000	0.500	0.500	137.77	12.744
60	H18	SAE 3.5X3.5X0.25	33.0	46.39	46.39	100X	-7.594NESC Extre	16.369	40.800	48.937	1.000	0.500	0.500	188.06	17.062
61	H2	SAE 2X2X0.1875	33.0	3.12	3.12	101P	-0.139NESC Broke	4.471	13.600	12.234	1.000	1.000	1.000	213.20	7.000
62	X7	SAE 2X2X0.1875	33.0	29.78	29.78	118P	-3.070NESC Broke	10.309	13.600	12.234	0.750	0.500	0.500	140.40	9.220
63	H5	SAE 2.5X2.5X0.25	33.0	25.13	25.13	119X	-3.734NESC Extre	14.856	27.200	32.625	1.000	1.000	1.000	171.08	7.000
64	H8	SAE 2X2X0.25	33.0	13.06	13.06	120P	-3.278NESC Extre	16.440	13.600	16.312	0.750	0.500	0.500	127.70	8.322
65	H1	SAE 2.5X2.5X0.1875	33.0	24.10	24.10	121P	-1.488NESC Extre	11.388	27.200	24.469	1.000	1.000	1.000	169.70	7.000
66	H8	SAE 2X2X0.25	33.0	20.75	20.75	122P	-2.822NESC Broke	16.440	13.600	16.312	0.750	0.500	0.500	127.70	8.322
67	X6	SAE 2X2X0.25	33.0	75.78	75.78	107X	-8.835NESC Broke	11.659	13.600	16.312	0.750	0.500	0.500	151.91	9.899
68	H4	SAU 3.5X2.5X0.25	33.0	36.70	36.70	108X	-4.991NESC Broke	36.936	13.600	16.312	0.750	0.500	0.500	177.21	7.000
69	H2	SAE 2X2X0.1875	33.0	34.97	34.97	131P	-1.561NESC Broke	4.471	13.600	12.234	1.000	1.000	1.000	213.20	7.000
70	D2	SAE 2.5X2.5X0.1875	33.0	1.03	1.03	132AP	-0.052NESC Extre	5.1168	13.600	12.234	1.000	1.000	1.000	223.50	9.220
71	H2	SAE 2X2X0.1875	33.0	35.45	35.45	133X	-1.582NESC Broke	6.344	13.600	12.234	1.000	1.000	1.000	213.20	7.000
72	D2	SAE 2.5X2.5X0.1875	33.0	15.65	15.65	134BP	-0.034NESC Extre	6.344	13.600	12.234	1.000	1.000	1.000	213.20	7.000
73	H2	SAE 2X2X0.1875	33.0	79.28	79.28	129P	-3.545NESC Broke	4.471	13.600	12.234	1.000	1.000	1.000	213.20	7.000
74	D2	SAE 2.5X2.5X0.1875	33.0	19.22	19.22	143P	-0.098NESC Extre	6.344	13.600	12.234	1.000	1.000	1.000	201.74	8.322
75	H10	SAE 3.5X3.5X0.25	33.0	7.15	0.00	142P	-0.000	6.344	13.600	12.234	1.000	1.000	1.000	213.20	7.000
76	X10	SAE 2X2X0.1875	33.0	52.13	52.13	143P	-2.571NESC Broke	18.774	27.200	24.469	0.750	0.500	0.500	185.88	10.750
77	H9	SAE 2X2X0.1875	33.0	7.92	7.92	145X	-0.746NESC Heavy	9.420	27.200	24.469	0.750	0.500	0.500	228.84	15.027
78	H3	SAE 3X3X0.25	33.0	8.60	0.00	146BX	0.000	29.570	40.800	48.937	1.000	1.000	1.000	163.71	10.750
79	X9	SAU 2.5X1.5X0.25	33.0	16.08	16.08	147Y	-1.825NESC Broke	11.348	40.800	48.937	0.500	0.500	0.500	108.95	5.375
80	X9	SAU 2.5X1.5X0.25	33.0	16.50	16.50	148Y	-1.894NESC Broke	11.417	40.800	48.937	0.500	0.750	0.500	164.54	7.587
81	H8	SAE 2X2X0.25	33.0	8.57	0.00	149X	0.000	12.534	27.200	32.625	1.000	1.000	1.000	163.93	7.587
82	H15	SAE 3X3X0.1875	33.0	21.14	21.14	150P	-0.414NESC Broke	7.568	27.200	24.469	1.000	1.000	1.000	163.11	5.315
83	X12	SAE 2X2X0.1875	33.0	1.21	1.21	151Y	-0.684NESC Extre	3.237	13.600	12.234	0.750	0.500	0.500	255.02	12.666
84	H14	SAE 2X2X0.1875	33.0	3.57	3.57	152P	-0.666NESC Heavy	5.462	13.600	12.234	0.750	0.500	0.500	250.54	16.452
85	H13	SAE 3X3X0.25	33.0	2.81	1.67	153X	-0.685NESC Heavy	19.149	27.200	32.625	1.000	0.500	0.500	192.88	12.666
86	X11	SAE 2X2X0.1875	33.0	2.87	0.10	154Y	-0.075NESC Broke	4.513	13.600	12.234	0.750	0.500	0.500	163.43	12.666
87	H19	SAE 3X3X0.1875	33.0	2.87	0.10	155P	-0.010NESC Heavy	10.549	13.600	12.234	0.750	0.500	0.500	212.19	13.934
88	X13	SAE 2X2X0.1875	33.0	92.14	92.14	156XY	-1.378NESC Broke	1.496	13.600	12.234	0.500	0.500	0.500	171.97	17.082

Group Summary (Tension Portion) :

Group Label	Group Desc.	Angle Type	Steel Strength (ksi)	Max Usage %	Max In Control Tens. %	Tension Force (kips)	Control Case Capacity (kips)	Net Section Capacity (kips)	Shear Capacity (kips)	Conn. Bearing Capacity (kips)	Conn. Tens. Capacity (kips)	Conn. Rupture Capacity (kips)	Length Tens. Member (ft)	No. of Bolts	Hole Diameter (in)
1	L1	SAE 2.5X2.5X0.1875	33.0	40.35	17.56	1X	3.849NESC Broke	21.917	27.200	24.469	0.000	0.000	9.708	2	1.000
2	L2	SAE 5X5X0.375	33.0	9.36	5.48	2P	5.483NESC Extre	100.072	0.000	0.000	0.000	0.000	5.000	0	1.760
3	L3	SAE 5X5X0.375	33.0	14.96	4.10	3P	3.399NESC Extre	82.747	0.000	0.000	0.000	0.000	5.000	0	3.360
4	L4	SAE 5X5X0.375	33.0	28.78	19.33	4X	15.993NESC Extre	82.747	0.000	0.000	0.000	0.000	5.000	0	3.360
5	L5	SAE 5X5X0.375	33.0	24.75	4.10	5X	3.111NESC Broke	75.817	136.000	244.687	0.000	0.000	5.000	10	4.000
6	L6	SAE 8X8X0.5	33.0	14.46	4.53	6X	10.500NESC Broke	231.928	0.000	0.000	0.000	0.000	5.000	0	1.650
7	L7	SAE 8X8X0.5	33.0	23.49	21.20	7X	49.175NESC Broke	231.928	0.000	0.000	0.000	0.000	5.000	0	1.650
8	L8	SAE 8X8X0.5	33.0	17.99	17.99	8X	35.614NESC Broke	198.000	272.000	326.249	0.000	0.000	5.000	10	4.000
9	L9	SAE 8X8X0.5	50.0	27.07	24.02	10X	38.870NESC Broke	355.562	0.000	0.000	0.000	0.000	5.107	0	1.460
10	L10	SAE 8X8X0.5	50.0	25.31	21.05	11X	72.048NESC Broke	300.000	380.800	944.999	0.000	0.000	5.107	28	4.000
11	L11	SAE 8X8X0.5	50.0	30.88	24.16	12X	63.140NESC Broke	300.000	0.000	0.000	0.000	0.000	5.107	0	4.000
12	L12	SAE 8X8X0.5	50.0	31.58	28.29	13X	72.472NESC Broke	300.000	380.800	944.999	0.000	0.000	5.107	28	4.000
13	L13	SAE 8X8X0.5	50.0	29.98	29.98	14Y	66.855NESC Broke	300.000	380.800	944.999	0.000	0.000	24.177	28	4.000
14	PEAK	SAE 2.5X2.5X0.1875	33.0	46.99	46.05	17Y	12.527NESC Extre	21.917	27.200	24.469	0.000	0.000	10.271	2	1.000
15	TTC	SAE 3X3X0.25	33.0	40.98	37.08	19X	13.449NESC Broke	36.271	27.200	32.625	0.000	0.000	4.500	2	1.000
16	TTC	SAE 4X4X0.25	33.0	18.91	6.99	39Y	1.902NESC Broke	36.271	0.000	0.000	0.000	0.000	4.500	2	1.000
17	ARMTT	SAE 4X4X0.25	33.0	68.27	64.41	22P	32.930NESC Extre	51.121	27.200	32.625	0.000	0.000	7.000	0	1.000
18	MTC	SAE 4X4X0.25	33.0	41.18	41.18	25X	21.053NESC Extre	51.121	0.000	0.000	0.000	0.000	4.500	2	1.000
19	MTC	SAE 4X4X0.25	33.0	12.34	4.28	40Y	1.747NESC Extre	49.952	40.800	48.937	0.000	0.000	4.500	0	1.000
20	ARMTT	SAE 4X4X0.25	33.0	71.18	70.67	28P	44.635NESC Broke	63.159	0.000	0.000	0.000	0.000	7.000	3	1.000
21	BTC	SAE 4X4X0.3125	33.0	51.27	41.39	30X	22.319NESC Extre	55.038	40.800	48.937	0.000	0.000	4.500	0	1.000
22	BTC	SAE 4X4X0.3125	33.0	12.19	4.66	41Y	1.900NESC Extre	61.697	40.800	81.562	0.000	0.000	6.000	0	1.180
23	ARMTT	SAE 8X8X0.5	33.0	15.23	14.26	34P	30.967NESC Broke	217.181	0.000	0.000	0.000	0.000	7.000	3	1.000
24	BTTC	SAE 6X6X0.5	33.0	30.95	30.95	38X	37.889NESC Broke	131.794	122.400	0.000	0.000	0.000	5.250	9	1.000
25	BTTC	SAE 2X2X0.1875	33.0	40.77	33.29	58X	5.398NESC Broke	16.214	27.200	24.469	0.000	0.000	7.222	2	1.000
26	W1	SAE 4X4X0.375	33.0	40.02	35.77	73P	24.321NESC Broke	70.324	68.000	122.344	0.000	0.000	5.000	2	1.000
27	W2	SAE 4X4X0.375	33.0	40.12	40.12	76P	21.826NESC Broke	63.159	54.400	81.562	0.000	0.000	7.313	4	1.000
28	W3	SAE 4X4X0.3125	33.0	40.12	40.12	76P	21.826NESC Broke	63.159	54.400	81.562	0.000	0.000	5.091	5	1.000

W4	SAE	4X4X0.3125	33.0	70.50	62.04	67P	33.749NESC Broke	59.748	54.400	81.562	0.000	7.810	4	1.420	0.875
29	SAE	4X4X0.25	33.0	76.75	62.48	69XY	25.045NESC Extre	49.627	54.400	65.250	0.000	6.727	4	1.230	0.875
30	SAE	4X3.5X0.25	33.0	74.47	63.53	61P	25.918NESC Broke	44.531	40.800	48.937	0.000	7.810	3	1.420	0.875
31	SAE	3X3.5X0.25	33.0	72.86	48.32	63XY	19.715NESC Extre	43.696	40.800	48.937	0.000	6.727	3	1.000	0.875
32	SAE	3X3X0.1875	33.0	79.53	51.92	55P	12.703NESC Broke	27.500	27.200	24.469	0.000	7.810	2	1.000	0.875
33	SAE	3X3X0.3125	33.0	53.04	40.82	59X	16.655NESC Broke	44.745	40.800	51.172	0.000	6.727	3	1.000	0.875
34	SAE	3X2.5X0.25	33.0	52.88	48.71	64P	13.249NESC Broke	32.410	27.200	32.625	0.000	5.000	2	1.000	0.875
35	SAE	4X4X0.25	33.0	63.17	57.90	65X	27.570NESC Extre	47.613	54.400	65.250	0.000	6.727	3	1.000	0.875
36	SAE	3.5X3.5X0.25	33.0	49.58	46.93	70Y	19.147NESC Extre	43.696	40.800	48.937	0.000	5.000	4	1.540	0.875
37	SAE	4X4X0.375	33.0	48.70	45.44	71XY	30.588NESC Extre	66.816	68.000	122.344	0.000	6.727	3	1.000	0.875
38	SAE	4X4X0.375	33.0	61.78	48.49	50P	32.975NESC Broke	75.197	68.000	122.344	0.000	6.727	5	1.860	0.875
39	SAE	4X4X0.25	33.0	74.06	60.81	47X	28.951NESC Extre	47.613	54.400	65.250	0.000	6.727	5	1.000	0.875
40	SAE	3X3X0.3125	33.0	65.19	47.26	45XY	19.282NESC Extre	44.745	40.800	61.172	0.000	6.727	4	1.540	0.875
41	BAR	2 x 0.1875	33.0	44.07	44.07	43P	2.761NESC Heavy	6.265	27.200	24.469	0.000	6.727	3	1.000	0.875
42	DAS	3X3X0.25	33.0	79.38	48.74	51V	26.514NESC Extre	72.542	54.400	65.250	0.000	8.602	2	2.000	0.875
43	DAS	4X3X0.4375	33.0	84.52	47.99	52XY	39.158NESC Extre	121.751	81.600	171.281	0.000	19.905	2	2.000	0.875
44	HB1	3X3X0.1875	33.0	9.75	5.64	53Y	1.552NESC Extre	27.500	40.800	36.703	0.000	30.734	3	2.000	0.875
45	HB1	7X4X0.4375	33.0	9.58	9.58	77XY	9.878NESC Extre	103.105	149.600	314.015	0.000	17.145	3	2.000	0.875
46	X1	2X2X0.1875	33.0	9.98	6.37	79P	1.033NESC Broke	16.214	27.200	24.469	0.000	7.354	11	3.000	0.875
47	X2	2.5X2.5X0.25	33.0	30.65	29.54	81X	8.034NESC Broke	28.1846	27.200	32.625	0.000	8.602	2	1.000	0.875
48	X3	3X3X0.3125	33.0	20.33	20.33	84X	8.296NESC Broke	46.745	40.800	61.172	0.000	8.602	2	1.000	0.875
49	X4	2.5X2.5X0.25	33.0	10.08	10.08	86Y	2.742NESC Broke	28.846	27.200	32.625	0.000	9.407	3	1.000	0.875
50	X5	3X3X0.1875	33.0	28.57	12.22	88XY	2.990NESC Broke	27.500	27.200	24.469	0.000	8.110	2	1.000	0.875
51	D1	SAU	33.0	84.39	11.57	89X	8.177NESC Extre	19.184	27.200	24.469	0.000	18.752	2	1.000	0.875
52	X14	SAU	33.0	28.35	28.35	90XY	5.810NESC Extre	28.846	40.800	48.937	0.000	10.403	3	1.000	0.875
53	DB3	SAU	33.0	21.13	21.13	91X	2.096NESC Extre	27.500	40.800	36.703	0.000	22.082	3	1.000	0.875
54	DB4	SAE	33.0	21.13	14.66	96P	1.794NESC Heavy	21.917	27.200	24.469	0.000	7.000	2	1.000	0.875
55	H1	SAE	33.0	8.07	3.63	97X	1.463NESC Extre	33.952	40.800	61.172	0.000	7.000	1	1.000	0.875
56	H2	SAE	33.0	3.69	3.69	98P	1.469NESC Broke	59.835	40.800	48.937	0.000	5.415	3	1.000	0.875
57	H3	SAU	33.0	14.74	14.74	99P	4.010NESC Extre	39.835	27.200	32.625	0.000	12.744	3	1.000	0.875
58	H16	SAU	33.0	46.39	0.00	100X	0.000	43.696	40.800	48.937	0.000	17.082	3	1.000	0.875
59	H17	SAU	33.0	3.12	1.75	117P	0.214NESC Broke	16.214	13.600	12.234	0.000	7.000	1	1.000	0.875
60	H18	SAE	33.0	29.78	24.79	110X	3.033NESC Broke	16.214	13.600	12.234	0.000	9.220	1	1.000	0.875
61	H2	SAE	33.0	25.13	14.48	119P	3.938NESC Extre	28.846	27.200	32.625	0.000	7.000	2	1.000	0.875
62	H3	SAE	33.0	24.10	22.48	120X	3.057NESC Broke	21.421	13.600	16.312	0.000	8.322	2	1.000	0.875
63	H4	SAU	33.0	13.06	7.71	121X	1.689NESC Heavy	21.917	27.200	24.469	0.000	7.000	2	1.000	0.875
64	H5	SAE	33.0	20.75	13.02	122X	1.771NESC Extre	21.421	13.600	16.312	0.000	8.322	1	1.000	0.875
65	H6	SAE	33.0	75.78	51.69	107XY	7.029NESC Broke	21.421	13.600	16.312	0.000	9.899	1	1.000	0.875
66	H7	SAU	33.0	36.70	4.05	124X	0.551NESC Heavy	36.271	13.600	16.312	0.000	7.000	1	1.000	0.875
67	H8	SAU	33.0	17.21	17.21	132BP	0.000NESC Extre	16.214	13.600	12.234	0.000	7.000	1	1.000	0.875
68	H9	SAU	33.0	15.65	15.65	139X	0.000	16.214	13.600	12.234	0.000	9.220	1	1.000	0.875
69	H10	SAU	33.0	35.45	15.65	134AP	1.915NESC Broke	21.917	13.600	12.234	0.000	7.000	1	1.000	0.875
70	H11	SAU	33.0	79.28	13.01	129X	1.592NESC Heavy	16.214	13.600	12.234	0.000	8.322	1	1.000	0.875
71	H12	SAE	33.0	15.52	15.52	136BP	1.899NESC Broke	21.917	13.600	12.234	0.000	7.000	1	1.000	0.875
72	H13	SAE	33.0	7.15	7.15	143P	1.944NESC Heavy	43.696	27.200	32.625	0.000	8.322	1	1.000	0.875
73	H14	SAE	33.0	52.13	1.16	144P	0.189NESC Broke	16.214	27.200	24.469	0.000	10.750	2	1.000	0.875
74	H15	SAE	33.0	7.92	0.00	145X	0.000	16.214	27.200	24.469	0.000	15.027	2	1.000	0.875
75	H16	SAE	33.0	8.60	8.60	146X	3.118NESC Broke	36.271	40.800	48.937	0.000	10.750	2	1.000	0.875
76	H17	SAU	33.0	16.08	0.00	147Y	0.000	21.421	40.800	48.937	0.000	5.375	3	1.000	0.875
77	H18	SAU	33.0	16.50	0.00	148Y	0.000	21.421	40.800	48.937	0.000	7.587	3	1.000	0.875
78	H19	SAU	33.0	5.48	0.00	149P	1.836NESC Broke	21.421	40.800	48.937	0.000	5.315	3	1.000	0.875
79	H20	SAE	33.0	21.14	7.77	153XY	0.000	27.500	27.200	32.625	0.000	7.000	2	1.000	0.875
80	H21	SAE	33.0	1.21	0.00	152X	0.991NESC Broke	16.214	13.600	12.234	0.000	12.666	2	1.000	0.875
81	H22	SAE	33.0	3.57	0.09	153P	0.024NESC Broke	36.271	13.600	12.234	0.000	16.452	2	1.000	0.875
82	H23	SAE	33.0	2.81	2.81	154P	0.344NESC Heavy	16.214	13.600	12.234	0.000	12.666	1	1.000	0.875
83	H24	SAE	33.0	2.87	2.87	155P	0.351NESC Extre	16.214	13.600	12.234	0.000	13.934	2	1.000	0.875
84	H25	SAE	33.0	92.14	6.16	156Y	0.754NESC Broke	16.214	13.600	12.234	0.000	17.082	1	1.000	0.875
85	H26	SAE	33.0	92.14	6.16	156Y	0.754NESC Broke	16.214	13.600	12.234	0.000	24.202	1	1.000	0.875

*** Maximum Stress Summary for Each Load Case

Summary of Maximum Usages by Load Case:

Load Case Maximum Element Element

Usage %	Label	Type
83.15	89P	Angle
84.39	89P	Angle
92.14	156XY	Angle

Summary of Insulator Usages:

Insulator Label	Insulator Type	Insulator Maximum Usage %	Load Case	Maximum Weight (lbs)
C1	Clamp	12.00	NESC Heavy	0.0
C2	Clamp	8.27	NESC Heavy	0.0
C3	Clamp	7.43	NESC Heavy	0.0
C4	Clamp	7.43	NESC Heavy	0.0
C5	Clamp	7.43	NESC Heavy	0.0
C6	Clamp	23.70	NESC Broken Wire	0.0
C7	Clamp	7.43	NESC Heavy	0.0
C8	Clamp	7.43	NESC Heavy	0.0
C9	Clamp	7.43	NESC Heavy	0.0
C10	Clamp	7.43	NESC Heavy	0.0
C11	Clamp	7.43	NESC Heavy	0.0
C12	Clamp	7.43	NESC Heavy	0.0
C13	Clamp	7.43	NESC Heavy	0.0
C14	Clamp	7.43	NESC Heavy	0.0
C15	Clamp	7.46	NESC Heavy	0.0
C16	Clamp	7.46	NESC Heavy	0.0
C17	Clamp	7.46	NESC Heavy	0.0
C18	Clamp	7.46	NESC Heavy	0.0
C19	Clamp	7.48	NESC Heavy	0.0
C20	Clamp	7.48	NESC Heavy	0.0
C21	Clamp	7.48	NESC Heavy	0.0
C22	Clamp	7.48	NESC Heavy	0.0
C23	Clamp	7.49	NESC Heavy	0.0
C24	Clamp	7.49	NESC Heavy	0.0
C25	Clamp	7.49	NESC Heavy	0.0
C26	Clamp	7.49	NESC Heavy	0.0
C27	Clamp	9.20	NESC Extreme	0.0
C28	Clamp	1.39	NESC Heavy	0.0
C29	Clamp	2.68	NESC Heavy	0.0
C30	Clamp	1.86	NESC Heavy	0.0
C31	Clamp	2.20	NESC Heavy	0.0
C32	Clamp	3.99	NESC Heavy	0.0
C33	Clamp	2.50	NESC Heavy	0.0
C34	Clamp	10.21	NESC Extreme	0.0
C35	Clamp	1.47	NESC Extreme	0.0
C36	Clamp	2.69	NESC Heavy	0.0
C37	Clamp	1.86	NESC Heavy	0.0
C38	Clamp	2.20	NESC Heavy	0.0
C39	Clamp	3.99	NESC Heavy	0.0
C40	Clamp	2.50	NESC Heavy	0.0
C41	Clamp	8.48	NESC Heavy	0.0
C42	Clamp	9.48	NESC Extreme	0.0
C43	Clamp	2.34	NESC Extreme	0.0
C44	Clamp	2.71	NESC Extreme	0.0

Loads At Insulator Attachments For All Load Cases:

Case	Insulator Label	Insulator Type	Structure Attach Label	Structure Attach Load X (kips)	Structure Attach Load Y (kips)	Structure Attach Load Z (kips)
NESC Heavy	C1	Clamp	1P	0.000	5.742	1.745
NESC Heavy	C2	Clamp	1X	0.000	3.900	1.376
NESC Heavy	C3	Clamp	15P	0.000	3.354	1.594
NESC Heavy	C4	Clamp	15X	0.000	3.354	1.594

NESC Heavy	15XY	0.000	3.354	1.594	3.714
NESC Heavy	15Y	0.000	3.354	1.594	3.714
NESC Heavy	16P	0.000	3.354	1.594	3.714
NESC Heavy	16X	0.000	3.354	1.594	3.714
NESC Heavy	16XY	0.000	3.354	1.594	3.714
NESC Heavy	17P	0.000	3.354	1.594	3.714
NESC Heavy	17X	0.000	3.354	1.603	3.717
NESC Heavy	17XY	0.000	3.354	1.603	3.717
NESC Heavy	22P	0.000	3.354	1.603	3.717
NESC Heavy	22X	0.000	3.363	1.616	3.731
NESC Heavy	22XY	0.000	3.363	1.616	3.731
NESC Heavy	28P	0.000	3.363	1.634	3.731
NESC Heavy	28XY	0.000	3.363	1.634	3.739
NESC Heavy	28Y	0.000	3.363	1.634	3.739
NESC Heavy	34P	0.000	3.363	1.647	3.739
NESC Heavy	34X	0.000	3.363	1.647	3.745
NESC Heavy	34XY	0.000	3.363	1.647	3.745
NESC Heavy	3Y	0.000	1.226	3.815	4.007
NESC Heavy	5Y	0.000	0.245	0.648	0.693
NESC Heavy	7Y	0.000	-0.097	1.338	1.342
NESC Heavy	9Y	0.000	0.278	0.888	0.930
NESC Heavy	11Y	0.000	0.304	1.055	1.098
NESC Heavy	13Y	0.000	0.620	1.899	1.997
NESC Heavy	14XY	0.000	0.284	1.217	1.250
NESC Heavy	3Y	0.000	1.367	3.471	3.642
NESC Heavy	5Y	0.000	0.261	0.577	0.726
NESC Heavy	7Y	0.000	-0.156	1.338	1.347
NESC Heavy	9Y	0.000	0.278	0.888	0.930
NESC Heavy	11Y	0.000	0.304	1.055	1.098
NESC Heavy	13Y	0.000	0.620	1.899	1.997
NESC Heavy	14Y	0.000	0.284	1.217	1.250
NESC Heavy	3X	0.000	1.102	3.471	3.642
NESC Heavy	3P	0.000	1.243	3.736	3.937
NESC Heavy	7X	0.000	-0.221	0.994	1.019
NESC Heavy	7P	0.000	-0.280	0.994	1.033
NESC Extreme	1P	0.000	5.144	0.494	5.168
NESC Extreme	1X	0.000	2.475	0.403	2.508
NESC Extreme	15P	0.000	2.846	0.636	2.916
NESC Extreme	15X	0.000	2.846	0.636	2.916
NESC Extreme	15XY	0.000	2.846	0.636	2.916
NESC Extreme	15Y	0.000	2.846	0.636	2.916
NESC Extreme	16P	0.000	2.846	0.636	2.916
NESC Extreme	16X	0.000	2.846	0.636	2.916
NESC Extreme	16XY	0.000	2.846	0.636	2.916
NESC Extreme	16Y	0.000	2.846	0.636	2.916
NESC Extreme	17X	0.000	2.846	0.642	2.918
NESC Extreme	17Y	0.000	2.846	0.642	2.918
NESC Extreme	22P	0.000	2.846	0.642	2.918
NESC Extreme	22X	0.000	2.861	0.646	2.933
NESC Extreme	22XY	0.000	2.861	0.646	2.933
NESC Extreme	22Y	0.000	2.861	0.646	2.933
NESC Extreme	28P	0.000	2.861	0.646	2.933
NESC Extreme	28X	0.000	2.861	0.655	2.935
NESC Extreme	28XY	0.000	2.861	0.655	2.935
NESC Extreme	28Y	0.000	2.861	0.655	2.935
NESC Extreme	34P	0.000	2.861	0.664	2.937
NESC Extreme	34X	0.000	2.861	0.664	2.937
NESC Extreme	34XY	0.000	2.861	0.664	2.937
NESC Extreme	34Y	0.000	2.861	0.664	2.937
NESC Extreme	3XY	0.000	4.206	1.859	4.598
NESC Extreme	5XY	0.000	0.649	0.234	0.650
NESC Extreme	7XY	0.000	-0.663	0.647	0.926

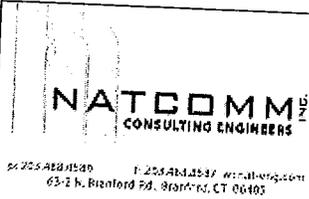
Case	Component	9XY	0.000	0.746	0.373	0.834
C30	Clamp	11XY	0.000	0.857	0.423	0.956
C31	Clamp	13XY	0.000	1.689	0.819	1.877
C32	Clamp	14XY	0.000	0.756	0.694	1.026
C33	Clamp	3Y	0.000	4.705	1.973	5.103
C34	Clamp	5Y	0.000	0.687	0.256	0.733
C35	Clamp	7Y	0.000	-0.875	0.655	1.093
C36	Clamp	9Y	0.000	0.746	0.381	0.838
C37	Clamp	11Y	0.000	0.857	0.434	0.960
C38	Clamp	13Y	0.000	1.689	0.834	1.884
C39	Clamp	14Y	0.000	0.756	0.694	1.026
C40	Clamp	3X	0.000	3.848	1.780	4.240
C41	Clamp	3P	0.000	4.348	1.886	4.740
C42	Clamp	7X	0.000	-1.021	0.568	1.168
C43	Clamp	7P	0.000	1.233	0.568	1.357
C44	Clamp	1P	0.000	5.742	1.745	6.001
C1	Clamp	1X	0.000	3.900	1.376	4.136
C2	Clamp	15P	0.000	3.354	1.594	3.714
C3	Clamp	15X	0.000	0.045	0.132	0.140
C4	Clamp	15XY	11.252	3.354	1.594	11.849
C5	Clamp	15Y	0.000	3.354	1.594	3.714
C6	Clamp	16P	0.000	3.354	1.594	3.714
C7	Clamp	16X	0.000	3.354	1.594	3.714
C8	Clamp	16XY	0.000	3.354	1.594	3.714
C9	Clamp	16Y	0.000	3.354	1.594	3.714
C10	Clamp	17P	0.000	3.354	1.594	3.714
C11	Clamp	17X	0.000	3.354	1.594	3.714
C12	Clamp	17XY	0.000	3.354	1.603	3.717
C13	Clamp	17Y	0.000	3.354	1.603	3.717
C14	Clamp	22P	0.000	3.363	1.616	3.731
C15	Clamp	22X	0.000	3.363	1.616	3.731
C16	Clamp	22XY	0.000	3.363	1.616	3.731
C17	Clamp	22Y	0.000	3.363	1.616	3.731
C18	Clamp	28P	0.000	3.363	1.634	3.731
C19	Clamp	28X	0.000	3.363	1.634	3.731
C20	Clamp	28XY	0.000	3.363	1.634	3.739
C21	Clamp	28Y	0.000	3.363	1.634	3.739
C22	Clamp	34P	0.000	3.363	1.647	3.739
C23	Clamp	34X	0.000	3.363	1.647	3.739
C24	Clamp	34XY	0.000	3.363	1.647	3.745
C25	Clamp	34Y	0.000	3.363	1.647	3.745
C26	Clamp	3XV	0.000	3.363	1.647	3.745
C27	Clamp	5XY	0.000	1.226	0.815	4.007
C28	Clamp	7XY	0.000	-0.097	0.648	0.693
C29	Clamp	9XY	0.000	0.278	1.338	1.342
C30	Clamp	11XY	0.000	0.304	1.055	1.098
C31	Clamp	13XY	0.000	0.620	1.899	1.997
C32	Clamp	14XY	0.000	0.284	1.217	1.250
C33	Clamp	3Y	0.000	1.367	4.080	4.303
C34	Clamp	5Y	0.000	0.261	0.677	0.726
C35	Clamp	7Y	0.000	-0.156	1.338	1.347
C36	Clamp	9Y	0.000	0.278	0.888	0.930
C37	Clamp	11Y	0.000	0.304	1.055	1.098
C38	Clamp	13Y	0.000	0.620	1.899	1.997
C39	Clamp	14Y	0.000	0.284	1.217	1.250
C40	Clamp	3X	0.000	1.102	3.471	3.642
C41	Clamp	3P	0.000	1.243	3.736	3.937
C42	Clamp	7X	0.000	-0.221	0.994	1.019
C43	Clamp	7P	0.000	-0.280	0.994	1.033
C44	Clamp	7P	0.000	-0.280	0.994	1.033

Overturning Moments For User Input Concentrated Loads:
 Moments are static equivalents based on central axis of 0.0.

Load Case	Total Tran. Load (kips)	Total Long. Load (kips)	Total Overturning Moment (ft-k)
C30	0.000	0.000	0.000
C31	0.000	0.000	0.000
C32	0.000	0.000	0.000
C33	0.000	0.000	0.000
C34	0.000	0.000	0.000
C35	0.000	0.000	0.000
C36	0.000	0.000	0.000
C37	0.000	0.000	0.000
C38	0.000	0.000	0.000
C39	0.000	0.000	0.000
C40	0.000	0.000	0.000
C41	0.000	0.000	0.000
C42	0.000	0.000	0.000
C43	0.000	0.000	0.000
C44	0.000	0.000	0.000

NESC Heavy	93.387	0.000	58.365	6398.572	-26.972
NESC Extreme	87.700	0.000	23.683	6087.354	-6.499
NESC Broken Wire	90.078	11.252	56.903	6166.016	868.071
*** Weight of structure (lbs):					
Weight Of Angles*Section DLF:			31305.4		
Total:			31305.4		

*** End of Report



Subject:

Foundation Analysis CL&P Tower # 1102

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO5

Foundation Analysis

Input Data:

Max. Reactions at Tower Leg:

Shear (Compression Leg) =	Shear _{cl} := 43.62-kips	(User Input)
Shear (Uplift Leg) =	Shear _{ul} := 22.91-kips	(User Input)
Compression =	Comp := 129.65-kips	(User Input)
Uplift =	Uplift := 92.79-kips	(User Input)

Tower Properties:

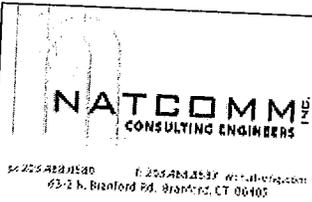
Tower Height =	H _t := 94-ft	(User Input)
----------------	-------------------------	--------------

Foundation Properties:

Pier Height =	P _H := 9.5-ft	(User Input)
Pier Width Top =	P _{w1} := 3-ft	(User Input)
Pier Width Bottom =	P _{w2} := 6-ft	(User Input)
Pier Projection Above Grade =	P _p := 0.5-ft	(User Input)
Pad Width =	Pd _w := 11-ft	(User Input)
Pad Thickness =	Pd _t := 3-ft	(User Input)
Depth to Neglect =	n := 1-ft	(User Input)

Subgrade Properties:

Concrete Unit Weight =	γ _c := 150-pcf	(User Input)
Water Unit Weight =	γ _w := 62.4-pcf	(User Input)
Soil Unit Weight =	γ _s := 90-pcf	(User Input)
Uplift Angle =	ψ := 30.0-deg	(User Input)
Soil Bearing Capacity =	BC _{soil} := 3500-psf	(User Input)



Subject:

Foundation Analysis CL&P Tower # 1102

Location:

Norwalk, CT

Rev. 1: 7/8/09

Prepared by: T.J.L. Checked by: C.F.C.
Job No. 08174.CO5

Calculated Data:

Coefficient of Lateral Soil Pressure =

$$K_p := \frac{1 + \sin(\psi)}{1 - \sin(\psi)} = 3$$

Passive Pressure =

$$P_{pn} := K_p \cdot \gamma_s \cdot n = 0.27 \cdot \text{ksf}$$

$$P_{pt} := K_p \cdot \gamma_s \cdot (P_H) = 2.565 \cdot \text{ksf}$$

$$P_{top} := \text{if}[n < (P_H), P_{pt}, P_{pn}] = 2.565 \cdot \text{ksf}$$

$$P_{bot} := K_p \cdot \gamma_s \cdot (P_H + P_d) = 3.375 \cdot \text{ksf}$$

$$P_{ave, pad} := \frac{P_{top} + P_{bot}}{2} = 2.97 \cdot \text{ksf}$$

$$T_p := \text{if}[n < (P_H), P_{dt}, (P_H + P_{dt} - n)] = 3 \text{ ft}$$

Pad Area =

$$A_{pad} := P_{d_w} \cdot T_p = 33 \text{ ft}^2$$

Ultimate Shear Pad =

$$S_{u, pad} := P_{ave, pad} \cdot A_{pad} = 98.01 \cdot \text{kip}$$

$$P_{ave, pier} := \frac{P_{pn} + P_{pt}}{2} = 1.418 \cdot \text{ksf}$$

Pier Area =

$$A_{pier} := P_{w1} \cdot (P_H - n) = 25.5 \text{ ft}^2$$

Ultimate Shear Pier =

$$S_{u, pier} := P_{ave, pier} \cdot A_{pier} = 36.146 \cdot \text{kip}$$

Cross Sectional Area of Pad =

$$A_{pier} := P_{d_w}^2 = 121 \text{ ft}^2$$

Resisting Pyramid Base 1 =

$$B_1 := P_{d_w}^2 = 121 \text{ ft}^2$$

Resisting Pyramid Base 2 =

$$B_2 := [P_{d_w} + 2 \cdot \tan(\psi) \cdot (P_H - P_P)]^2 = 457.6 \text{ ft}^2$$

Volume of the Concrete Pad =

$$V_{pad} := P_{d_w}^2 \cdot P_{dt} = 363 \cdot \text{ft}^3$$

Volume of the Concrete Pier =

$$V_{pier} := \frac{P_H}{3} \cdot (P_{w1}^2 + P_{w2}^2 + \sqrt{P_{w1}^2 \cdot P_{w2}^2}) = 199.5 \cdot \text{ft}^3$$

Total Volume of Concrete =

$$V_{Conc} := V_{pad} + V_{pier} = 562.5 \cdot \text{ft}^3$$

Volume of Soil =

$$V_{Soil} := \left[\frac{(P_H - P_P)}{3} \cdot (B_1 + B_2 + \sqrt{B_1 \cdot B_2}) \right] - V_{pier} = 2242.3 \cdot \text{ft}^3$$

Mass of Concrete =

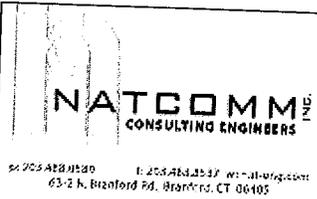
$$\text{Mass}_{Conc} := V_{Conc} \cdot \gamma_c = 84.4 \cdot \text{kips}$$

Mass of Soil =

$$\text{Mass}_{Soil} := V_{Soil} \cdot \gamma_s = 201.8 \cdot \text{kips}$$

Total Mass =

$$\text{Mass}_{Tot} := \text{Mass}_{Soil} + \text{Mass}_{Conc} = 286.2 \cdot \text{kips}$$



Subject: Foundation Analysis CL&P Tower # 1102
 Location: Norwalk, CT
 Rev. 1: 7/8/09
 Prepared by: T.J.L. Checked by: C.F.C.
 Job No. 08174.CO5

Check Uplift:

Required Factor of Safety =

$$F_S := 1.5$$

$$\text{ActualFS} := \frac{\text{MassTot}}{\text{Uplift}} = 3.1$$

$$\text{Uplift_Check} := \text{if} \left(\frac{\text{MassTot}}{\text{Uplift}} \geq F_S, \text{"OK"}, \text{"Overstressed"} \right)$$

Uplift_Check = "OK"

Check Bearing:

$$\text{Bearing} := \frac{\text{Comp} + \text{MassConc}}{A_{\text{pier}}} = 1.77 \cdot \text{ksf}$$

$$\text{Bearing_Check} := \text{if} (\text{Bearing} \leq \text{BC}_{\text{soil}}, \text{"OK"}, \text{"No Good"})$$

Bearing_Check = "OK"

Check Overturning (Compression Legs):

Overturning Moment =

$$\text{OM} := (\text{Shear}_{\text{cl}} + \text{Shear}_{\text{ul}}) \cdot (P_H + P_d_t) = 831.63 \cdot \text{kip}\cdot\text{ft}$$

Resisting Moment =

$$\text{RM} := \left[(\text{Comp} + \text{MassConc}) \cdot \frac{P_d_w}{2} \right] + S_{u,\text{pad}} \cdot \frac{P_d_t}{3} + (S_{u,\text{pier}}) \left[P_d_t + \frac{(P_H - n)}{3} \right] = 1486 \cdot \text{kip}\cdot\text{ft}$$

$$\text{Overturning_Check} := \text{if} \left(\frac{\text{RM}}{\text{OM}} \geq F_S, \text{"OK"}, \text{"No Good"} \right)$$

Overturning_Check = "OK"

From: "Fiedler, Hans" <Hans.Fiedler@T-Mobile.com>
To: "Tim Lynn" <TLynn@nat-eng.com>, <grayrd@nu.com>, <Tim.Burks@SAI-Comm.com>
Date: 7/1/2009 9:58:17 AM
Subject: RE: CL&P structure #1102, T-Mobile CT11356, AT&T 5046

Tim L,

Please find attached a revised RFDS for CT11356.

We have changed the Antenna model and have confirmed line size.

Additional comments have been modified for we are no longer making any modifications to our 2G equipment.

Please call with any clarification questions needed.

Thanks.

Hans Fiedler
Development Manager CT
T-Mobile
35 Griffin Road
Bloomfield, CT 06002
Office 860-692-7123
Mobile: 860-436-0333

-----Original Message-----

From: Tim Lynn [mailto:TLynn@nat-eng.com]
Sent: Monday, June 29, 2009 1:27 PM
To: grayrd@nu.com; Tim.Burks@SAI-Comm.com; Fiedler, Hans
Subject: CL&P structure #1102, T-Mobile CT11356, AT&T 5046

Gentlemen,

Along with verifying the new antenna locations please verify that none of the inventory has changed.

We have the following for the tower.

T-Mobile:

- (3) RFS APX16PV-16PVL @114'
- (3) RFS APXV18-206516s-A20 @114' on proposed mast
 - (12) 1-1/4" dia. coax cables
- (6) 1-1/4" dia. coax cables - Proposed

AT&T:

- (3) Powerwave 7770 panel antennas @ 104'
- (6) Powerwave LGP21401 TMAs
- (6) Powewave LGP21901 Diplexers

(6) 1-1/4" dia. coax cables

Timothy J. Lynn, EIT
Structural Engineer

Natcomm. Inc,
63-2 North Branford Road
Branford, CT 06405
(t) 203.488.0580 ext.149
(f) 203.488.8587
email: t.lynn@nat-eng.com

UMTS RFDS v2.0

T-Mobile

Site ID	CT11356C	Site Type	Co-Location
Address	2 Wiliruss Street Pole #1102 Line # 1880, Norwalk, CT, 6850	Latitude	41.12576
		Longitude	-73.4327

TMO UMTS Engineer: M Lucey

GSM Impacted?

Alpha	X
Beta	X
Gamma	X
Delta	

History (approvals)	Date
RFDS	07/01/09
GSM RF Acceptance	

RFDS Revision: 4

Site Leasing/Zoning	Preliminary Leasing	Preliminary Zoning
* # of Sectors	6	---
* # of Antennas	6	not specified
Antenna Model	EMS DB65-18-02DPLQ	---
Antenna Size	---	not specified
* # of TMA	not specified	---
* # of Feeders	not specified	not specified
Feeder Diameter	1 5/8	NA
Leased area (sq ft)	not specified	not specified
* # of Cabinets	3	---
Cabinet Model	S8000	---
Site Comments	Cabinet reduction, all coax run to primary cabinet. UMTS overlay.	

* Legend: Config under threshold Config meets threshold Config above threshold Text / Not checked

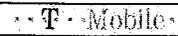
GSM Information

Existing Configuration				Proposed Configuration			
Alpha	Beta	Gamma	Delta	Alpha	Beta	Gamma	Delta
114	114	114		114	114	114	
YES	YES	YES		YES	YES	YES	
1 1/4"	1 1/4"	1 1/4"		1 1/4"	1 1/4"	1 1/4"	
130	130	130		130	130	130	
3	3	2		3	3	2	
4	3	2		4	3	2	
S12000 outdoor 2				S12000 outdoor 1			

UMTS Information

Existing Configuration				Proposed Configuration			
Alpha	Beta	Gamma	Delta	Alpha	Beta	Gamma	Delta
---	---	---	---	114	114	114	
---	---	---	---	YES	YES	YES	
---	---	---	---	1 1/4"	1 1/4"	1 1/4"	
---	---	---	---	130	130	130	
---				RBS 3106 1			

UMTS RFDS v2.0



Site ID	CT11356C	Site Type	Co-Location
Address	2 Willruss Street Pole #1102 Line # 1880, Norwalk, CT, 6850	Latitude	41.12576
		Longitude	-73.4327

TMO UMTS Engineer:

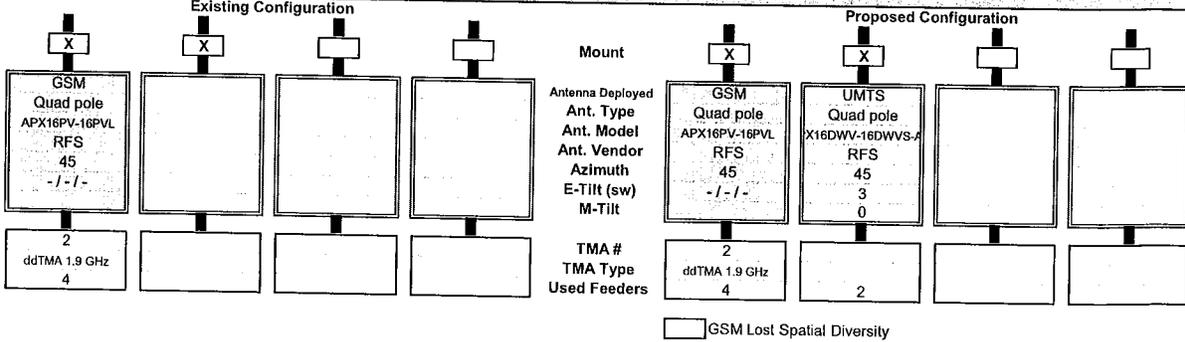
GSM Impacted?

Alpha	<input checked="" type="checkbox"/>
Beta	<input checked="" type="checkbox"/>
Gamma	<input checked="" type="checkbox"/>
Delta	<input type="checkbox"/>

History (approvals)	Date
RFDS	07/01/09
GSM RF Acceptance	

RFDS Revision:

ALPHA



UMTS RFDS v2.0

T-Mobile

Site ID	CT11356C	Site Type	Co-Location
Address	2 Willruss Street Pole #1102 Line # 1880, Norwalk, CT, 6850	Latitude	41.12576
		Longitude	-73.4327

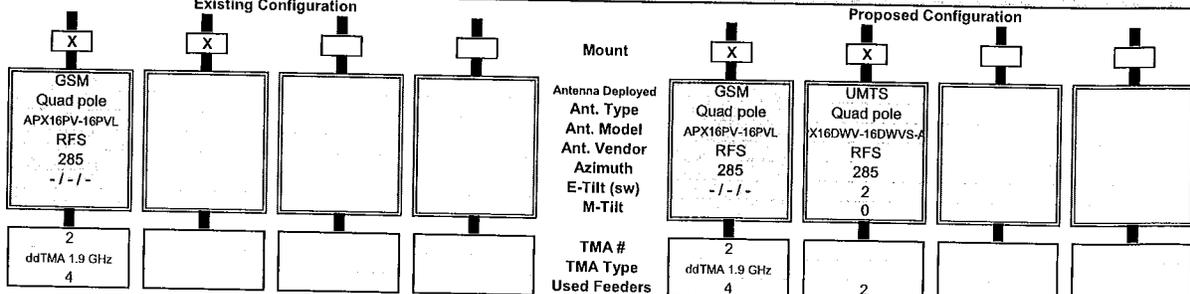
TMO UMTS Engineer: M Lucey

GSM Impacted?	
Alpha	X
Beta	X
Gamma	X
Delta	X

History (approvals)	Date
RFDS	07/01/09
GSM RF Acceptance	

RFDS Revision: 4

GAMMA



GSM Lost Spatial Diversity

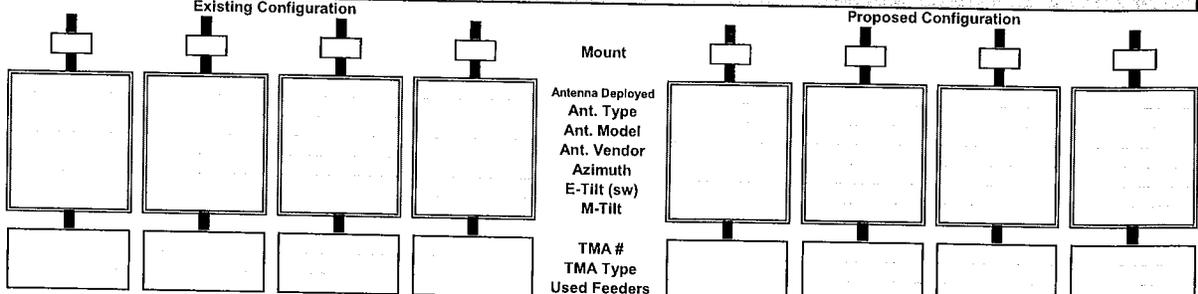
Req	OK
X	
X	

- Add new Mount
- Relocate GSM antenna
- Swap GSM antenna
- Consolidate GSM feeders
- Add Twin TMA
- Swap single TMA with twin TMA
- Add Booster
- Add two new feeders for UMTS
- Reuse GSM feeders for UMTS

Comments

Add new antenna and 2 coax on new mount opposite existing 2G antenna. We will go above AT&T's location with a new mount and replace AT&T's equipment. No UMTS TMA, leave 2G TMA as is unless needed to move to the one remaining cabinet. Tie in RET system for 3G only, leave existing 2G as is since we will not touch that system

DELTA



GSM Lost Spatial Diversity

Req	OK

- Add new Mount
- Relocate GSM antenna
- Swap GSM antenna
- Consolidate GSM feeders
- Add Twin TMA
- Swap single TMA with twin TMA
- Add Booster
- Add two new feeders for UMTS
- Reuse GSM feeders for UMTS

Comments

From: "BURKS, TIM (ATTCINW)" <TB7635@att.com>
To: "Tim Lynn" <TLynn@nat-eng.com>
Date: 7/1/2009 2:42:59 PM
Subject: RE: CL&P structure #1102, T-Mobile CT11356, AT&T 5046

On second thought, let's just stay with the original plan for ATT. RF Data Sheet attached.

3 Powerwave 7770 antennas
6 Powerwave LGP 21401 TMAs
No Diplexers
6 1-1/4" coax
3 1/2" RET cables

Tim Burks
AT&T Mobility
500 Enterprise Drive, Suite 3A, Rocky Hill, CT 06067
(860) 513-7218 desk (860) 513-7190 fax (860) 989-0001 mobile

-----Original Message-----

From: Tim Lynn [mailto:TLynn@nat-eng.com]
Sent: Wednesday, July 01, 2009 11:40 AM
To: Tim Burks
Subject: RE: CL&P structure #1102, T-Mobile CT11356, AT&T 5046

Tim,

What do you want to use to mount the 6 antennas, 6 tma's, 6 diplexers to meet your RF requirements for standoff/separation.

Timothy J. Lynn, EIT
Structural Engineer

Natcomm. Inc,
63-2 North Branford Road
Branford, CT 06405
(t) 203.488.0580 ext.149
(f) 203.488.8587
email: t.lynn@nat-eng.com

>>> "Tim Burks" <Tim.Burks@SAI-Comm.com> 6/30/2009 9:32 PM >>>
Would it be possible for ATT to get 6 antennas, 6 TMAs, 6 Diplexers,
12
coax?

-----Original Message-----

From: Tim Lynn [mailto:TLynn@nat-eng.com]
Sent: Monday, June 29, 2009 1:27 PM
To: grayrd@nu.com; Tim Burks; Hans.Fiedler@T-Mobile.com
Subject: CL&P structure #1102, T-Mobile CT11356, AT&T 5046

Gentlemen,

Along with verifying the new antenna locations please verify that none

of the inventory has changed.
We have the following for the tower.

T-Mobile:

- (3) RFS APX16PV-16PVL @114'
- (3) RFS APXV18-206516s-A20 @114' on proposed mast
 - (12) 1-1/4" dia. coax cables
- (6) 1-1/4" dia. coax cables - Proposed

AT&T:

- (3) Powerwave 7770 panel antennas @ 104'
- (6) Powerwave LGP21401 TMAs
- (6) Powewave LGP21901 Diplexers
- (6) 1-1/4" dia. coax cables

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email: t.lynn@nat-eng.com



AT&T Mobility

New England Market

RF Configuration Data Sheet (Pre-install)

Site No.:

Site Name:

Address:

Latitude (DMS):

Longitude (DMS):

Latitude: N

Longitude: W

UMTS Polygon:

IP Address:

Updated on:

Sector	1	2	3
Number of existing antennas	1	2	3
Number of antennas to be replaced	1	1	1
Existing antenna model	1	1	1
Existing antenna azimuth	7262.02	7262.02	7262.02
Existing antenna center line (ft)	0	120	240
Existing number of feeders	104	104	104
Existing feeder manufacturer	2	2	2
Existing feeder diameter	Andrew	Andrew	Andrew
Existing feeder length (ft)	1 1/4"	1 1/4"	1 1/4"
Replace existing feeder	145	145	145
Sectorization required	No	No	No
New antenna center line (ft)	N/A	N/A	N/A
New antenna model	104	104	104
New antenna vendor	7770 (85° / 4.6ft)	7770 (85° / 4.6ft)	7770 (85° / 4.6ft)
Number of new antennas	Powerwave	Powerwave	Powerwave
New antenna dimensions LxWxD (inch)	1	1	1
New antenna weight (lb)	55 x 11 x 5	55 x 11 x 5	55 x 11 x 5
New mechanical tilt (degree)	35	35	35
New electrical tilt - 850 MHz band (degree)	0	0	0
New electrical tilt - 1900 MHz band (degree)	TBD	TBD	TBD
New antenna azimuth	2 (ANT1)	2 (ANT1)	0 (ANT1)
Total number of feeder runs	0	0	0
Number of new feeders	2	2	2
New feeder diameter	0	0	0
New feeder length (ft)	N/A	N/A	N/A
New feeder vendor	N/A	N/A	N/A
Number of jumper cable A	N/A	N/A	N/A
Number of jumper cable B	4	4	4
Number of jumper cable C	2	2	2
Number of jumper cable D	2	2	2
Jumper cable A & B vendor / model	4	4	4
Jumper cable C & D vendor / model	Andrew / LDF4-50A (1/2")	Andrew / LDF4-50A (1/2")	Andrew / LDF4-50A (1/2")
Total number of jumper cable	Andrew / LDF4-50A (1/2")	Andrew / LDF4-50A (1/2")	Andrew / LDF4-50A (1/2")
Total number of TMA	12	12	12
Number of new TMA	2	2	2
TMA vendor / model	2	2	2
No. of new Bias-T/CIN (for TMA / Surge Arrestor)	Powerwave / LGP 21401 (Dual Band - 850 Bypass)	Powerwave / LGP 21401 (Dual Band - 850 Bypass)	Powerwave / LGP 21401 (Dual Band - 850 Bypass)
Bias-T/CIN vendor / model (for TMA / S. Arrestor)	2	2	2
Number of PDU for TMA	Polyphaser / 1000860	Polyphaser / 1000860	Polyphaser / 1000860
Model of PDU for TMA	1	1	1
Number of new diplexer at BTS end	LGP 12104	LGP 12104	LGP 12104
Number of new diplexer at antenna end	2	2	2
Diplexer vendor / model	0	0	0
Number of new diplexer at BTS	Powerwave / LGP 21901	Powerwave / LGP 21901	Powerwave / LGP 21901
Duplexer vendor / model	N/A	N/A	N/A
Number of attenuators	N/A	N/A	N/A
Total number of RCU/RET	N/A	N/A	N/A
RCU/RET vendor / model	1	1	1
Number of new Bias-T/CILOC (for RCU/RET)	Powerwave / 7020 (DB)	Powerwave / 7020 (DB)	Powerwave / 7020 (DB)
Bias-T/CILOC vendor / model (for RCU/RET)	0	0	0
Number of RCU/RET cable at antenna end	N/A	N/A	N/A
Number of RCU/RET cable at BTS end	0	0	0
Number of RCS splitters	1	1	1
RC feeder cable model	N/A	N/A	N/A
Number of RC feeder cable	N/A	N/A	N/A
Number of LPD (Kathrein 860-10030)	N/A	N/A	N/A
Number of CCU/MCU for RCU/RET	N/A	N/A	N/A
Model of CCU/MCU for RCU/RET	1	1	1
Node B/BTS type	Ericsson RBS 3000 series	Ericsson RBS 3000 series	Ericsson RBS 3000 series
Sector comment	Powerwave / 7070	Powerwave / 7070	Powerwave / 7070
Site comment	Existing 1900 RXAIT	Existing 1900 RXAIT	Existing 1900 RXAIT
Plumbing Diagram Template			

AT&T RF Engineer:

Cingular PM Manager:

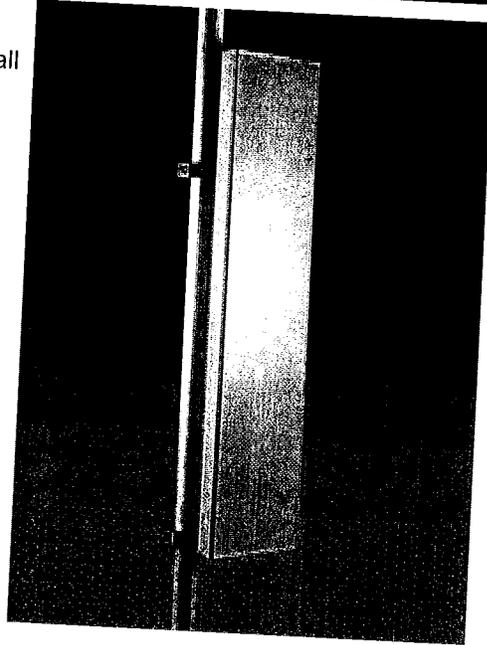
Date Issued:

Version:



Product Description

Gathering two X-Polarised antennas in a single radome this pair of variable tilt antenna provides exceptional suppression of all upper sidelobes at all downtilt angles. It also features a wide downtilt range with optional remote tilt.



Features/Benefits

- Variable electrical downtilt - provides enhanced precision in controlling intercell interference. The tilt is infield adjustable 0-10 deg.
- High Suppression of all Upper Sidelobes (Typically <-20dB).
- Optional remote tilt - can be retrofitted.
- Two X-Polarised panels in a single radome.
- Dual polarization.
- Low profile for low visual impact.
- Broadband design.

Technical Features

Frequency Band	PCS 1900 (1850-1990 MHz)
Horizontal Pattern	Directional
Antenna Type	Panel Dual Polarized
Electrical Down Tilt Option	Variable
Gain, dBi (dBd)	17.8 (15.8) , 17.8 (15.8)
Frequency Range, MHz	1850-1990 , 1850-1990

RFS The Clear Choice™

APX16PV-16PVL-C

Print Date: 21.03.2005

Please visit us on the internet at <http://www.rfsworld.com>

Radio Frequency Systems

All information contained in the present datasheet is subject to confirmation at time of ordering.



Optimizer® Panel Dual Polarized Antenna

Connector Type	(4) 7-16 DIN Female
Connector Location	Bottom
Mount Type	Downtilt
Electrical Downtilt, deg	0-10 , 0-10
Horizontal Beamwidth, deg	66 , 66
Mounting Hardware	APM40-2
Rated Wind Speed, km/h (mph)	160 (100)
VSWR	< 1.5:1
Vertical Beamwidth, deg	6.6
1st Upper Sidelobe Suppression, dB	> 17 (typically > 20)
Upper Sidelobe Suppression, dB	> 18 all (typically > 20)
Polarization	Dual pol +/-45°
Front-To-Back Ratio, dB	> 25
Maximum Power Input, W	300
Isolation between Ports, dB	> 30
Lightning protection	Direct Ground
3rd Order IMP @ 2 x 38 dBm, dBc	> 160
Overall Length, m (ft)	1.35 (4.42)
Dimensions - HxWxD, mm (in)	1349 x 330 x 80 (53 x 12.9 x 3.1)
Weight w/o Mtg. Hardware, kg (lb)	18.0 (39.6)
Radiating Element Material	Brass
Radome Material	Fiberglass
Reflector Material	Aluminum
Max Wind Loading Area, m ² (ft ²)	0.64 (6.6)
Maximum Thrust @ Rated Wind, N (lbf)	787 (177)
Shipping Weight, kg (lb)	23.8 (52)
Packing Dimensions, HxWxD, mm (in)	1550 x 420 x 210 (61 x 16.5 x 8.3)
Survival Wind Speed, km/h (mph)	200 (125)

All information contained in the present datasheet is subject to confirmation at time of ordering.

RFS The Clear Choice™

APX16PV-16PVL-C

Print Date: 21.03.2005

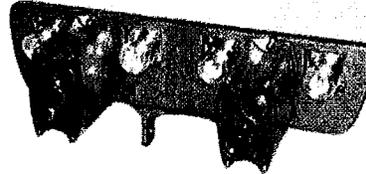
Please visit us on the internet at <http://www.rfsworld.com>

Radio Frequency Systems



Product Description

A combination of two X-Polarized antennas in a single radome, this pair of variable tilt antennas provides exceptional suppression of all upper sidelobes at all downtilt angles. It also features a wide downtilt range. This antenna is optimized for performance across the entire frequency band (1710-2200 MHz). The antenna comes pre-connected with two antenna control units (ACU).



Features/Benefits

- Variable electrical downtilt - provides enhanced precision in controlling intercell interference. The tilt is infield adjustable 0-10 deg.
- High Suppression of all Upper Sidelobes (Typically <-20dB).
- Gain tracking - difference between AWS UL (1710-1755 MHz) and DL (2110-2155 MHz) <1dB.
- Two X-Polarised panels in a single radome.
- Azimuth horizontal beamwidth difference <4deg between AWS UL (1710-1755 MHz) and DL (2110-2155 MHz).
- Low profile for low visual impact.
- Dual polarization; Broadband design.
- Includes (2) AISG 2.0 Compatible ACU-A20-N antenna control units.

Technical Features

Frequency Band	3G/UMTS (Single, Broad, Dual and Triple-Band)
Horizontal Pattern	Directional
Antenna Type	Panel Dual Polarized - Side by Side
Electrical Down Tilt Option	Variable
Gain, dBi (dBd)	18.4 (16.3)
Frequency Range, MHz	1710-2200
Connector Type	(4) 7-16 DIN Female
Connector Location	Bottom
Mount Type	Downtilt
Electrical Downtilt, deg	0-10, 0-10
Horizontal Beamwidth, deg	65
Mounting Hardware	APM40-2
Rated Wind Speed, km/h (mph)	160 (100)
VSWR	< 1.5:1
Vertical Beamwidth, deg	5.9 to 7.7
1st Upper Sidelobe Suppression, dB	> 18 (typically > 20)
Upper Sidelobe Suppression, dB	> 18 all (typically > 20)
Polarization	Dual pol +/-45°
Front-To-Back Ratio, dB	>26 (typically 28)
Maximum Power Input, W	300

RFS The Clear Choice™

APX16DWV-16DWVS-C-A20

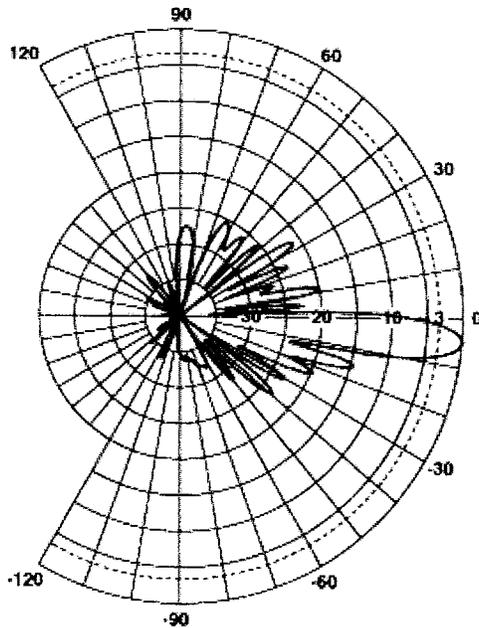
Print Date: 03.11.2008



Isolation between Ports, dB	> 30
Lightning Protection	Direct Ground
3rd Order IMP @ 2 x 43 dBm, dBc	> 150 (155 Typical)
Impedance, Ohms	50
Overall Length, m (ft)	1.42 (4.6)
Mounting Hardware Weight, kg (lb)	3.4 (7.5)
Dimensions - HxWxD, mm (in)	1420 x 337 x 80 (55.9 x 13.3 x 3.15)
Weight w/o Mtg Hardware, kg (lb)	18.5 (40.7)
Radiating Element Material	Brass
Radome Color	Light Grey RAL7035
Radome Material	Fiberglass
Mounting Hardware Material	Diecasted Aluminum
Reflector Material	Aluminum
Max Wind Loading Area, m ² (ft ²)	0.64 (6.6)
Survival Wind Speed, km/h (mph)	200 (125)
Maximum Thrust @ Rated Wind, N (lbf)	787 (177)
Front Thrust @ Rated Wind, N (lbf)	787 (177)
Packing Dimensions, HxWxD, mm (in)	1550 x 420 x 260 (61 x 16.5 x 10.3)

Notes

For additional mounting information please click "External Document Link" below.



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Dual Broadband Antenna

90° 1.4 m MET Antenna

Part Number:
7770.00

Horizontal Beamwidth: 90°
Gain: 13.5/16 dBi

Electrical Downtilt: Adjustable
Connector Type: 7/16 female

The Powerwave dual band dual polarized broadband antenna has individual adjustable electrical downtilt per band (upgradeable to Remote Electrical Tilt (RET)). Four connector ports allow separate tilts on each frequency band and ensure the use of diversity concepts. The phase shifter technology, based on a patented sliding dielectric, minimizes intermodulation distortion and maximizes efficiency. The slant +/- 45° dual polarization system provides the independent fading signals needed for achieving top-quality coverage via diversity concepts. The Powerwave Broadband antenna design is based on a patented stacked aperture-coupled patch technology, which provides high isolation performance and a wide VSWR bandwidth. The antennas have superior radiation patterns due to a unique reflector design which provides a very small variation of the -3dB horizontal beam width over the frequency band as well as a high front-to-back ratio.

800-988-7710



Key Benefits

- Excellent broad- and multi-band capabilities
- Polarization purity makes good diversity gain
- Excellent pattern performance and high gain over frequency
- High passive intermodulation performance
- Light, slim and robust design

Preliminary

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 **Powerwave**
technologies

Dual Broadband Antenna

Electrical Specifications (Preliminary)

Frequency band (MHz)	806-960	1710-2170
Gain, ± 0.5 dB (dBi)	13.5	16.0
Polarization	Dual linear $\pm 45^\circ$	
Nominal Impedance (Ohm)	50	
VSWR	1.5:1	
VSWR		1.5:1
Isolation between inputs (dB)	30	
Isolation between inputs (dB)		30
Inter band isolation (dB)	40	
Horizontal -3 dB beamwidth	$85 \pm 5^\circ$	$85 \pm 5^\circ$
Tracking, Horizontal plane, $\pm 60^\circ$ (dB)	< 2.0	
Tracking, Horizontal plane, $\pm 60^\circ$ (dB)		< 2.0
Electrical downtilt range (adjustable)	0° to 10°	0° to 8°
Vertical -3 dB beamwidth	$14.3 \pm 2.0^\circ$	$6.6 \pm 1^\circ$
Sidelobe suppression, Vertical 1 st upper (dB)	$> 17, 16, 15$ $x=0, 5, 10^\circ$ MET	$> 17, 16, 15$ $x=0, 4, 8^\circ$ MET
Vertical beam squint	$< 0.8^\circ$	$< 0.5^\circ$
First null-fill (dB)	< -25	< -25
Front-to-back ratio (dB)	> 25	> 27
Front-to-back ratio, total power (dB)	> 20	> 23
IM3, 2Tx@43dBm (dBc)	< -153	
IM3, 2Tx@43dBm (dBc)		< -153
IM7, 2Tx@43dBm (dBc)		< -160
Power Handling, Average per input (W)	400	250
Power Handling, Average total (W)	800	500

All specifications are subject to change without notice.
Contact your Powerwave representative for complete performance data.

Mechanical Specifications

Connector Type	4 x 7/16 DIN female
Connector Position	Bottom
Dimensions, HxWxD	1408mm x 280mm x 125mm (55"x11"x5")
Weight Including Brackets	15.8 kg (35 lbs)
Wind Load, Frontal, 42m/s Cd=1	435N (98 lbf)
Survival Wind Speed (m/s)	70 (156mph)
Lightning Protection	DC grounded
Radome Material	GRP
Radome Color	Light Gray
Mounting	Pre-mounted Standard Brackets
Packing Size	1550mm x 355mm x 255mm (61"x14"x10")

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Tower Mounted Amplifier

Dual Band 1900 MHz with 850 MHz Bypass

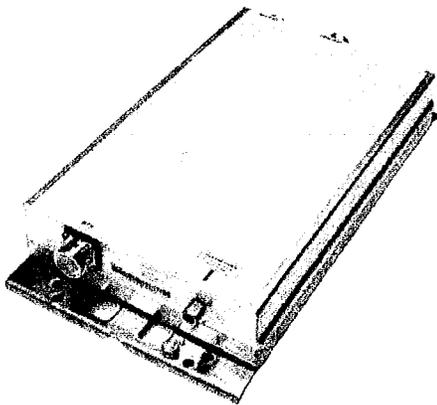
Part Number:
LGP 214nn

Up-link: 1850-1910 MHz
Down-link: 1930-1990 MHz
Bypass: 824-894 MHz

Gain: 12 dB
Noise Figure: < 1.7 dB

The Powerwave® TMA-DD 1900/850 is a dual band Tower Mounted Amplifier (TMA) to be installed near the antenna. Deployed in an AMPS, GSM, GPRS, EDGE and CDMA network it will increase capacity and coverage as well as extend the battery life time for the handsets. The TMA System will provide enhanced coverage and improved up-link signal quality. Appropriate for new rollouts by optimizing coverage with a reduced number of BTSs or as an upgrade to existing BTSs for enhancing the existing coverage.

Extended band TMA facilitates simplified logistics, especially when the frequency bands are scattered. The unit comprises of high Q band-pass filters, dual balanced low noise amplifiers with circuits for active bias, supervision, alarms and lightning protection circuit. The Powerwave patented design with all active components integrated within the filter body provides an extremely reliable, compact and lightweight TMA solution. The vented enclosure design is employed to prevent the effect of condensation, thereby guaranteeing long, reliable, maintenance-free service in all environmental conditions. These TMAs offer an easy to install, maintenance free, cost effective solution for coverage enhancement and increased quality in mobile communication networks.



Key Benefits:

- 850 MHz Bypass
- Improved Network Quality
- Increased Coverage
- State of the Art Performance
- Excellent Power Handling
- Low Tx Loss
- Exceptional Reliability

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Tower Mounted Amplifier

Technical Specifications

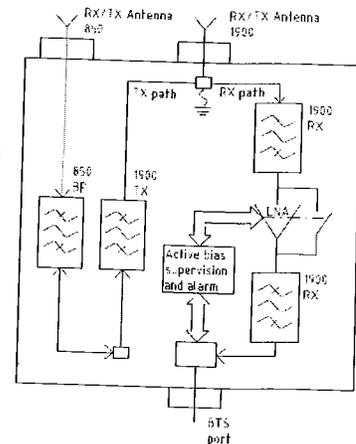
Product Number	LGP214nn	
850 MHz	Bypass (MHz)	824-894
	Return loss* (dB)	> 20
	Insertion loss* (dB)	< 0.3
1900 MHz		
Up-link	Frequency range, full band (60 MHz)	1850-1910
	Nominal gain (dB)	12
	Return loss* (dB)	> 20
	Noise figure* (dB)	< 1.7
	Output 3rd order Intercept Point* (dBm)	> +23
Down-link	Frequency range, full band (60 MHz)	1930-1990
	Insertion loss* (dB)	< 0.6
	Return loss* (dB)	> 20
Intermodulation	2 Tx@x43 dBm (dBc)	<-158
Alarm Functionality	Two levels, individually supervised LNAs	
Power Consumption	@12 VDC	1.2 W

* Typical

All specifications subject to change without notice. Please contact your Powerwave representative for complete performance data.

Mechanical Specifications

Size, W x H x D (without mounting plate)	235 x 366 x 66 mm (9.2 x 14.4 x 2.6 in)
Weight	6.4 kg (14.1 lbs)
Color	Off white (NCS 1502-R)
Housing	Aluminum
RF-connectors	DIN 7/16 female.
Mounting kit	Mounting kit for pole and wall is included
Temperature range	-40 °C to +65 °C (-40 °F to +149 °F)
MTBF	> 1 million hours
Safety	UL 60 950
Ingress protection, IP 65	EN 60 529
Environmental	ETS 300 019
EMC	FCC Part 15



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